

Non-inertial Eulerian Hydrodynamic Code for ICF Implosion Simulations

A. BOSE, R. BETTI, P.-Y. CHANG, AND J. R. DAVIES

University of Rochester, Fusion Science Center and Laboratory for Laser Energetics

Objective and Motivation

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Objective

- Develop a Eulerian hydrodynamic code in spherical geometry that solves the equations of motion of a fluid in the frame of reference of the target center of mass, then study the effects of Rayleigh–Taylor instability on the deceleration phase

Motivation

- A non-inertial frame of reference can be defined so that the imploding shell boundaries are static; a fine-mesh region can be constructed in non-inertial coordinates that covers the dense shell and accurately resolves hydrodynamic instabilities

TC10329

Coordinate transformation to a non-inertial frame is used

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Coordinate transformation:

$$\begin{aligned} x &\equiv r \\ t &\equiv t \\ \theta &\equiv \theta \end{aligned}$$

- r is the radial coordinate in spherical geometry
- $R(t)$ is a time dependent reference (e.g., the shell's center of mass)

This coordinate transformation leads to:

$$\begin{aligned} \partial_r &\equiv \frac{1}{R(t)} \partial_x \\ \partial_t &\equiv -\frac{x}{R} \partial_x + \partial_t \\ \partial_\theta &\equiv \partial_\theta \end{aligned}$$

TC10332

The polar and azimuthal components of the momentum equation have no inertial forces

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B. Polar component: a term proportional to \dot{R} is introduced as a result of the transformation

$$\partial_t(\rho v_\theta) + \frac{1}{r^2} \partial_r(r^2 \rho v_r v_\theta) + \frac{1}{r \sin \theta} \partial_\theta(\rho v_\theta^2 \sin \theta) + \frac{\rho v_\theta v_r}{r} - \frac{\rho v_\theta^2 \cot \theta}{r} = -\frac{1}{r} \partial_\theta p$$

$$\begin{aligned} \partial_t(Qw_\theta) + \frac{1}{R} \partial_x(Qw_\theta w_x) + \frac{1}{xR \sin \theta} \partial_\theta(Qw_\theta^2 \sin \theta) \\ + \frac{Qw_\theta w_x}{xR} - \frac{Qw_\theta^2 \cot \theta}{xR} - xR^2 \partial_\theta p - \frac{QRw_\theta}{R} \end{aligned}$$

C. Azimuthal component: if $v_\phi = w_\phi = 0$, then this equation does not contribute and the system is reduced to 2-D geometry

TC10335

The benefits from the new center-of-mass frame of reference include a static grid, allowing high resolution when needed

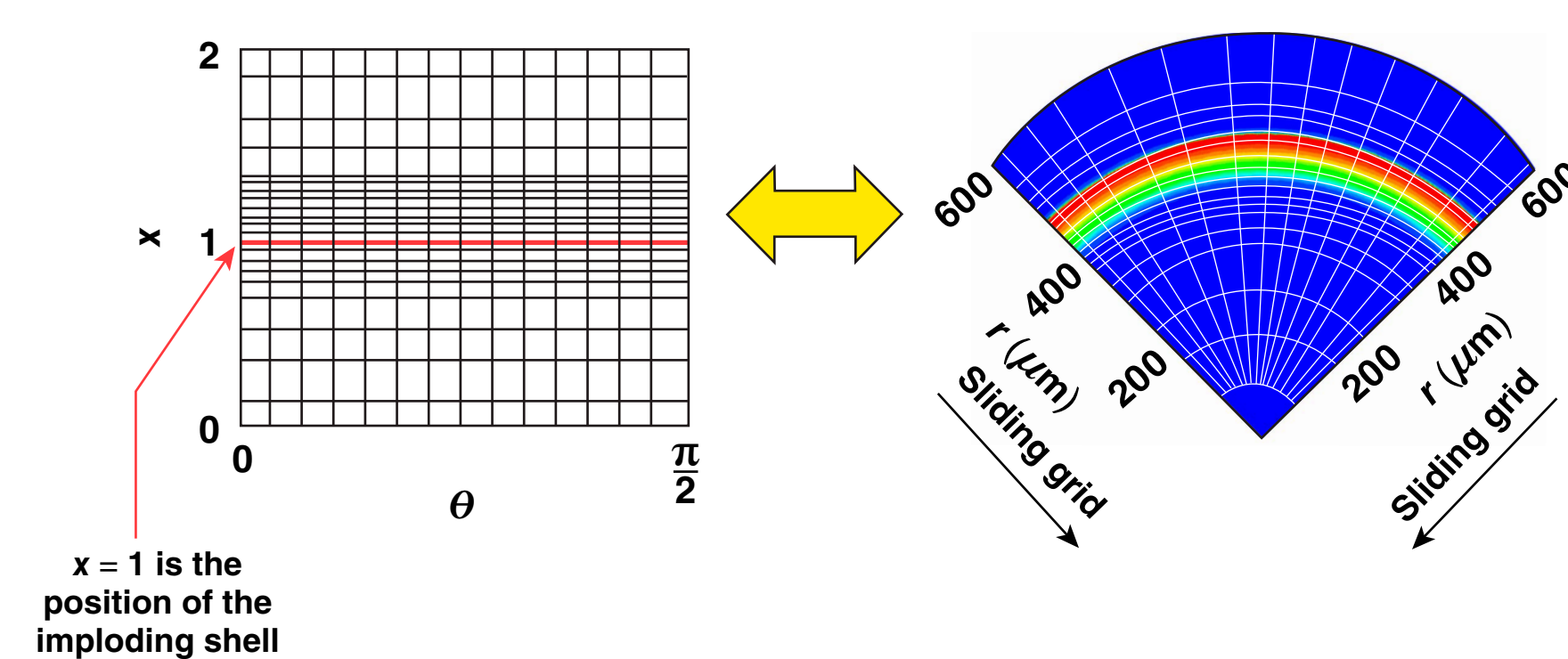
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- Defining $R(t)$ to be the position of the center of mass of the shell at time t . In non-inertial coordinates, $x = 1$ is always the location of the center of mass
- The sharp density gradients occur at the shell boundaries that would be around $x = 1$. Therefore, the finer mesh would be static around this region
- The center of the system is $r = 0$, which is mapped to $x = 0$ and is always fixed
- As $R(t)$ changes with time the coordinates are rescaled. Since $R(t)$ decreases, the new coordinate allows automatic zooming to the region between the origin and the center of mass
- \dot{R} and \ddot{R} are the velocity and acceleration of center of mass, respectively

TC10340

A non-inertial frame of reference is equivalent to a moving grid with high resolution in the region including the imploding shell

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Static grid in non-inertial coordinates.

A grid moving with the imploding shell.

TC10330

The continuity equation requires redefining the density, in transformed coordinates

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$$\partial_t \rho + \nabla \cdot (\rho \vec{v}) = 0$$

In spherical polar coordinates, assuming azimuthal symmetry

$$\partial_t \rho + \frac{1}{r} \partial_r(r^2 \rho v_r) + \frac{1}{r \sin \theta} \partial_\theta(\rho v_\theta \sin \theta) = 0$$

In new coordinates:

$$\partial_t Q + \frac{1}{R} \partial_x(Qw_x) + \frac{1}{xR \sin \theta} \partial_\theta(Qw_\theta \sin \theta) = 0$$

With new variables in non-inertial coordinates

$$\begin{aligned} Q &= x^2 R^3 \rho && \text{Redefined density parameter} \\ w_x &= v_r - \dot{R}x \\ w_\theta &= v_\theta \\ w_\phi &= v_\phi \end{aligned}$$

TC10333

The energy equation is written in a conserved-Eulerian form with a redefined total energy ξ

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Assuming ideal gas EOS,

$$\partial_t \left(\frac{p}{\gamma - 1} + \frac{\rho v^2}{2} \right) + \nabla \cdot \left(\frac{\gamma p}{\gamma - 1} + \frac{\rho v^2}{2} \right) = 0$$

In new coordinates,

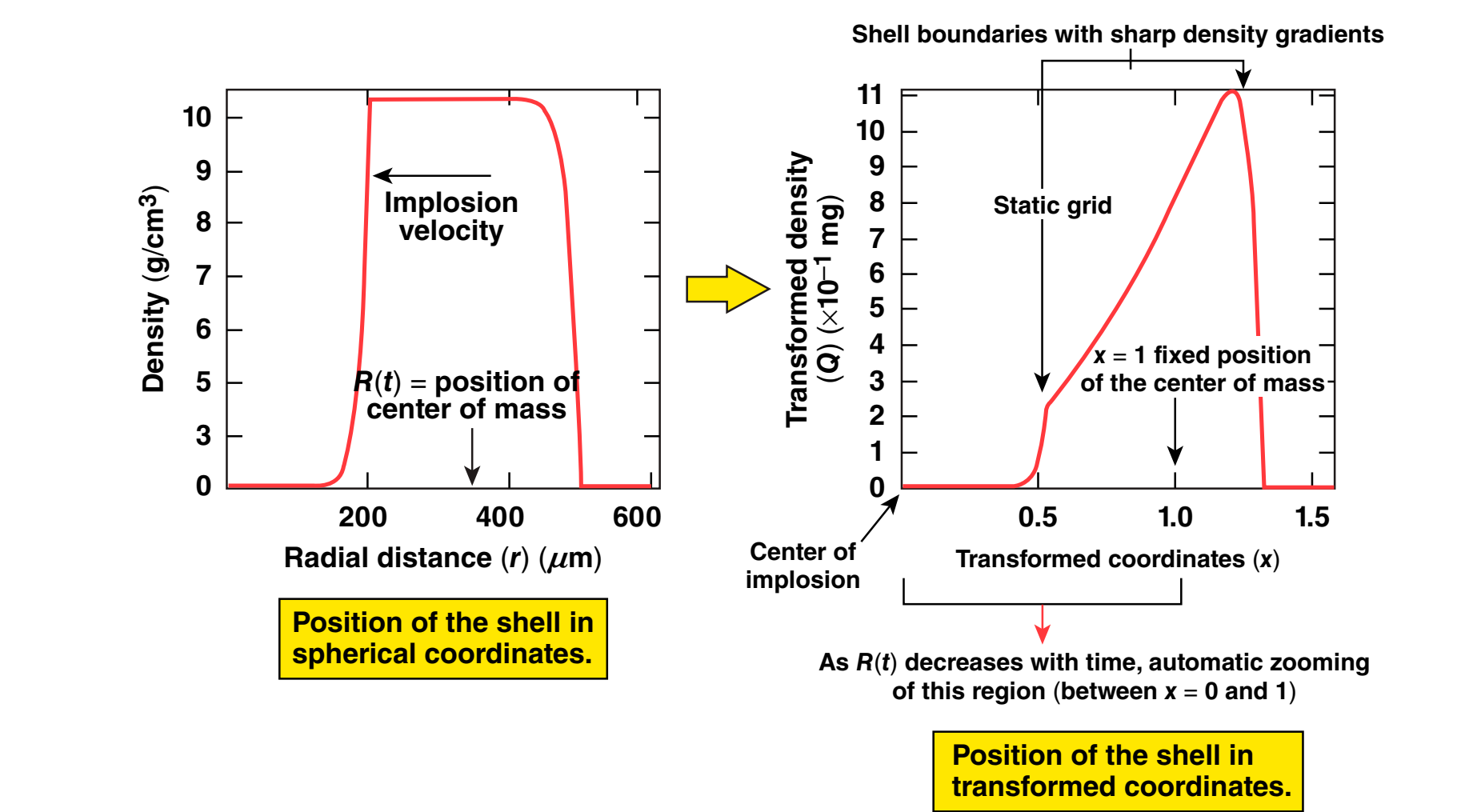
$$\begin{aligned} \partial_t \xi + \frac{1}{R} \partial_x(\xi w_x) + \frac{1}{xR \sin \theta} \partial_\theta(\xi w_\theta \sin \theta) \\ = -\frac{1}{R} \partial_x \left(\frac{Qpw_x}{\rho} \right) - \frac{1}{xR \sin \theta} \partial_\theta \left(\frac{Qpw_\theta \sin \theta}{\rho} \right) - \frac{\dot{R}}{R} \partial_x \left(\frac{Qpx}{\rho} \right) \end{aligned}$$

$$\begin{aligned} \text{with total energy } \xi &= \left[\frac{Qp}{\rho(\gamma - 1)} + \frac{Qw^2}{2} \right] \\ \text{using } w^2 &= (w_x + x\dot{R})^2 + w_\theta^2 + w_\phi^2 \end{aligned}$$

TC10336

The transformed density shown in non-inertial coordinates using a static grid

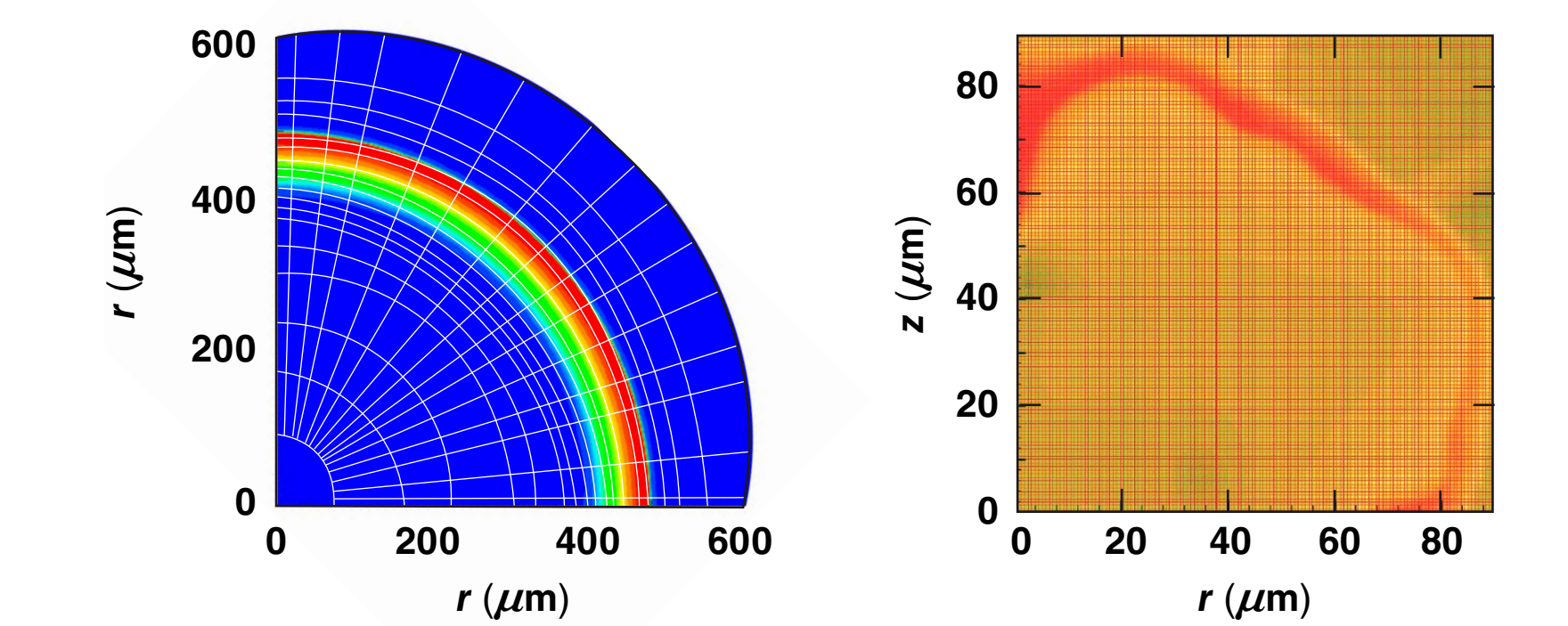
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The code makes use of spherical geometry which allows accurate positioning of the fine mesh region on the imploding shell unlike in cylindrical coordinates

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In spherical geometry the fine-mesh can be applied to the shell even at early stages of the implosion when the shell radius is larger.

In cylindrical geometry the fine-mesh is practically applicable only to the stagnation phase.

TC10331

*K. Anderson et al., Bull. Am. Phys. Soc. 46, 280 (2001).

The momentum equation has pseudo-force terms in non-inertial coordinates

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$$\partial_t(\rho \vec{v}) + \nabla \cdot (\rho \vec{v} \vec{v}) = -\nabla p$$

A. Radial equation:

In spherical coordinates

$$\partial_t(\rho v_r) + \frac{1}{r^2} \partial_r(r^2 \rho v_r v_r) + \frac{1}{r \sin \theta} \partial_\theta(\rho v_\theta v_r \sin \theta) - \frac{\rho(v_\theta^2 + v_\phi^2)}{r} = -\partial_r p$$

Transformed equation:

$$\begin{aligned} \partial_t(Qw_x) + \frac{1}{R} \partial_x(Qw_x^2) + \frac{1}{xR \sin \theta} \partial_\theta(Qw_x w_\theta \sin \theta) - \frac{Q}{xR} (w_\theta^2 + w_\phi^2) \\ = -x^2 R^2 \partial_x p - Q \left(x\dot{R} + \frac{w_x \dot{R}}{R} \right) \end{aligned}$$

Inertial forces

TC10334

The hydrodynamic equations are summarized for a 1-D non-inertial Eulerian frame

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Transformed parameters in 1-D

$$\begin{cases} Q = x^2 R^3 \rho \\ \xi = \left[\frac{Qp}{\rho(\gamma - 1)} + \frac{Qw^2}{2} \right] \\ w_x = v_r - \dot{R}x \\ w_\theta = v_\theta \\ w_\phi = v_\phi \\ w^2 = (w_x + x\dot{R})^2 + w_\theta^2 + w_\phi^2 \end{cases}$$

Transformed hydrodynamic equations

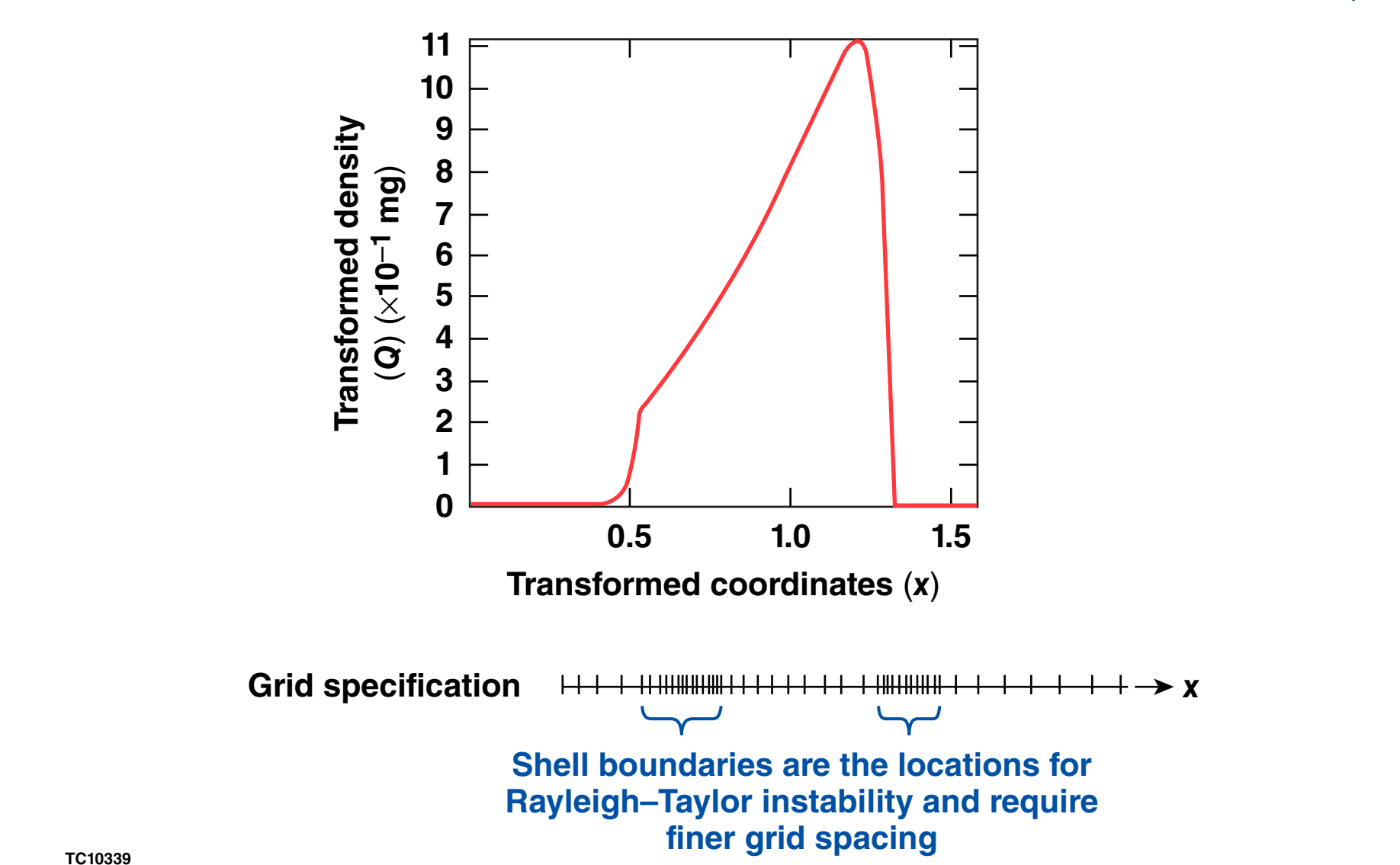
$$\begin{aligned} \partial_t Q + \frac{1}{R} \partial_x(Qw_x) &= 0 \\ \partial_t(Qw_x) + \frac{1}{R} \partial_x(Qw_x^2) &= -x^2 R^2 \partial_x p - Q \left(x\dot{R} + \frac{w_x \dot{R}}{R} \right) \\ \partial_t \xi + \frac{1}{R} \partial_x(\xi w_x) &= -\frac{1}{R} \partial_x \left(\frac{Qpw_x}{\rho} \right) - \frac{\dot{R}}{R} \partial_x \left(\frac{Qpx}{\rho} \right) \\ p &= \rho T / A \quad A = m_i / (1 + Z) \end{aligned}$$

These are the closed set of equations used to develop the 1-D non-inertial Eulerian hydrodynamic code to facilitate comparison with existing Lagrangian and Eulerian codes.

TC10337

Regions with sharp density gradients are static in non-inertial coordinates

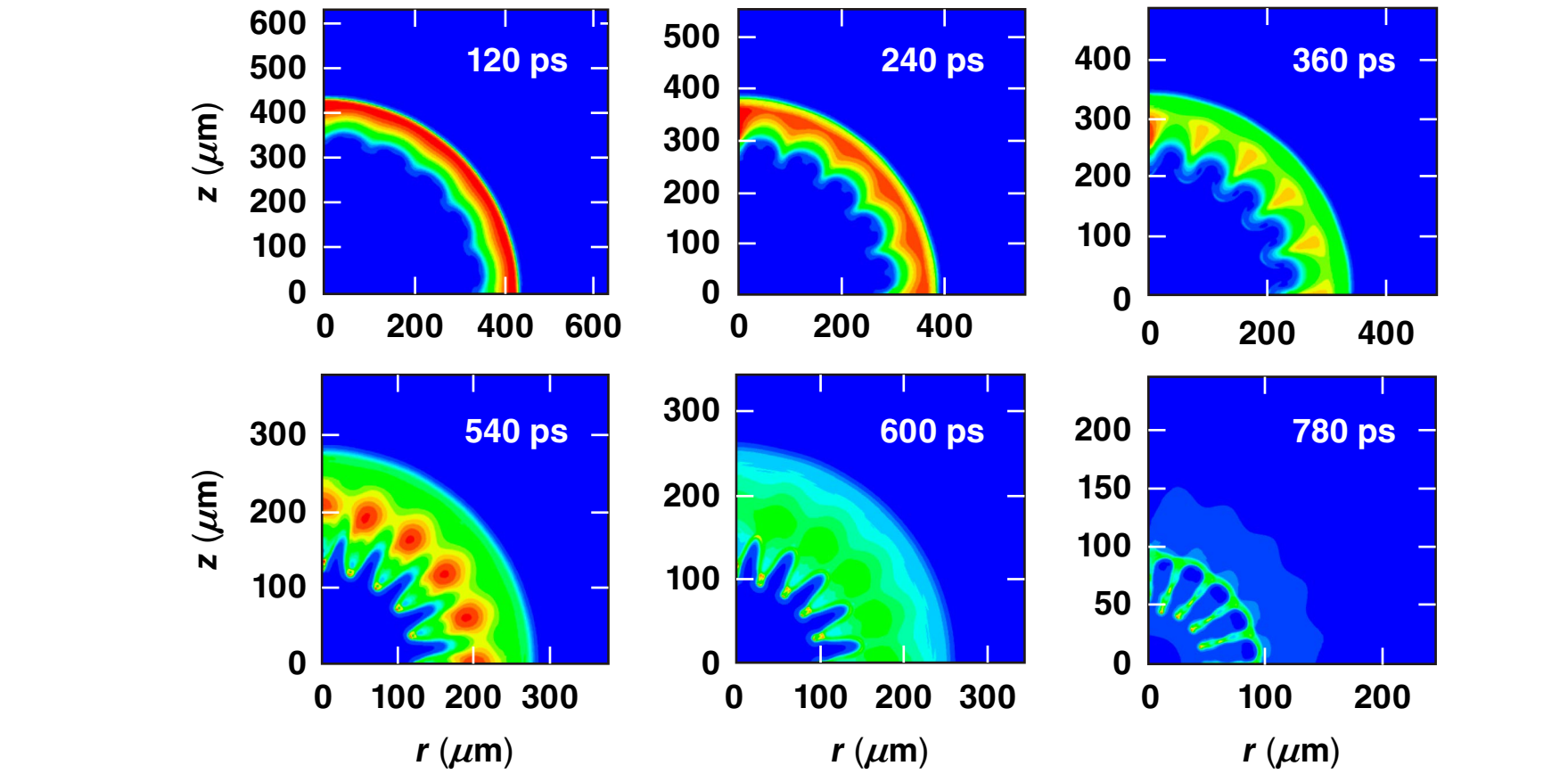
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TC10339

Simulations of the deceleration phase showing single-mode Rayleigh–Taylor growth in cylindrical non-inertial coordinates

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Cylindrical non-inertial transformation $\alpha = \frac{r}{R(t)}$, $\beta = \frac{z}{R(t)}$

TC10341

*K. Anderson et al., Bull. Am. Phys. Soc. 46, 280 (2001).

Conclusion

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- The accelerated coordinate system allows the use of a static Eulerian grid
- The new coordinates result in automatic zooming of the region between the origin and the center of mass
- In the new-coordinate system, the sharp density gradients at the shell boundaries are pinned around the center of mass, therefore specifying the location of fine mesh region. As a result the sharp density gradients at the shell boundaries are not missed

TC10342