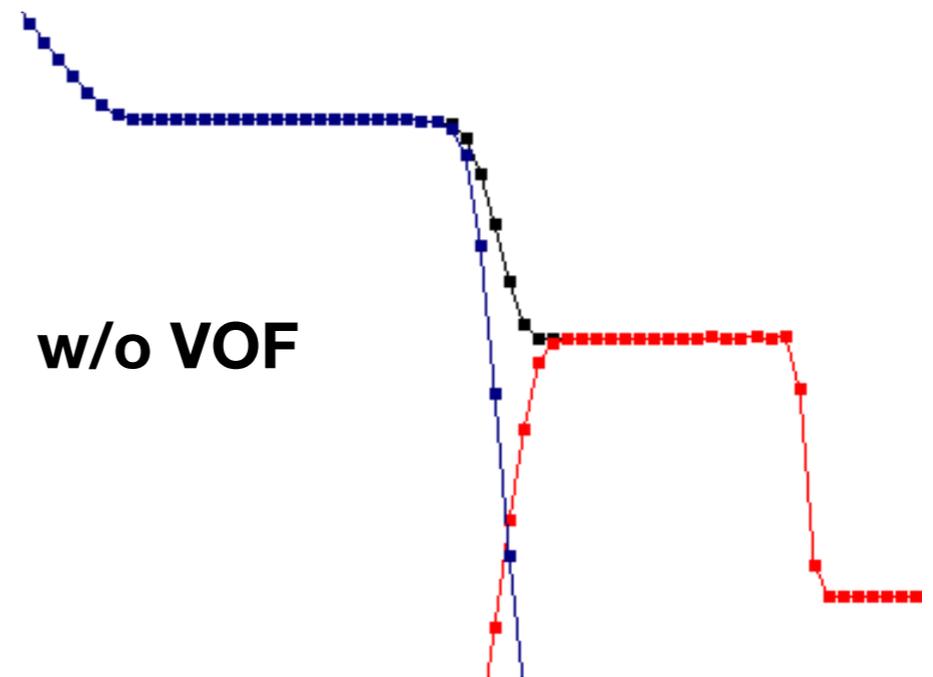
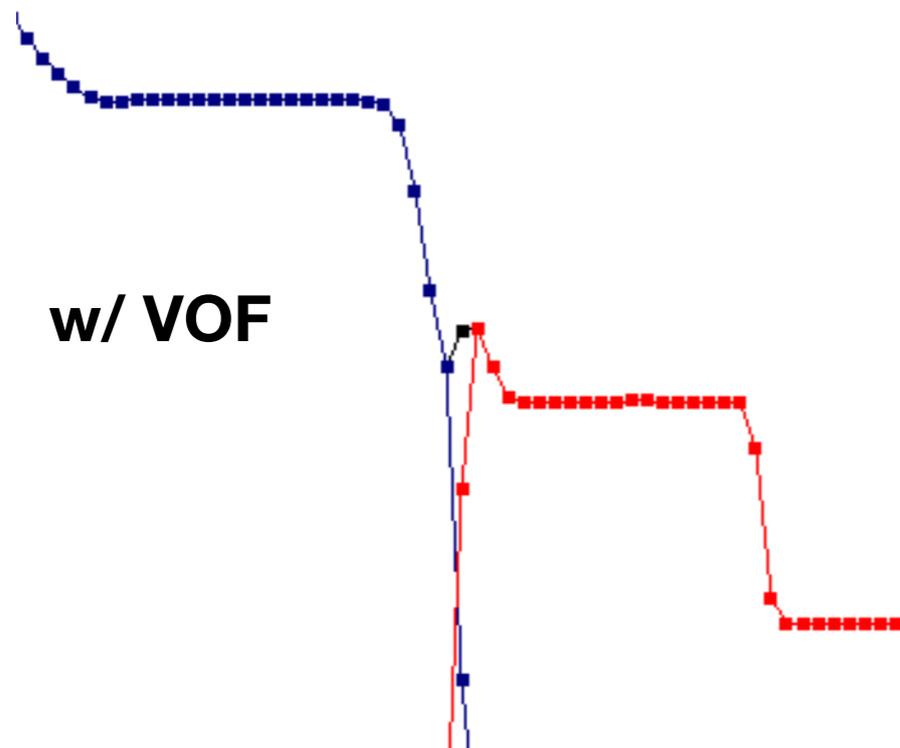


Implementation of a 2D Unsplit Volume of Fluid (VOF) Interface-capturing Method for Multifluid Compressible Flows in the FLASH Code



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63rd Annual APS DPP
Pittsburgh, PA
November 8-12 2021



Acknowledgments



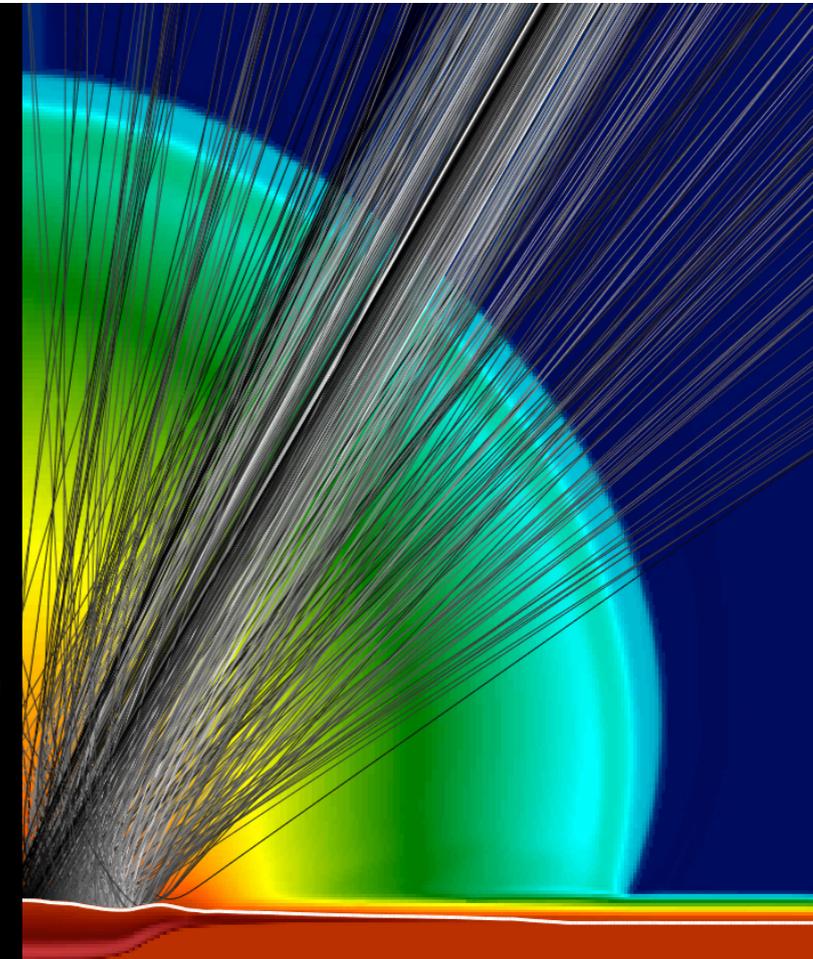
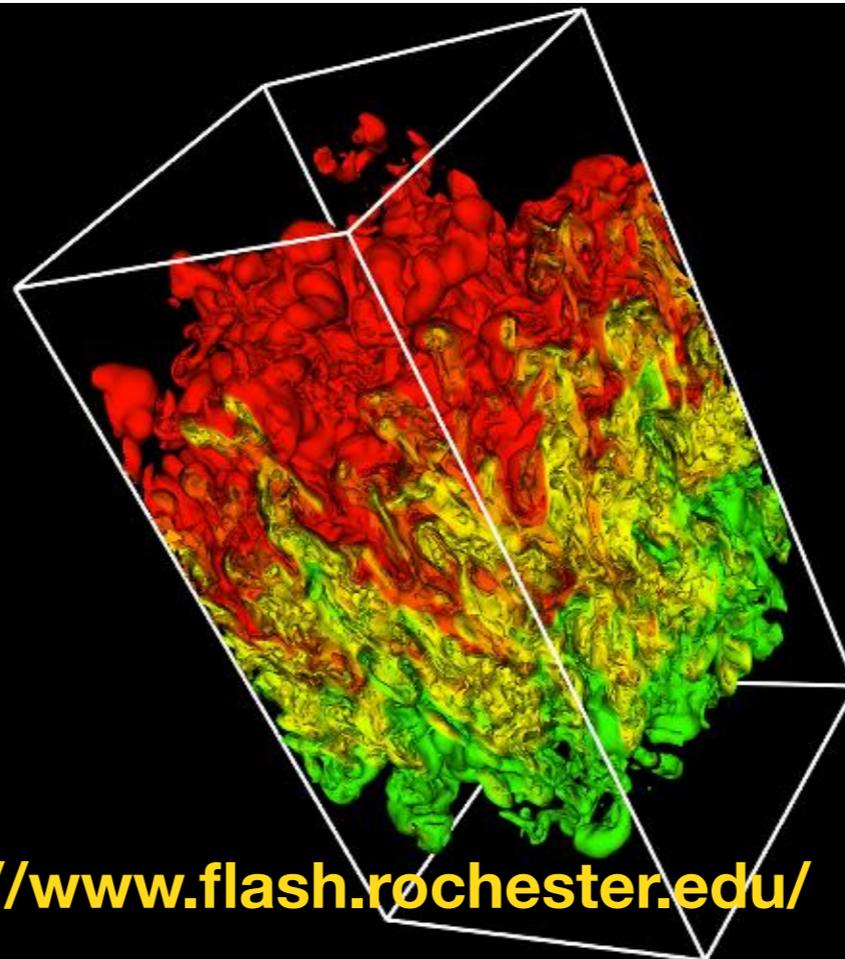
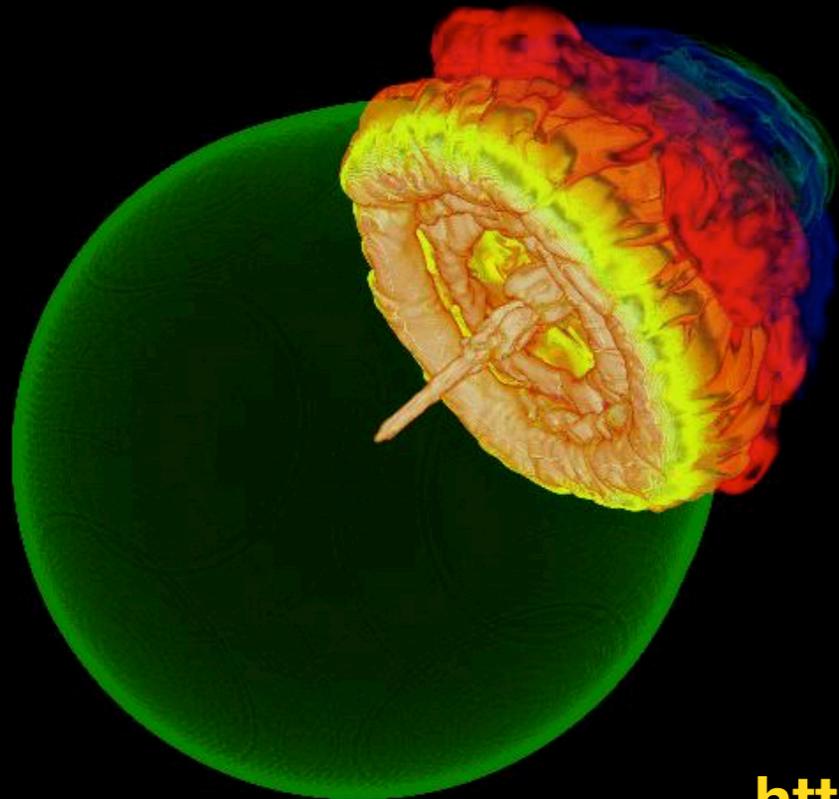
Lawrence Livermore
National Laboratory

The Flash Center acknowledges support by the U.S. DOE ARPA-E under Award DE-AR0001272, the National Science Foundation under Award PHY-2033925, and the U.S. DOE NNSA under Award DE-NA0003842, and Subcontracts 536203 and 630138 with LANL and B632670 with LLNL. This material is based upon work supported by the U.S. DOE NNSA under Award Number DE-NA0003856 through the Horton Fellowship Program at the Laboratory for Laser Energetics.

- ❑ FLASH is a publicly available, high performance computing (HPC), adaptive mesh refinement (AMR), finite-volume, hydro and MHD code with extended physics capabilities. Supported primarily by the U.S. DOE NNSA.
- ❑ FLASH is professionally managed software in continuous development for 20 years: coding standards; version control; daily automated regression testing; extensive documentation; user support; integration of extensive code contributions from external users.

> 3,500 users world wide

>1,200 papers published with
FLASH



<https://www.flash.rochester.edu/>

- Added capability of Flash's hydrodynamics solver to capture interfaces in compressible multi fluid flow using VOF
- Verification on 1D two-fluid Riemann problems shows that Flash is able to correctly predict shock speeds while maintaining material interfaces
- PLIC reconstruction of interfaces enables VOF advection in two dimensions
- Integration with the unsplit hydrodynamics solver in Flash requires corrections for volumes advected through cell corners

- Computational fluid dynamics (CFD) typically treated as an algebraic problem

$$U_i^{n+1} = U_i^n - \frac{1}{\Delta t} \int_{t^n}^{t^{n+1}} \frac{1}{\Delta x} (\hat{f}_{i+1/2} - \hat{f}_{i-1/2}) dt$$

- Tracking material interfaces is inherently a geometric problem
- The volume-of-fluid (VOF) method attempts to bridge the two
 - Evolve volume fraction of component fluids (interface capturing)
 - Reconstruct material interfaces from volume fractions

- (i) Single Velocity for all component fluids
 - (ii) Material interfaces remain in pressure equilibrium
-
- Pure cells neighboring pure cells w/ same type treated like single fluid hydro
 - Mixed cells and cells with potential to become mixed get interface reconstruction & volume advection

W. J. Rider and D. B. Kothe, "Reconstructing Volume Tracking," *Journal of Computational Physics*, vol. 141, no. 2, pp. 112–152, Apr. 1998, doi: [10.1006/jcph.1998.5906](https://doi.org/10.1006/jcph.1998.5906). [1]

G. H. Miller and E. G. Puckett, "A High-Order Godunov Method for Multiple Condensed Phases," *Journal of Computational Physics*, vol. 128, no. 1, pp. 134–164, Oct. 1996, doi: [10.1006/jcph.1996.0200](https://doi.org/10.1006/jcph.1996.0200). [2]

E. G. Puckett and J. S. Saltzman, "A 3D adaptive mesh refinement algorithm for multimaterial gas dynamics," *Physica D: Nonlinear Phenomena*, vol. 60, no. 1–4, pp. 84–93, Nov. 1992, doi: [10.1016/0167-2789\(92\)90228-F](https://doi.org/10.1016/0167-2789(92)90228-F). [3]

$$\partial_t(f^\alpha) + \nabla \cdot (\mathbf{u} f^\alpha) = \frac{f^\alpha \Gamma}{\Gamma^\alpha} \nabla \cdot \mathbf{u}$$

- “advected” volume fractions are updated ignoring RHS
- $\nabla \cdot \mathbf{u}$ is inferred by enforcing sum of volume fractions to be one

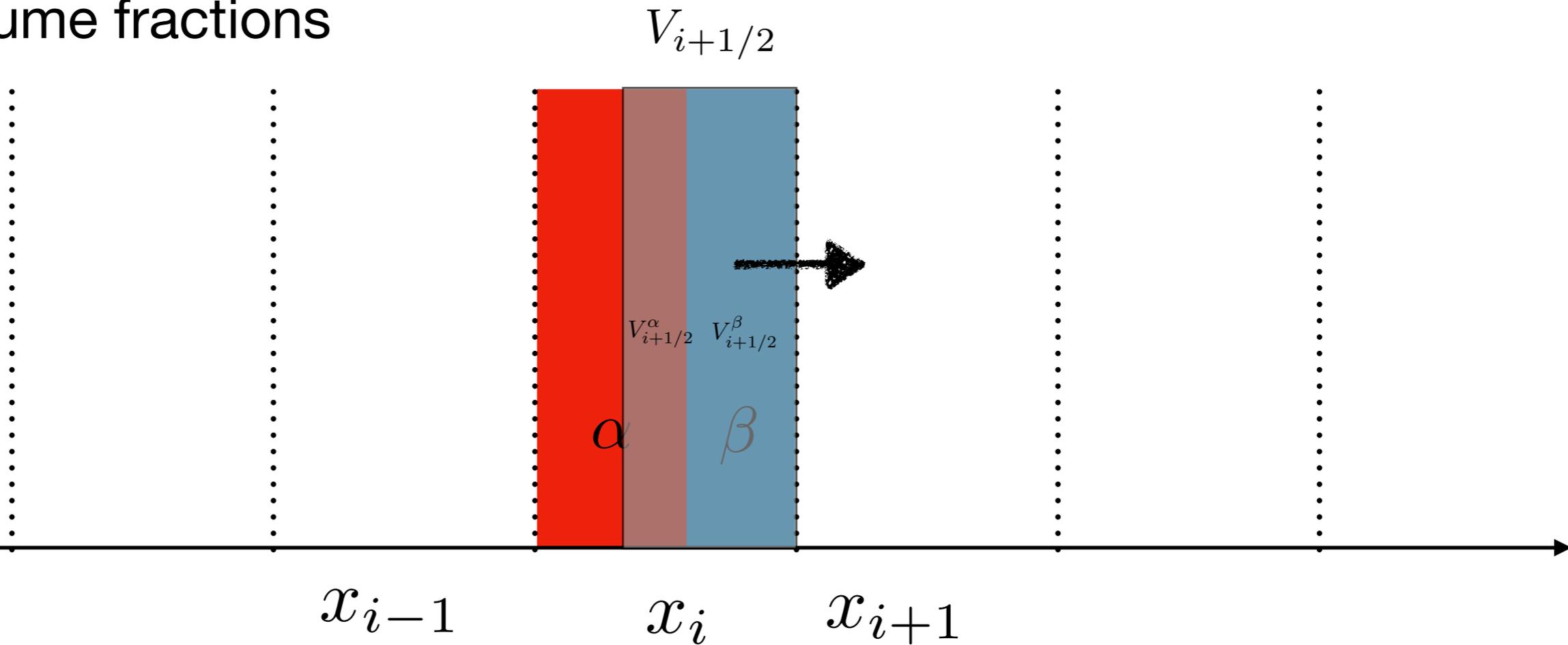
$$f^{\alpha,adv} = f^{\alpha,n} - \frac{1}{V_i} \left(V_{i+1/2}^{\alpha,adv} - V_{i-1/2}^{\alpha,adv} \right)$$

$$\nabla \cdot \mathbf{u}_i \approx 1 - \sum_{\alpha} f^{\alpha,adv}$$

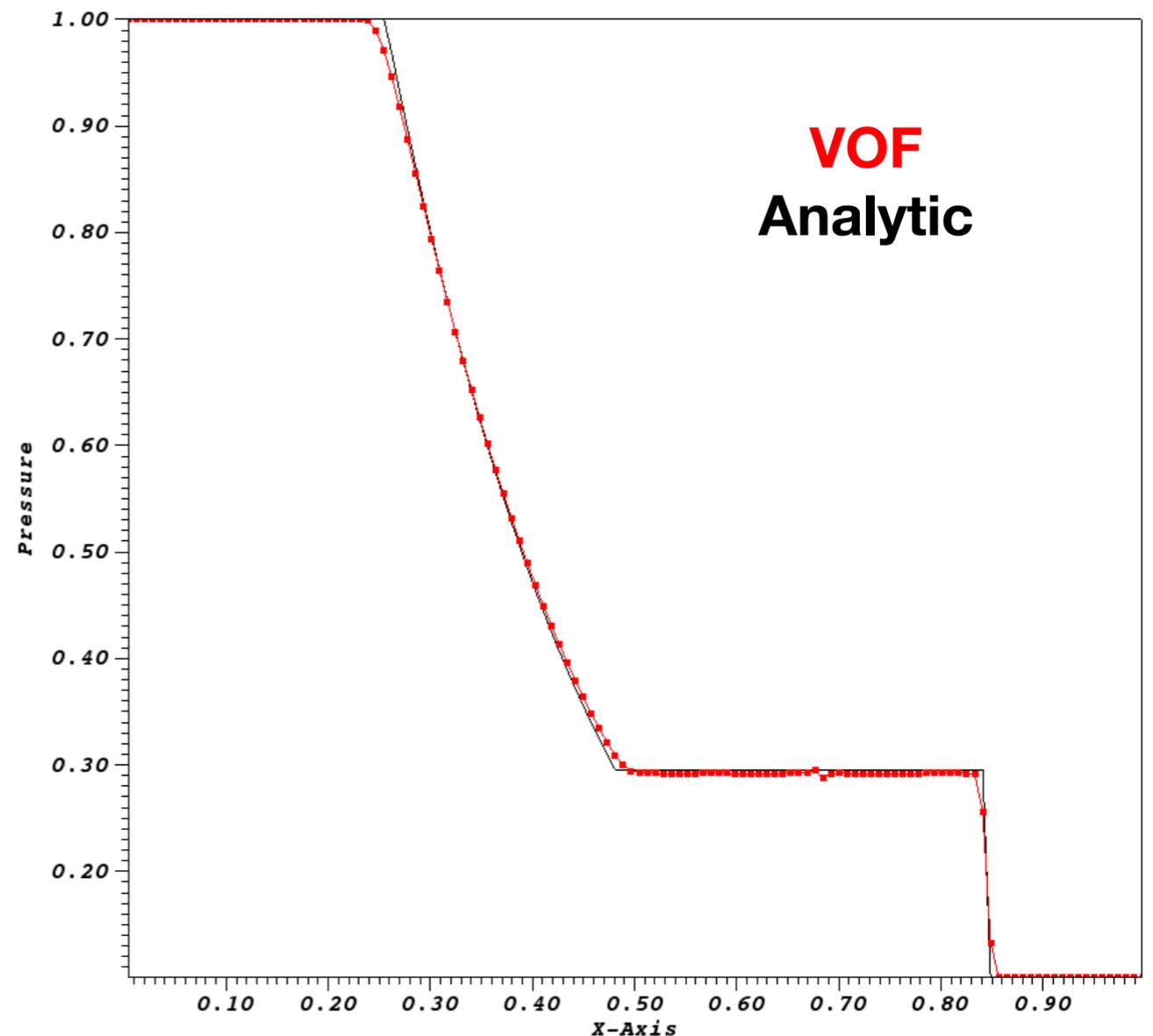
- Γ^α also needs to be advected with the volume

$$\Gamma^\alpha \equiv \frac{\rho^\alpha c_\alpha^2}{P^\alpha} \quad \Gamma = \left(\sum_{\alpha} \left(\frac{f^\alpha}{\Gamma^\alpha} \right) \right)^{-1}$$

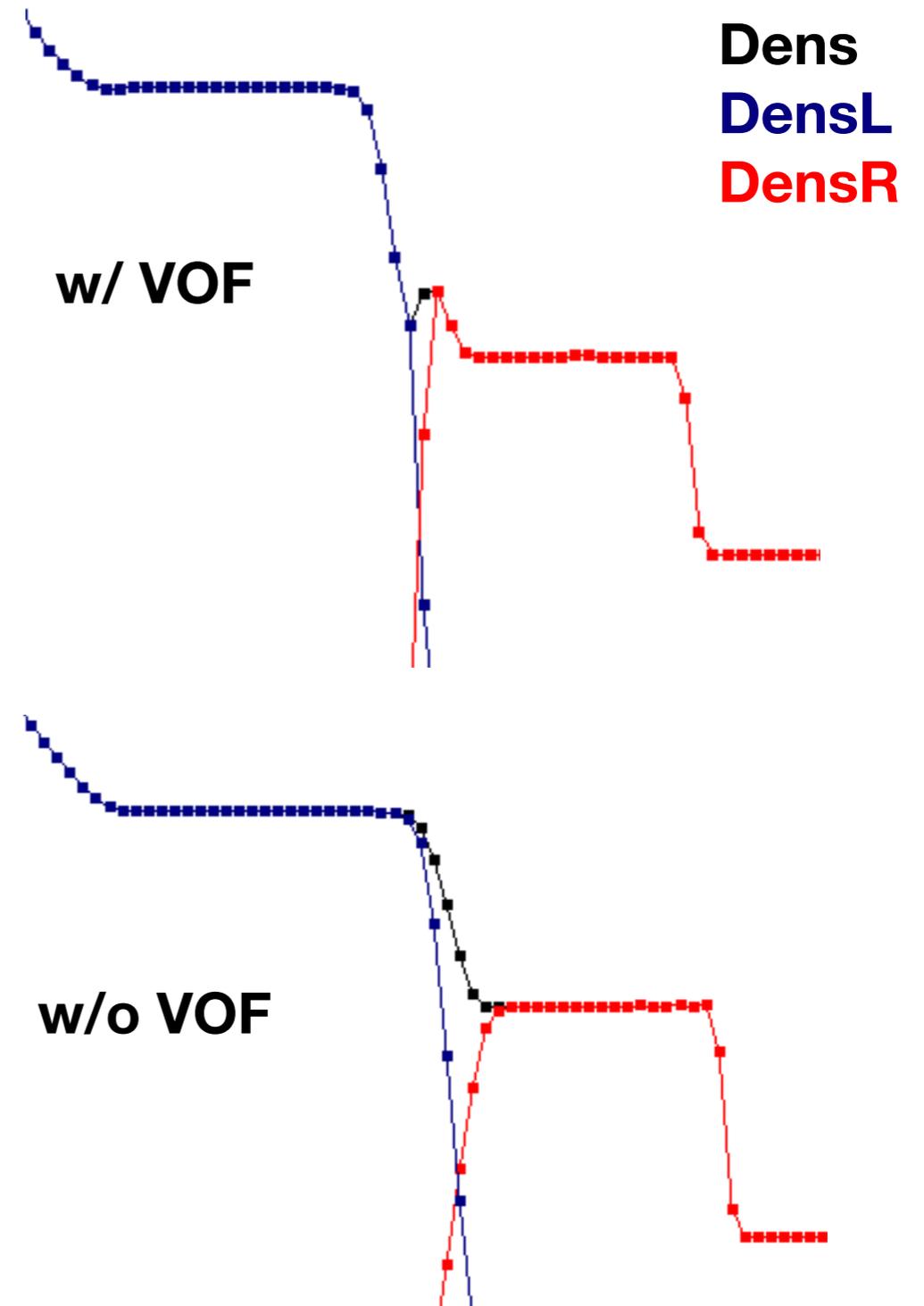
- Single-fluid hydro update gives a volume flux through cell interfaces
- VOF cuts advected volume with an interface to give flux of component volume fractions
- In 2D interfaces need to be reconstructed from neighboring volume fractions



- Sod shock tube with a jump in gamma
 - 1.5|1.4
 - Shock Speeds match analytic solution to 1D two-fluid Riemann problem
 - Mixing at material interface contained to a few cells

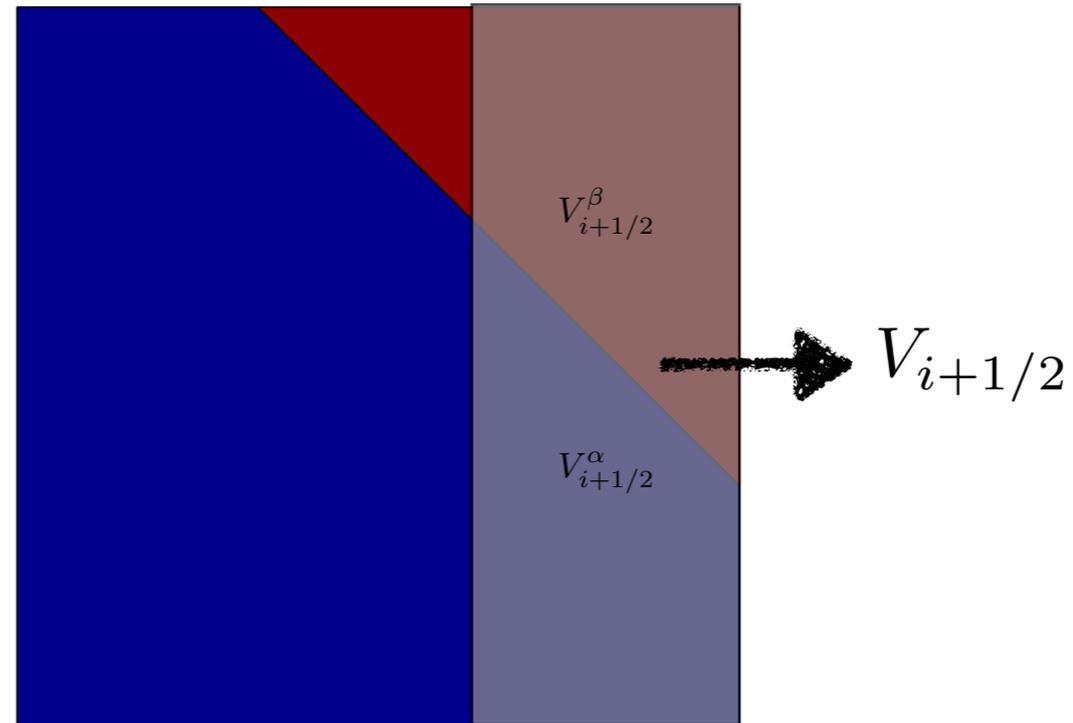


- Sod shock tube with a jump in gamma
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Piecewise Linear Interface Calculation (PLIC)

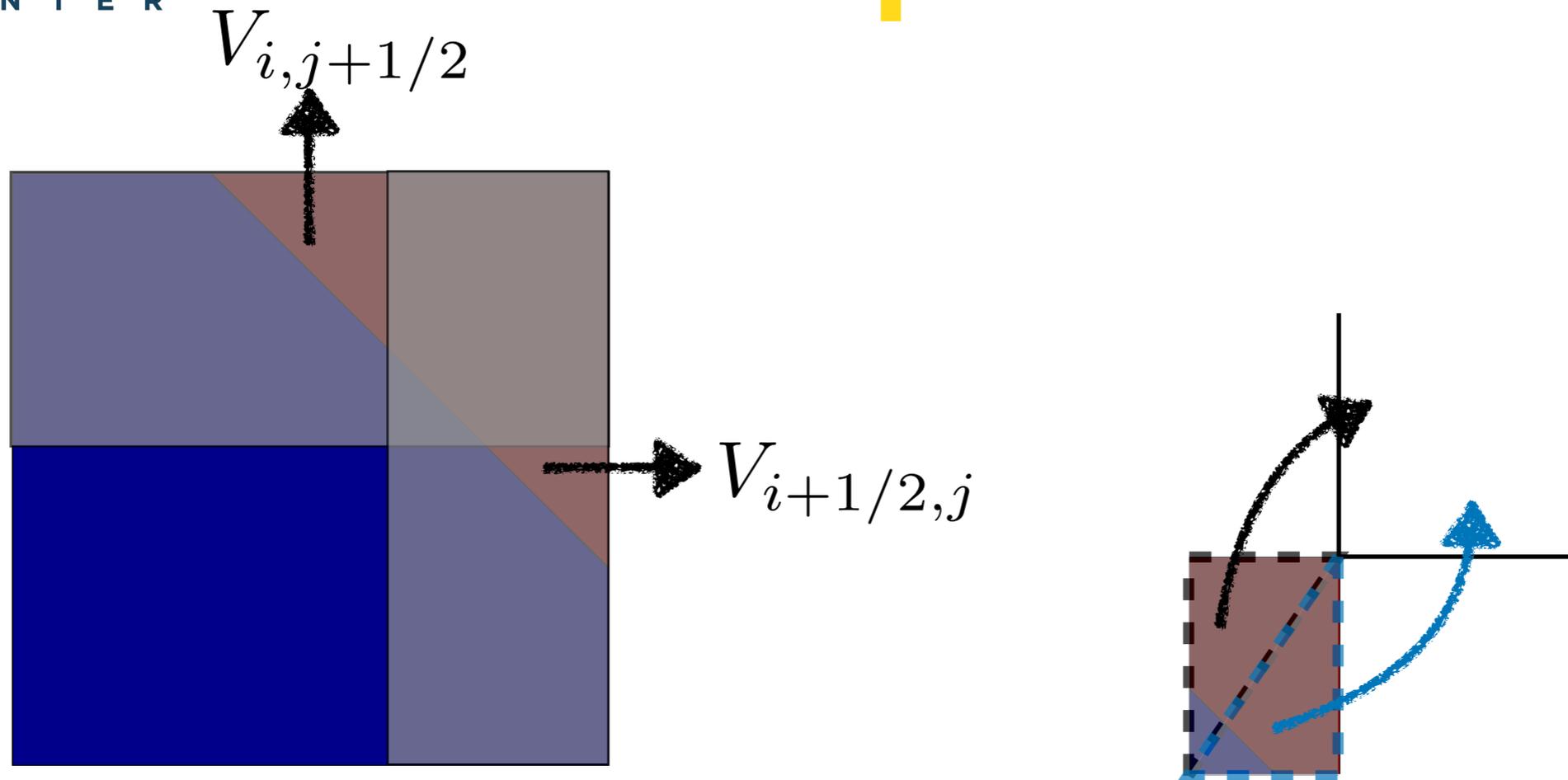
$$\mathbf{n} \cdot \mathbf{x} + \rho = 0$$



- Interface normal reconstructed as gradient of volume fraction
- Line constant fit to cell's volume fraction

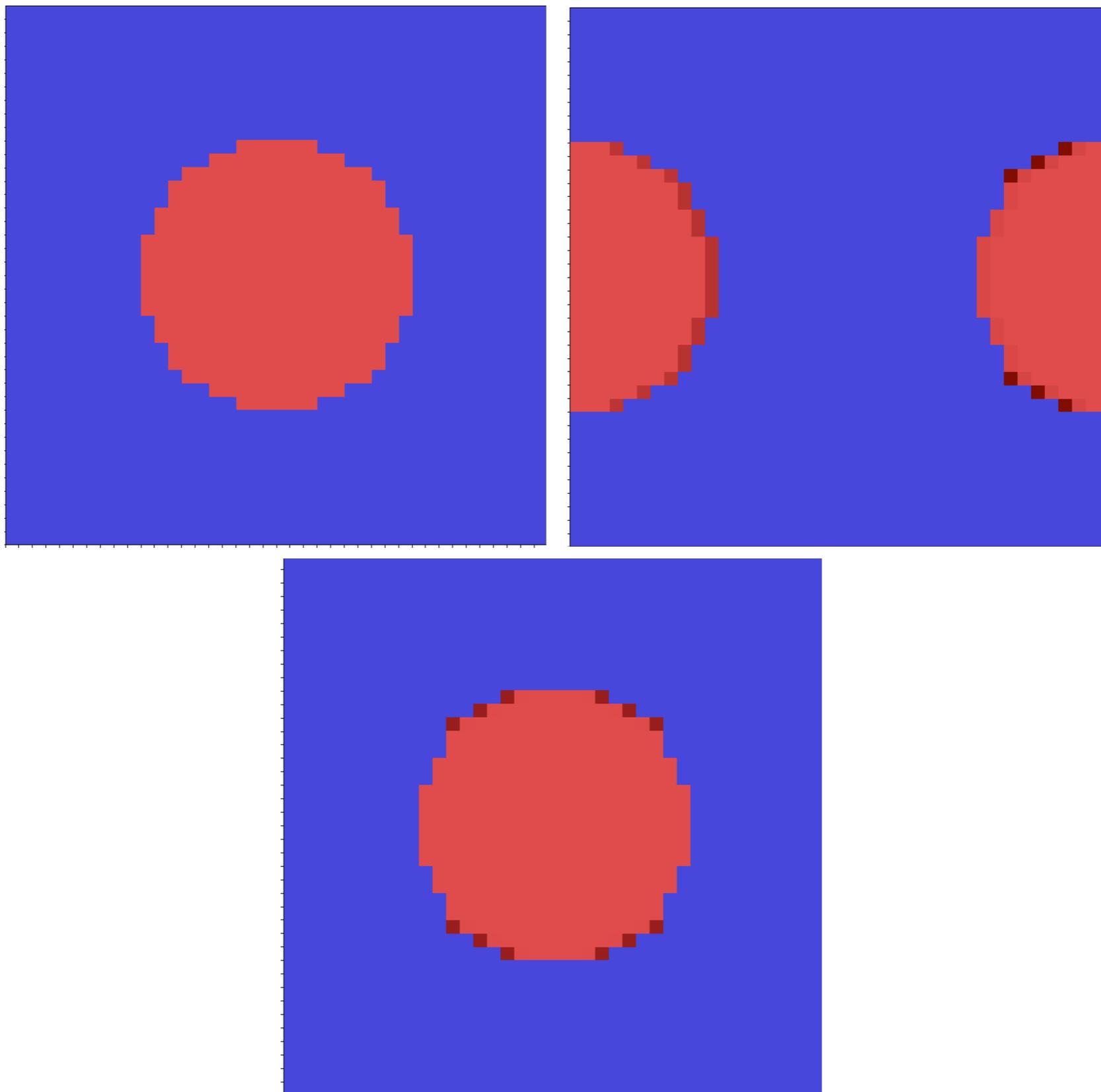
[1] W. J. Rider and D. B. Kothe, "Reconstructing Volume Tracking," *Journal of Computational Physics*, vol. 141, no. 2, pp. 112–152, Apr. 1998, doi: [10.1006/jcph.1998.5906](https://doi.org/10.1006/jcph.1998.5906).

[2] D. Youngs, "An interface tracking method for a 3D Eulerian hydrodynamics code," Jan. 1984.



- Unsplit hydro updates using x & y fluxes simultaneously
- Corner volume fluxes need to be reassigned to neighboring faces

2D Advection



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Compressible Multifluid Hydro

$$\partial_t \rho + \nabla \cdot (\rho \mathbf{u}) = 0$$

$$\partial_t (\rho \mathbf{u}) + \nabla \cdot (\rho \mathbf{u} \otimes \mathbf{u}) + \nabla P = 0$$

$$\partial_t (\rho E) + \nabla \cdot (\mathbf{u} (\rho E + P)) = 0$$

- Each component has

$$\Gamma^\alpha \equiv \frac{\rho^\alpha c_\alpha^2}{P^\alpha}$$

- Also for equivalent single fluid

$$\Gamma = \left(\sum_\alpha \frac{f^\alpha}{\Gamma^\alpha} \right)^{-1}$$

- Momentum is updated w/ single fluid fluxes
- Component density and energies are updated using single fluid fluxes weighed according to the ratio of advected volumes at the interface

$$\mathbf{F}_{i+1/2}^{\rho^\alpha} \frac{V_{i+1/2}^\alpha}{V_{i+1/2}} \mathbf{F}_{i+1/2}^\rho$$

- After update component pressures may not be in equilibrium with single fluid pressure

$$P^\alpha \neq P$$

- Adjust volume fractions, densities & energies to get to an average pressure:

$$P = \frac{\sum_\alpha f^\alpha / \Gamma^\alpha}{\sum_\alpha \frac{f^\alpha}{P^\alpha \Gamma^\alpha}}$$

$$f^\alpha = \frac{f^\alpha}{\alpha} \left(1 + \frac{P}{P^\alpha} \right)$$

$$f^\alpha = \frac{f^\alpha + f^\alpha}{f^\alpha + f^\alpha}$$

$$\rho^\alpha = \frac{f^\alpha \rho^\alpha}{f^\alpha + f^\alpha}$$

$$f^\alpha \rho^\alpha E^\alpha = \frac{f^\alpha \rho^\alpha E^\alpha}{f^\alpha + f^\alpha} + P f^\alpha$$

2D Advection

