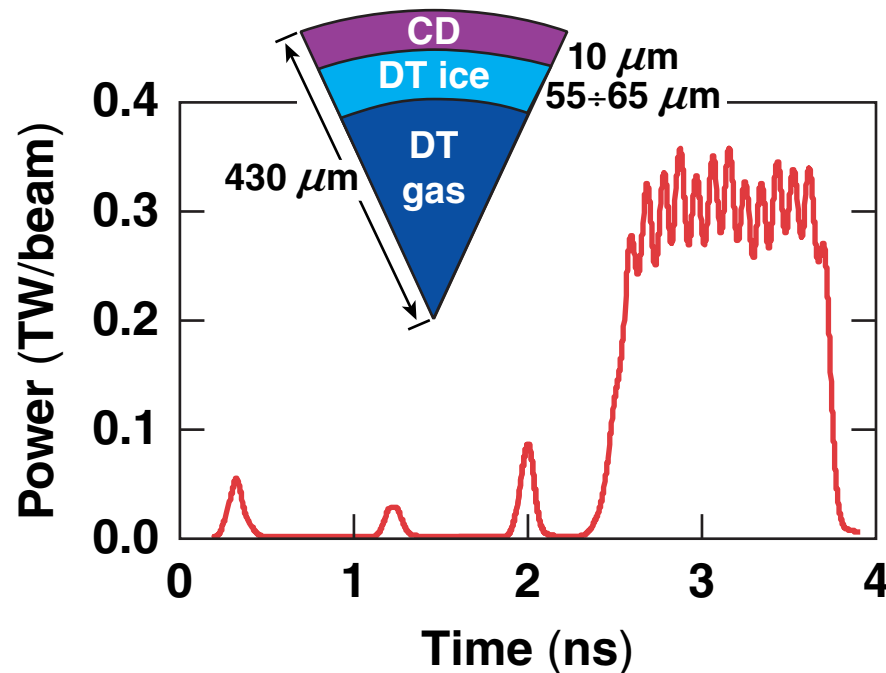


# Multiple-Picket Cryogenic Target Designs and Performance for OMEGA and the NIF



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## Summary

# Cryogenic low-adiabat, multiple-picket designs on OMEGA achieve areal densities above 85% of predicted values



- Multiple-picket designs are used to facilitate shock tuning
- Picket energies and step intensity in the main drive are adjusted to match the predictions
- High areal densities up to  $\sim 300 \text{ mg/cm}^2$  in cryogenic-DT-fuel compression have been achieved in designs with an implosion velocity  $\sim 3 \times 10^7 \text{ cm/s}$  driven at peak intensity  $\sim 8 \times 10^{14} \text{ W/cm}^2$

# Collaborators

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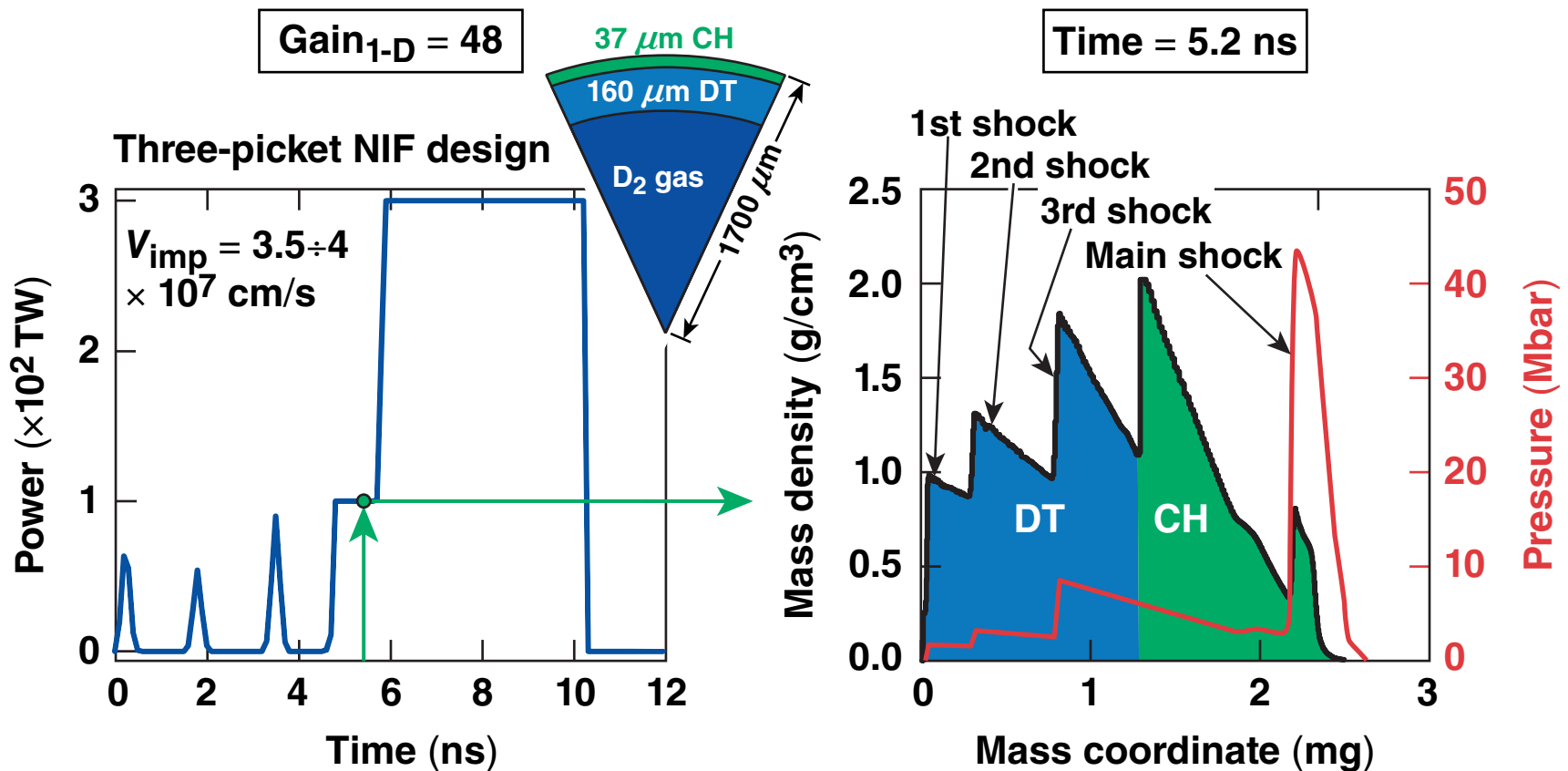
**T. C. Sangster, T. R. Boehly, S. Hu, R. L. McCrory,  
P. W. McKenty, D. D. Meyerhofer, P. B. Radha, W. Seka,  
S. Skupsky, and C. Stoeckl**

**University of Rochester  
Laboratory for Laser Energetics**

**J. A. Frenje, D. Casey, R. D. Petrasso, and C. K. Li**

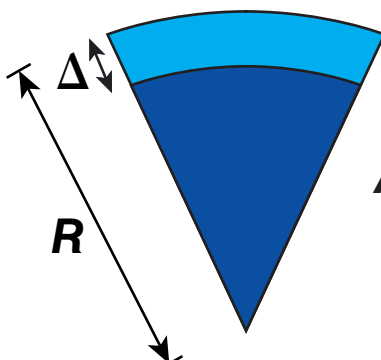
**Plasma Science and Fusion Center  
Massachusetts Institute of Technology**

# A new NIF ignition design uses three pickets to optimize shock tuning



# A step in the main drive is essential for low-adiabat, high-implosion-velocity designs

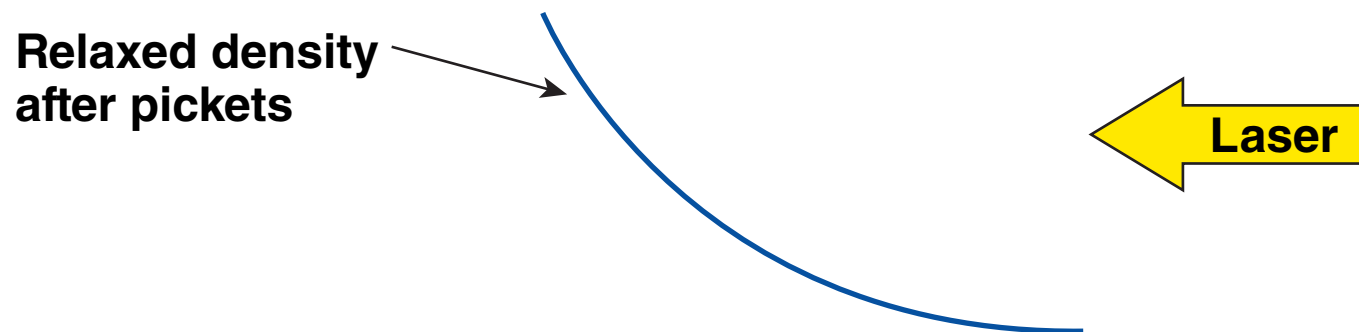
Drive pressure must exceed 100 Mbar

- Shell stability: 

$$A_{in} = \frac{R}{\Delta} \approx 60 \left( \frac{V_{imp}}{3 \times 10^7} \right)^2 \left( \frac{p_{Mbar}}{100} \right)^{-2/5} \alpha^{-3/5}$$

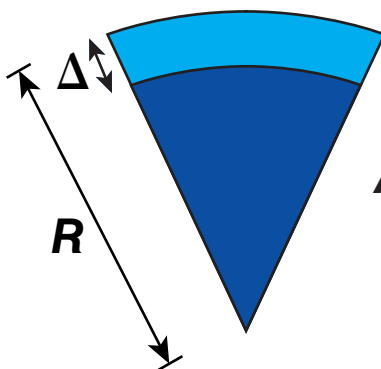
C. D. Zhou and R. Betti, Phys. Plasmas 14, 072703 (2007).

- Pressure of main shock increases as it propagates through the shell



# A step in the main drive is essential for low-adiabat, high-implosion-velocity designs

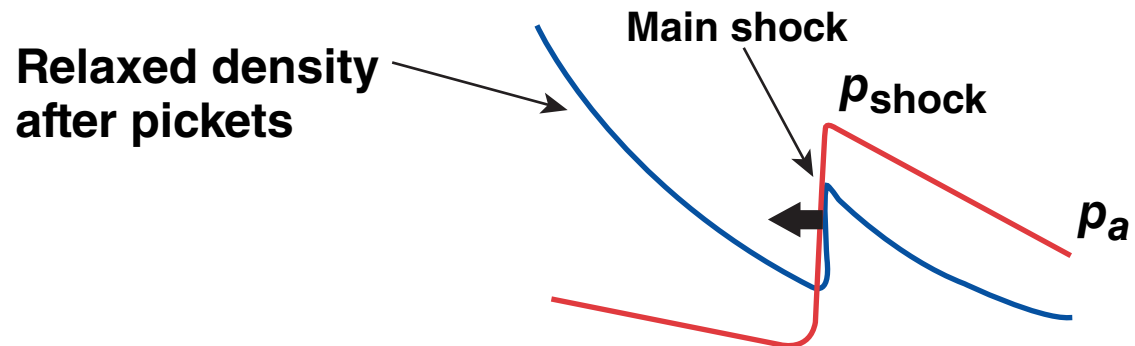
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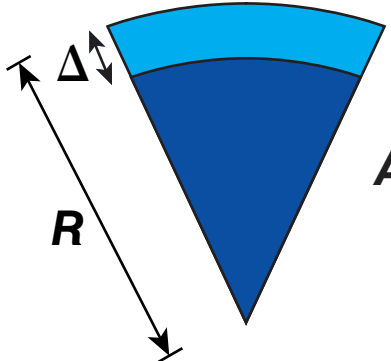
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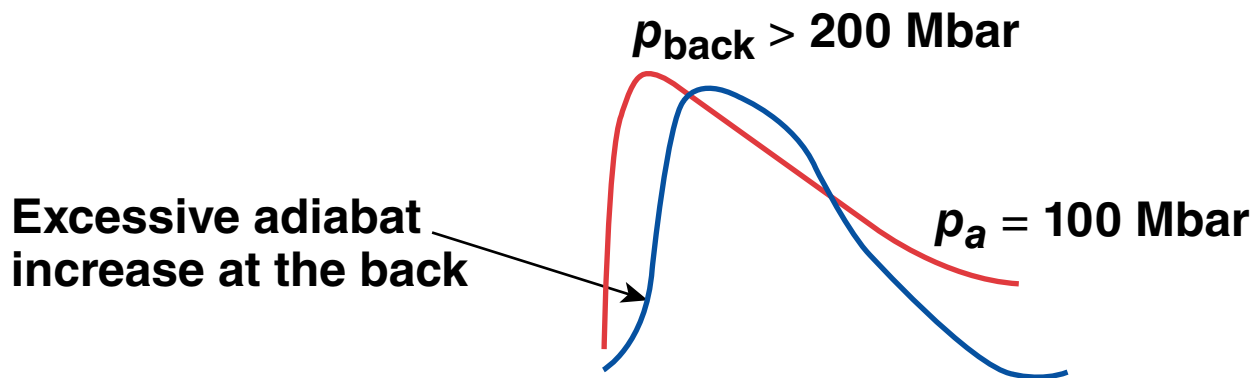
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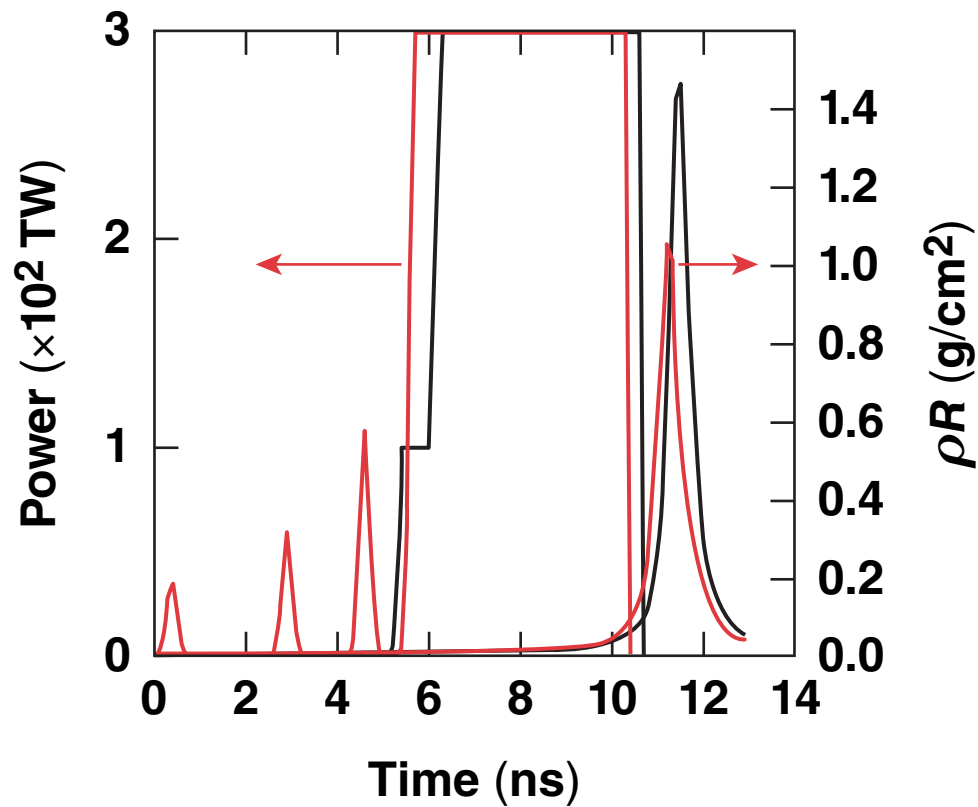
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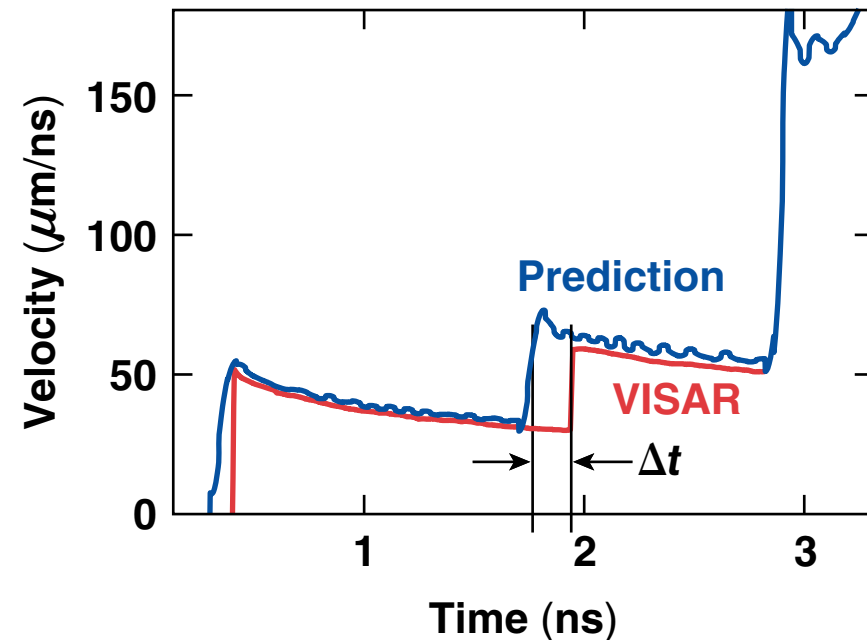
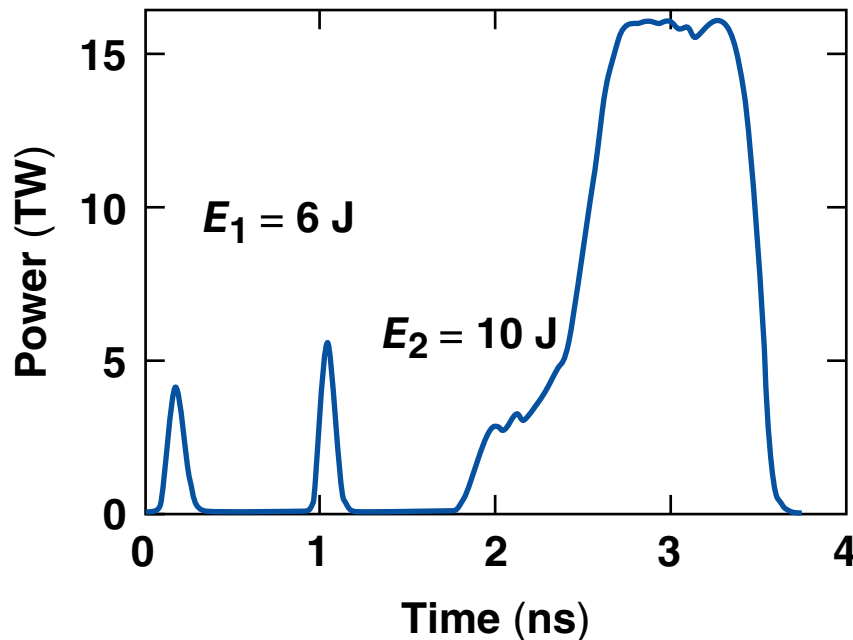


# Reducing the main shock strength leads to higher areal densities



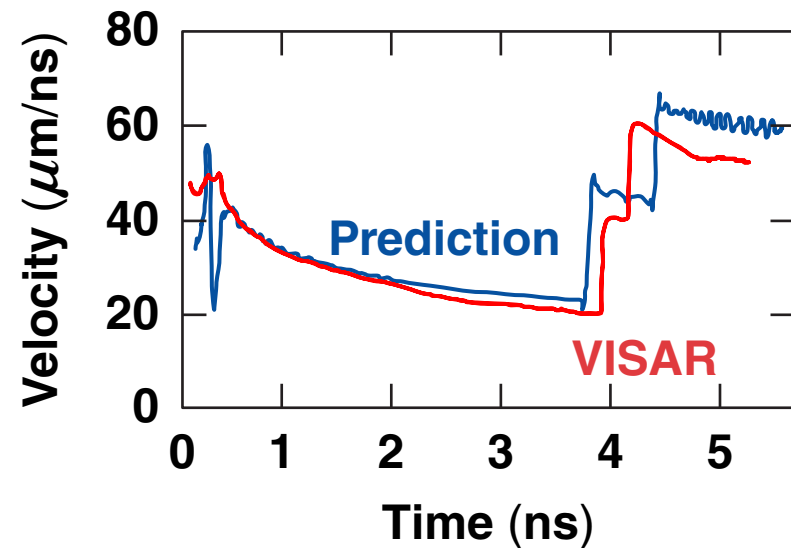
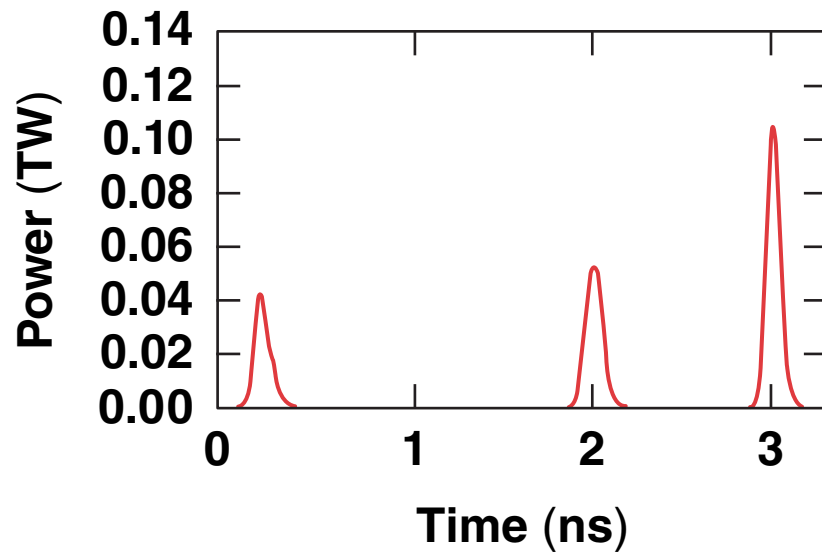


# The current experimental campaign addresses both shock timing and effect of reduction in the main shock strength

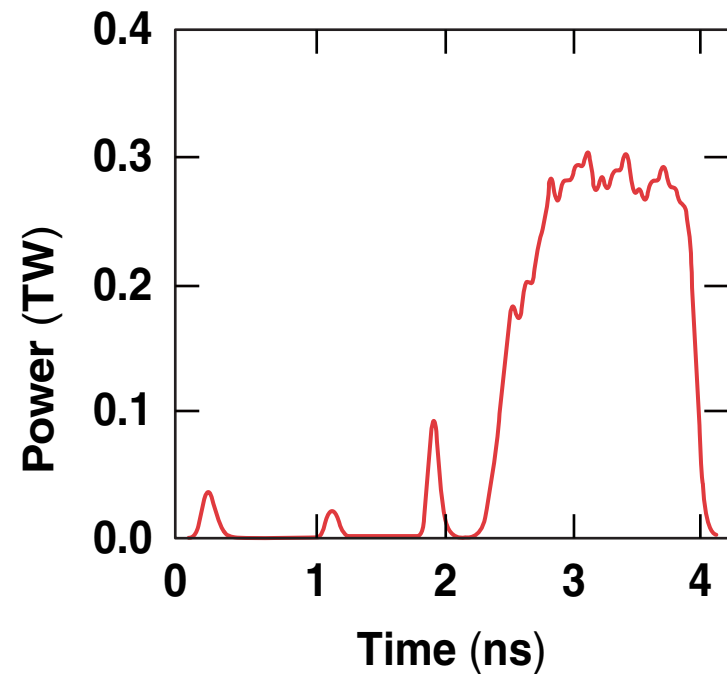
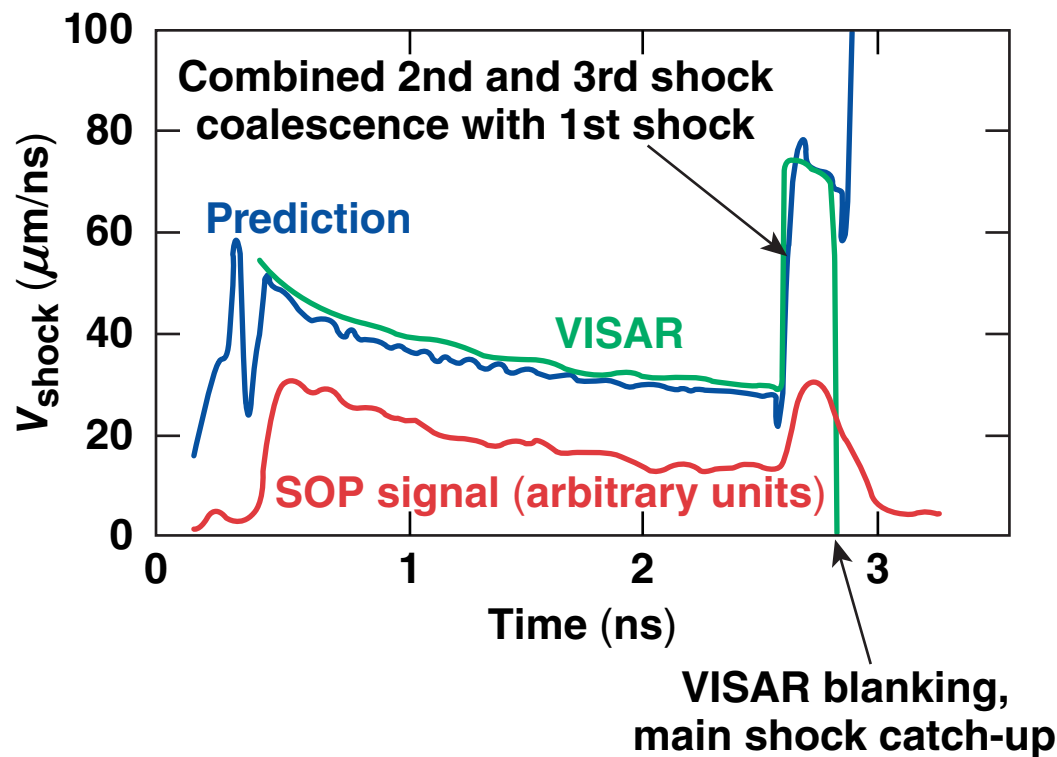


Timing of shocks launched by first two tickets is complete.

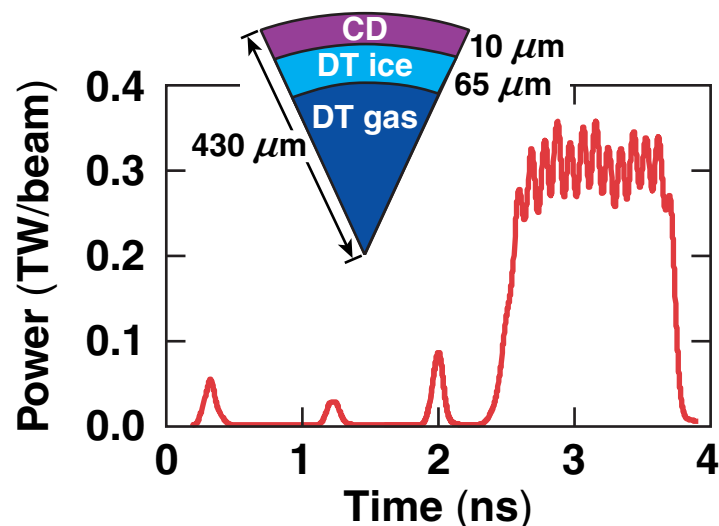
# Tuning of the third picket is carried out with stand-alone triple-picket pulses



# Main shock tuning is achieved by timing the catch-up signature in SOP and VISAR



# Areal densities $\sim 200 \text{ mg/cm}^2$ ( $>85\%$ of 1-D) are achieved in triple-picket square designs

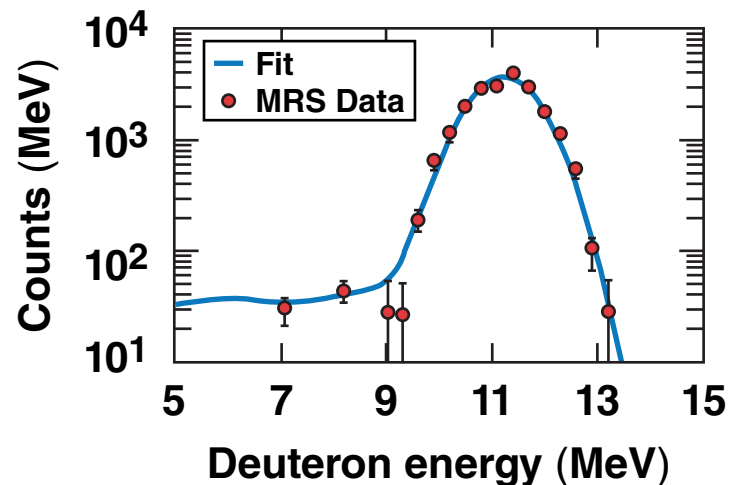
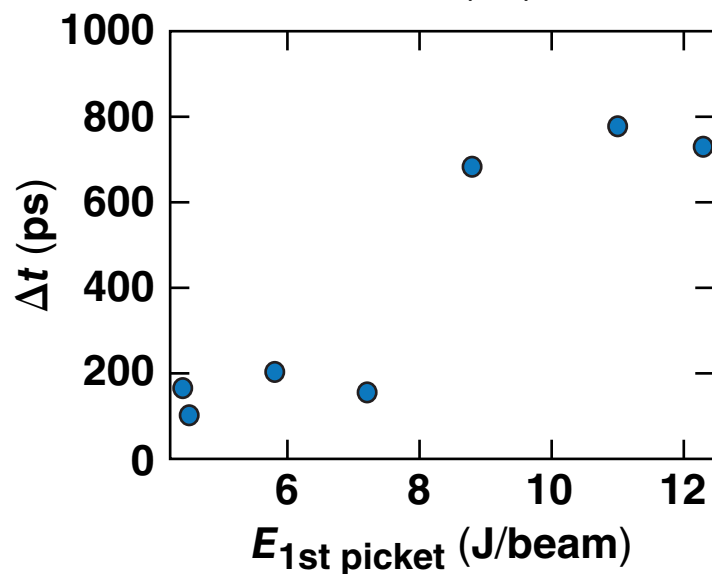


$V_{\text{imp}} \sim 3 \times 10^7 \text{ cm/s}$

$R_{\text{h.s.}} \sim 20 \text{ } \mu\text{m}$

YOC  $\sim 10\%$

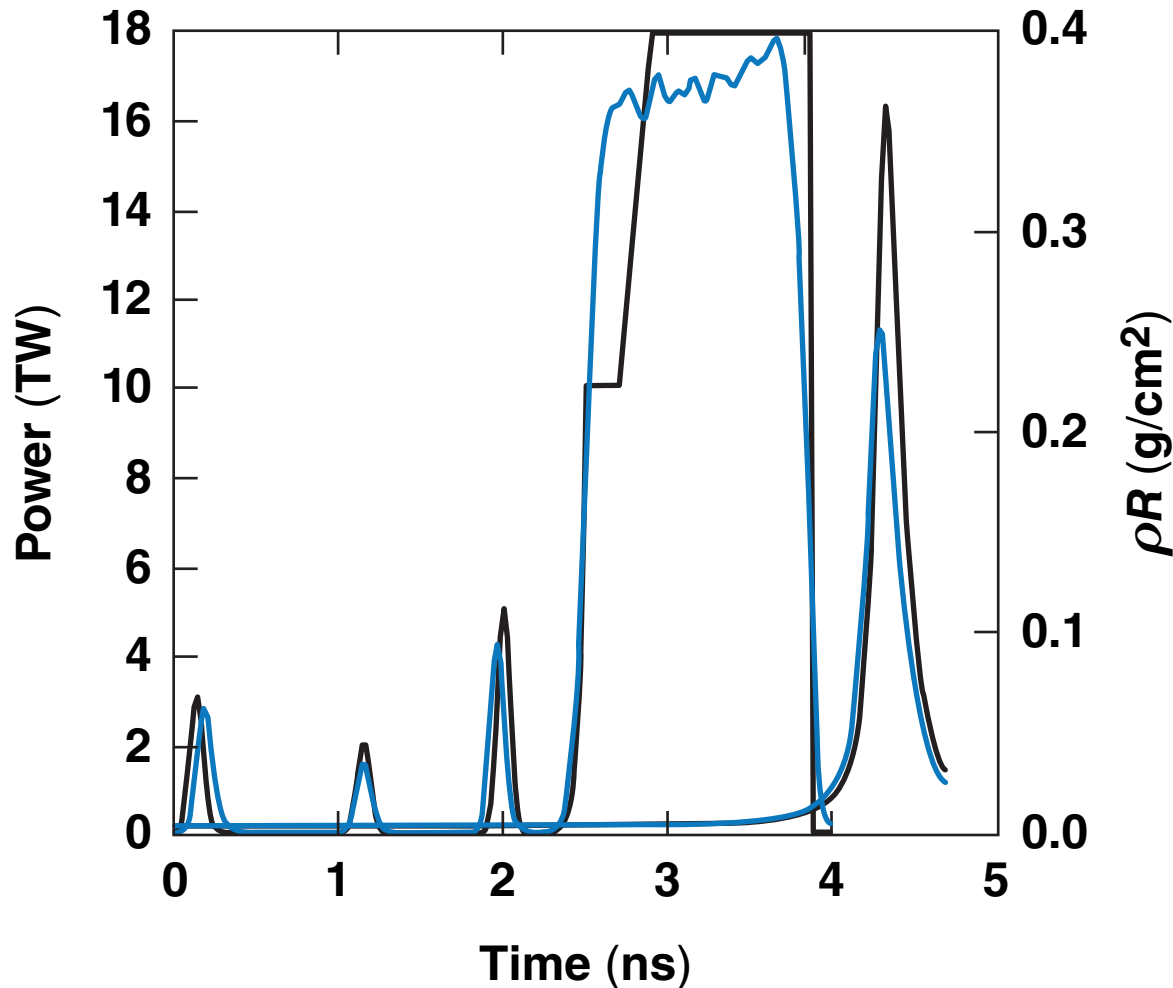
$I \sim 7.5 \text{ to } 8 \times 10^{14} \text{ W/cm}^2$



$\rho R = 185 \pm 27 \text{ mg/cm}^2$

$\rho R_{1-D} = 214 \text{ mg/cm}^2$

# Triple-picket designs with a step lead to higher measured areal densities



$V_{\text{imp}} \sim 3 \times 10^7 \text{ cm/s}$

$R_{\text{h.s.}} \sim 15 \mu\text{m}$

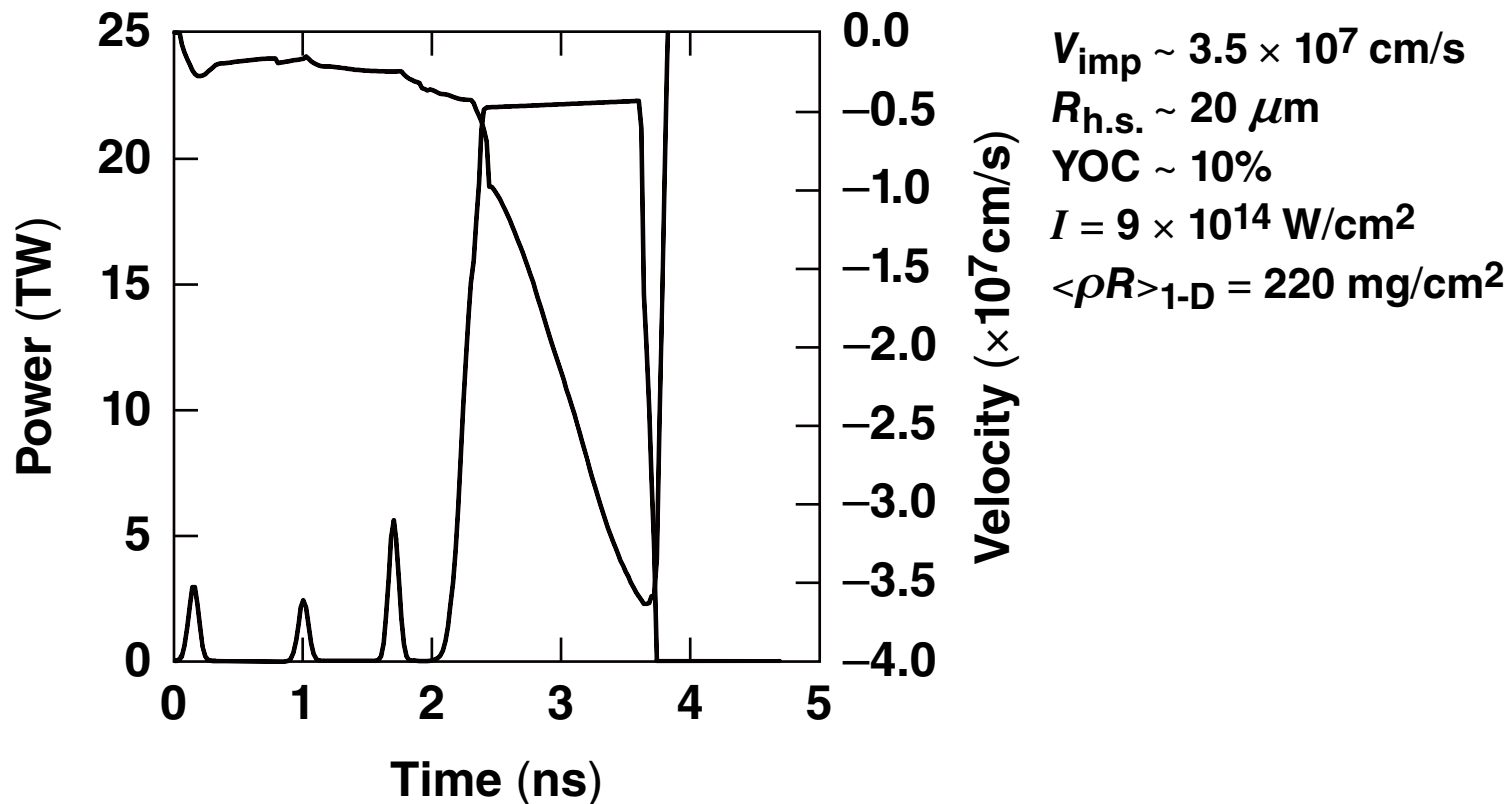
YOC  $\sim 5\%$

$I \sim 7.5 \text{ to } 8 \times 10^{14} \text{ W/cm}^2$

$\langle \rho R \rangle_{1-D} = 310 \text{ mg/cm}^2$

$\langle \rho R \rangle_{\text{exp}} = 295 \pm 65 \text{ mg/cm}^2$

Ignition-relevant implosion velocity  $V_{\text{imp}} \sim 3.5 \times 10^7$  cm/s will be achieved on OMEGA using 55- $\mu\text{m}$ -thick DT ice and  $I_{\text{peak}} \sim 9 \times 10^{14}$  W/cm<sup>2</sup>



A higher-adiabat square main pulse is used to enhance shell stability.

## Summary/Conclusions

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