Achieving Highest Fusion Yields in OMEGA Direct-Drive ICF Through Improved Energy Coupling



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Summary

Recent OMEGA implosions have achieved fuel gains >1 and record fusion yields above 3×10^{14}



- Highest yields on OMEGA (3.1 \times 10¹⁴) achieved using low-convergence, high-velocity (~600 km/s) DT liners
- 1st demonstration of fusion energy exceeding hot-spot energy in SDD* using both high CR^{**} targets and liners
- Silicon doping and multipulse-driver (MPD) show enhanced laser-to-target coupling
- Pressures near 80 Gbar reached with highest hydroscaled χ (0.83) at 2 MJ of laser energy, corresponding to the burning plasma regime



Collaborators



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General Atomics



Motivation



Optimization campaign

• Goal to achieve hydro-equivalent ignition $(\chi = 1)$ when scaled to 2 MJ of laser energy*

Thin-ice DT liner campaign

- Goal to produce the highest possible yields with the most stable implosions
- Possible neutron source on the NIF
- Lower convergence ratios and lower χ but higher yields

Hydro-scaling assumes the same hot-spot pressure at all scales and volume ~ $E_{\text{laser.}}$



Outline



- Fusion performance metrics
- Statistical mapping model
- Target and laser pulse modifications and recent achievements



The performance of direct-drive OMEGA implosions is assessed through measurements of the neutron yield and areal density to infer the Lawson parameter



• The Lawson parameter is hydroscaled

$$\chi \sim P \tau \sim \tau \sim R \sim E_L^{1/3}$$

Hydroequivalent ignition: χ = 1 at \approx 2 MJ

• Scaled ignition For ignition

$$\chi_{MJ} \equiv \chi_{OMEGA} \left(\frac{E_L(MJ)}{E_{Laser}^{OMEGA}} \right)^{1/3} \Rightarrow 1$$

$$\longrightarrow 1$$
About 4.2 × for 2 MJ

A. Christopherson et al, Phys. Plasmas 27, (2020)
 J. D. Lindl et al. Phys. Plasmas 25, 122704 (2018)
 R. Betti et al, Phys. Rev. Lett. 114, 255003 (2015)
 B.K. Spears et al, Phys. Plasmas 19, 056316 (2012)
 O. Hurricane et al, Phys. Plasmas 28, 022702 (2021)



Other performance metrics: hot-spot pressures and energies can be inferred using measurements from neutron and x-ray diagnostics

Generate constraints on P_{hs} and E_{hs} using

$$Y = f_D f_T \int dt \int_0^{R_{hs}} d^3 r \frac{P_i^2}{T_i^2} \langle \sigma v \rangle$$

- $T_i \neq T_e$.
- $T(t,r) \rightarrow T_0 \widehat{T}_{1D}(r)$ and $P(t,r) \rightarrow P_0 \widehat{P}_{1D}(r)$
- Process applied to *LILAC* simulations using synthetic neutron and x-ray diagnostics to ensure bang time profiles are reproduced by this method



LILAC pressure versus LILAC inferred pressure

TC16277

*Charles Cerjan, Paul T. Springer, and Scott M. Sepke , Physics of Plasmas 20, 056319 (2013)



Outline



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Statistical modeling of experimental data mapped onto simulated data is the main tool used to predict implosion performance and extract physical dependencies



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Degradation from short-wavelength perturbations and illumination nonuniformity determines the design space for targets and laser pulses





Outline



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Fusion energy is proportional to the product of hot-spot energy and Lawson parameter, placing a premium on improving the transfer of energy to the hot-spot





The values of χ required for hotspot gain above unity are within range of current OMEGA DT-layered implosions

$${}^{*}G_{hs} \equiv E_{f}/E_{hs}$$
$$G_{hs} \propto \chi$$

• The hotspot inference model on 1-D *LILAC* simulations shows that current OMEGA implosions with χ between 0.16 and 0.2 can access G_{hs} > 1







Laser-target energy coupling is enhanced by using silicon doping, larger OD targets, and multipulse-driver (MPD)





Si-doping leads to higher absorption in experiment and suppresses hot electron production originating from two-plasmon decay



	CD (shot 99922)	CHSi (shot 101777)
Experimental yield	1.6 × 10 ¹⁴	$2.0 imes 10^{14}$
HXRD (pC)	195±24	53±16
Absorption	59±5%	69±5%

P. Farmakis *et al.*, CO04.00003, V. Gopalaswamy *et al.*, CO04.00006, this conference.



Thin-Ice DT liners can reach implosion velocities ~600 km/s but must be driven at high adiabats to maintain stability



C. A. Williams et al., "High yields in direct-drive inertial confinement fusion using thin-ice DT liner targets," Phys. Plasmas 28, 122708 (2021)



Converting shell kinetic energy to hot-spot internal energy is most efficient for high-IFAR, high-adiabat implosions



Recent high-performance implosions are the first to exhibit higher fusion energy than hot-spot internal energy

1000 800 **Hot-spot gain** Fusion energy (J) 600 400 Liner Optimization Si-doped Optimization GDP 200 200 400 800 1000 600 Hot-spot energy (J)

Hotspot gains $G_{HS} > 1$ were reached in recent shots ٠

- Nearly all heating of hotspot comes from compression ٠ work (i.e., negligible alpha heating)
- Achieved with GDP plastic shells, Si-doped shells, • and DT liners

*C. A. Williams et al. in preparation

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2-D Simulations of DT liner shots suggest laser imprint minimally affects implosion performance even at $\alpha \approx 6$ in agreement with statistical modeling





Both liners and χ -optimization shots live in the shaded region.



Hot-spot pressures approaching 80 Gbar are reached in optimization shots, while DT liners demonstrate the highest yields at the lowest convergence ratios



DT liners provide a platform to achieve the highest yields with robust hydrodynamic stability.



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Liners do not reach the same level of extrapolated yield amplification as optimization shots due to lower convergence





Increased coupling has produced several shots that hydroscale into the burning plasma regime

0.4

Burning Plasma **Optimization-GDP**

8.0

2-MJ symmetric drive hydroscaling

Extrapolated Lawson Parameter

0.6

1.0

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0.0

0.0

Ignition

Si-Doped

Pre 100-Gbar

0.2

Liners

V. Gopalaswamy et al., CO04.00006, this conference.

Summary/Conclusions

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Supplemental Slides





Introduction of silicon and MPD appear to mitigate the L=2 perturbation, generating rounder hot spots and more conversion to hot-spot energy





Experimental hot spot x-ray images show liner compression responds to changes in ablator composition and thickness



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Hot-spot Model

$$Y = f_{B}f_{T} \int dt \int_{0}^{R_{hs}} d^{3}r \frac{P_{i}^{2}}{T_{i}^{2}} \langle \sigma v \rangle$$

$$E^{hs} = \sqrt{\frac{9\pi Y}{f_{D}f_{T}\tau}} R_{17}^{3/2} k_{B} \langle T_{i} \rangle \frac{\sqrt{\int_{0}^{1} x^{2} \left(\hat{P}_{i}^{2}/\hat{T}_{i}^{2}\right) \langle \sigma v \rangle \, dx}}{\int_{0}^{1} x^{2} \left(\hat{P}_{i}^{2}/\hat{T}_{i}^{2}\right) \langle \sigma v \rangle \, dx}} \left[\int_{0}^{1} x^{2} \hat{P}_{i} \, dx + \frac{\langle T_{e} \rangle}{\langle T_{i} \rangle} \frac{\int_{0}^{1} x^{2} \left(\hat{P}_{i}^{2}/\hat{T}_{i}\right) \langle \sigma v \rangle \, dx}}{\int_{0}^{1} x^{2} \left(\hat{P}_{i}^{2}/\hat{T}_{i}\right) \langle \sigma v \rangle \, dx} \int_{0}^{1} x^{2} \hat{P}_{e} \, dx \right]$$

$$\tau \to \tau' \approx 1.1\tau$$
Constraining hotspot properties using the yield and FWHM of the neutron rate (the burn width, \tau) is equivalent to saying the red shaded area is equal to the total area of the curve.
$$u^{10} = \frac{10^{10}}{\sqrt{10^{10}}} \frac{10^{$$

