#### **Preparing for Polar Drive** at the National Ignition Facility



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# Polar drive provides a viable alternative for hot-spot ignition on the NIF

- A 2-D polar-drive design gives a gain of 32 with NIF-specific target and laser nonuniformities
- UV beam smoothing includes polarization smoothing and Multi-FM 1-D smoothing by spectral dispersion (SSD)
- SSD smoothing is required only during the picket pulses
- Polar-drive experiments on OMEGA and NIF have addressed several aspects of PD including adiabat, symmetry, and drive
- One-dimensional, Multi-FM single-beam smoothing is being tested on OMEGA EP

Implementation of polar drive for ignition on the NIF requires modest additional capabilities.



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#### Outline



- The polar-drive point design
- Sensitivity analysis of the polar-drive point design
- Recent experiments on OMEGA
   and the NIF

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### In polar drive, the four NIF beam cones per hemisphere are repointed to three regions on the target



### Repointing corresponds to a lateral translation of the beam in the target plane



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- Oblique irradiation near the equator is at lower densities, causing
  - reduced absorption
  - reduced hydrodynamic efficiency
  - lateral heat flow

TC9696

#### A multiple-picket, multiple-shock laser pulse is used to shape the adiabat



- This is based on a triple-picket design\* that achieved an areal density of 300 mg/cm<sup>2\*\*</sup> in OMEGA experiments
- Individual pulses lie within NIF limits for energy (9.3 kJ/beam) and power (~2.3 TW/beam peak power)

<sup>\*</sup>V. N. Goncharov et al., Phys. Rev. Lett. <u>104</u>, 165001 (2010).

<sup>\*\*</sup>T. C. Sangster et al., Phys. Plasmas <u>17</u>, 056312 (2010).

# The triple-picket polar-drive-ignition design was optimized in 1-D with the optimizer *Telios*

- Telios is a C++ implementation of a downhill simplex method used to diagnose and generate 1-D designs
- The pulse and target design are varied, maximizing the gain while remaining within laser-damage limits
- This method allows for tuning more variables than would be feasible by hand (e.g., 12+)
- This design has an ITF<sub>1-D</sub> = 4.6, where the ITF<sub>1-D</sub> is the ratio of the capsule kinetic energy to the minimum needed for ignition\*



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A simplex on a topographical map optimizing for maximum height

<sup>\*</sup>S. W. Haan et al., Phys. Plasmas <u>18</u>, 051001 (2011).

### The picket pulses are followed by a rapid-rise drive pulse

- Picket pulses are readily tuned experimentally\*
- Multiple pickets provide greater adiabat shaping and decreased shell instability\*\*
- Subsequent pickets must have diminishing spacing, limiting the number of pickets\*\*\*
- The 2-D gain is insensitive to minimum power between the third picket and step pulse below 0.1 TW/beam



<sup>\*</sup>T. R. Boehly et al., Phys. Plasmas <u>16</u>, 056302 (2009).

<sup>\*\*</sup>K. S. Anderson and R. Betti, Phys. Plasmas <u>11</u>, 5 (2004).

<sup>\*\*\*</sup>V. N. Goncharov et al., Phys. Rev. Lett. <u>104</u>, 165001 (2010).

# The equatorial beam coupling is increased using tailored phase plates



- Nearly Gaussian spots are more center peaked than higher-order spots, offering greater control of the energy deposition on the target
- The equatorial spot shape further combines a round spot with an elliptical spot to mitigate loss of coupling near the equator
- All spots are further enveloped with a high-order super-Gaussian centered on the target

# Multi-FM SSD beam smoothing and polarization smoothing are used to reduce single-beam nonuniformities

- Multi-FM 1-D SSD\* employs technology developed for the telecommunications industry
  - microwave phase modulators and drive electronics (~20 to 40 GHz)
  - an effective UV bandwidth of 500 GHz
  - a divergence of 100- $\mu$ rad half angle at full beam width
- Multi-FM uses a three-modulator configuration that achieves high gain in polar-drive simulations
- Polarization smoothing is also included to reduce single-beam nonuniformities



\*J. A. Marozas, J. D. Zuegel, and T. J. B. Collins, Bull. Am. Phys. Soc. <u>55</u>, 294 (2010). LLE Review Quarterly Report <u>114</u>, 73 (2008).

## Imprint mitigation with Multi-FM is comparable to that of 2-D SSD

• With single-modulator SSD the target fails to ignite; with Multi-FM or 2-D SSD it achieves full gain



At the end of the acceleration phase: 9.8 ns

# An ~10- $\mu$ m-amplitude ice-layer "shim" is used to lower the equatorial mass and reduce the laser energy required to drive the equator



- This perturbation may be introduced by shimming the cryogenic layering sphere itself or adding an IR source around the equator
- A 10- $\mu$ m shim allows for a ~10% reduction in equatorial beam power, allowing greater overall power while remaining below laser-damage thresholds
- Alternately, shimming permits lower equatorial intensities, reducing plasma instabilities
- When the shim is removed and the design scaled to 1.4 MJ and retuned, the gain with nonuniformities is reduced by 20%

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### The polar-drive design with target and beam nonuniformities and Multi-FM beam smoothing achieves a gain of 32

- Simulations use flux-limited thermal transport with a 6% flux limiter
- Initial gas density = 0.225 mg/cm<sup>3</sup>
- The sum of the outer- and inner-rms surface perturbations is only 25% of the shell thickness at the start of shell deceleration

Energy	1.52 MJ
Gain	32
V <sub>imp</sub> *	432 <i>µ</i> m/ns
IFAR <sub>2/3</sub>	36
In-flight $\alpha^{**}$	3
Convergence ratio	23
Peak $ ho R$	1.42 g/cm <sup>2</sup>

$$FAR_{2/3} = \frac{R}{\Delta R}$$
 at  $R = 2/3R_0$ 

 $V_{\rm imp} = (2E_{\rm kin}/M)^{1/2}$ 

\*\*At peak shell speed



# The polar-drive design has been simulated with all relevant sources of implosion nonuniformity

Nonuniformities (NIF specification)	
Target	Surface roughness (115 nm rms)
	lce roughness (1- $\mu$ m rms)
Single beam	Imprint
Multibeam	Power imbalance (8%)
	Beam mistiming (30 ps)
	Beam mispointing (50 $\mu$ m)

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• Single-beam nonuniformities are modeled including polarization smoothing

# Experiments and simulations are planned to investigate further aspects of this design



Hydrodynamics	This design will be simulated in 3-D using HYDRA
Energetics	<ul> <li>Nonlocal thermal transport using a modified Schurtz algorithm<sup>1</sup> has been implemented in <i>DRACO</i></li> <li>A crossed-beam energy transfer (CBET) model is being implemented in <i>DRACO</i><sup>2</sup></li> <li>Experiments on OMEGA suggest that CBET may be mitigated using beams that underfill the target<sup>3</sup></li> </ul>
Preheat	A possible mitigation strategy for two-plasmon decay is given by experiments on OMEGA that found decreased hard x-ray signals with Si- and Ge doped targets <sup>4</sup>

• Cryogenic PD experiments of relevant targets will be performed on OMEGA

<sup>3</sup>See I. V. Igumenshchev, YI3.00001.

<sup>4</sup>P. B. Radha et al., Bull. Am. Phys. Soc. <u>52</u>, 143 (2007).

<sup>&</sup>lt;sup>1</sup>Ph. D. Nocolaï, J.-L. A. Feugeas, and G. P. Schurtz, Phys. Plasmas <u>13</u>, 032701 (2006).

<sup>&</sup>lt;sup>2</sup>See J. A. Marozas, PO8.00003.

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### Simulations show little gain reduction when Multi-FM SSD is active for only the first picket\*

• Splicing in a separate pulse for the pickets means the drive pulse can operate with less bandwidth

- Motivation: using only native single-modulator SSD during the drive pulse reduces the risk of damage to the laser
- Single-beam smoothing asymptotes on 1-ns time scales\*\*



<sup>\*</sup>P. W. McKenty et al., Bull. Am. Phys. Soc. <u>51</u>, 295 (2006).

<sup>\*\*</sup>J. A. Marozas, presented at the International Workshop on ICF Shock Ignition, Rochester, NY, 8–10 March 2011. TC9706

#### Target performance is sensitive to positioning but less sensitive to ice roughness



- Simulations indicate that an offset of ~20  $\mu$ m is tolerated
- An ice-roughness power-law spectrum  $\sim\!\!\ell^{-1}$  is used, not including the shim, based on shadowgraphy measurements
- This design tolerates an ice roughness of over 2- $\mu$ m rms

#### The target is insensitive to mispointing and mistiming errors within the NIF specifications

 Pulse mistiming primarily impairs target performance caused by largeamplitude, low-mode illumination perturbations during the rise and fall of the pickets and drive pulse\*



<sup>\*</sup>R. Epstein et al., Bull. Am. Phys. Soc. 50, 114 (2005).

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### The target gain is sensitive to the initial target temperature

- The NIF specification is 18±0.5 K
- As the target warms, it pauses at the triple point (19.8 K) because of the phase change in DT
- Operating at the triple point reduces the 2-D target gain by 60%



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### Polar-drive experiments on OMEGA have addressed several aspects including adiabat, symmetry, and drive\*

- Low-adiabat pulses were used to drive high-convergence implosions of warm plastic shells
- Simulated equatorial shock speeds are within 5% of those measured by VISAR
- Backlit images of the compressed shells are in good agreement with simulated morphology



\*P. B. Radha et al., presented at the 7th International Conference on Inertial Fusion Sciences and Applications, Bordeaux, France, 12–16 September 2011. See F. Marshall. PO8.00007: P. B. Radha. PO8.00008.

### Areal densities up to 125 mg/cm<sup>2</sup> were recently demonstrated in polar drive implosions on OMEGA\*



 Higher areal density is obtained by eliminating shell coasting after the laser drive is off

See F. Marshall, PO8.00007; P. B. Radha, PO8.00008. \*P. B. Radha et al., presented at the 7th International Conference on Inertial Fusion Sciences and Applications, Bordeaux, France, 12–16 September 2011. \*\*F. J. Marshall et al., Phys. Rev. Lett. <u>102</u>, 185004 (2009).

# Exploding-pusher neutronics calibration experiments are providing a first test of polar drive on the NIF\*

- The first NIF PD DT shot was taken on 17 September 2010
- The observed scattered  $3\omega$  light\*\* was 34 mJ/cm<sup>2</sup> as measured by backscatter plates and the flux predicted by SAGE was 31 mJ/cm<sup>2</sup>

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- Gated x-ray images of shot N100917 show a circular stagnating glass shell
- Neutron yields for 1.5-mm-diam targets have been within 10% of projections



\* P. W. McKenty *et al.*, presented at the 7th International Conference on Inertial Fusion Sciences and Applications, Bordeaux, France, 12–16 September 2011.

<sup>\*\*</sup> See R. S. Craxton, UO8.00001

#### Implementing polar drive requires five additional capabilities on the NIF for an ignition demonstration



### Polar drive provides a viable alternative for hot-spot ignition on the NIF

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#### Multi-FM SSD will be tested on OMEGA EP\*

- A thin CH foil will be driven with 2.2 J in 3 ns
- The perturbation growth will be diagnosed with through-foil radiography, and the trajectory with side-on radiography
- Multi-FM SSD will be applied from the start of the pulse to up to 500 ps
- The duration of the smoothing will be varied, to test the use of \_\_\_\_?



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# Lower super-Gaussian beam-shape orders offer greater control of the energy density on the target



 Less energy is spilled over the horizon when lower super-Gaussian-order beams are repointed

### Independent ring pulse shapes are used to compensate for variations in the angle of incidence

- The equatorial rings are driven at a higher power than the other rings
- The mid-latitude rings must be lowered because of beam overlap
- The polar ring power is raised for the same reason
- Pickets and drive pulse require different relative ring powers; using ring pulse shapes that are multiples of each other reduces this target's gain by 40% because of the prominent P<sub>4</sub>



### Target performance shows a \_\_% reduction in gain when the spot size is reduced by 20%

- Use of underfilling spots has been proposed to reduce the effects of crossed-beam energy transfer\*
- When DPP spots are reduced by 20%, the gain is \_

<sup>\*</sup>I. V. Igumenshchev *et al.*, Phys. Plasmas <u>17</u>, 122708 (2010).