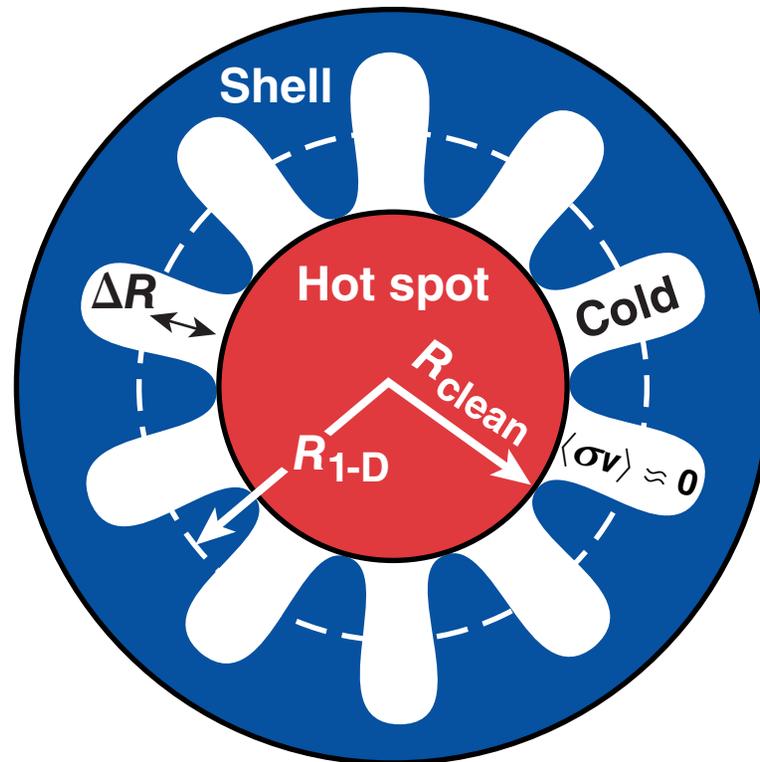


A Measurable Three-Dimensional Ignition Criterion for Inertial Confinement Fusion



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An analytic model of the hot-spot evolution provides a measurable 3-D ignition criterion for ICF



- The one-dimensional (1-D) measurable Lawson criterion of Zhou and Betti* is extended to 3-D using the Yield-Over-Clean (YOC) as a measure of the implosion uniformity
- The ignition parameter from the analytic theory depends on areal density, ion temperature, and yield-over-clean
- The analytic model is in reasonable agreement with a simulation database yielding
- Cryogenic implosions on OMEGA have achieved an ignition parameter $\chi^{\text{fit}} \approx 0.008$. Hydro-equivalent ignition on OMEGA requires $\chi \approx 0.04$.

Collaborators



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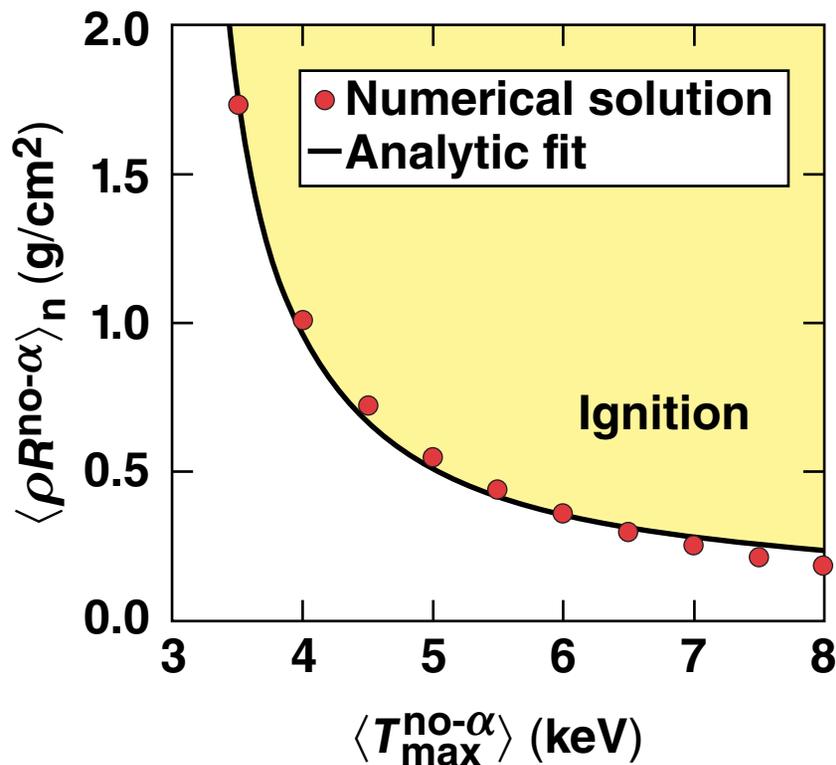
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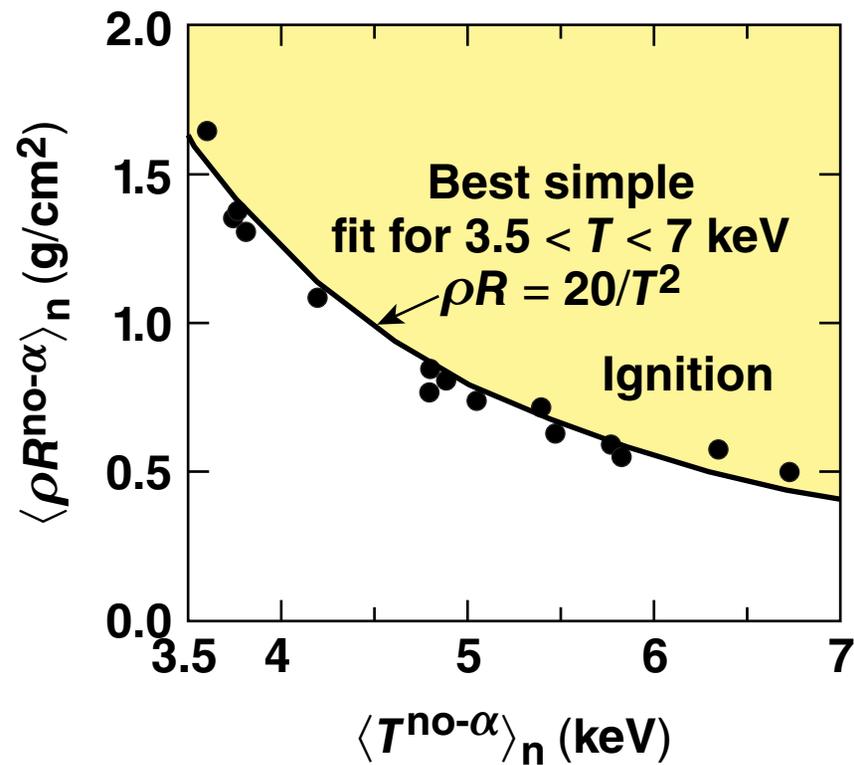
The one-dimensional ignition criterion depends on the total areal density and ion temperature (without calculated α -particle deposition)



Zhou and Betti 1-D Model



1-D Simulations



$$\left\langle \rho R_{\text{g/cm}^2}^{\text{no-}\alpha} \right\rangle_n \left(\frac{\left\langle T_{\text{keV}}^{\text{no-}\alpha} \right\rangle}{4.5} \right)^2 > 1 \quad \text{for } 3.5 < T_{\text{keV}}^{\text{no-}\alpha} < 7$$

The effects of nonuniformities in the deceleration phase are added to the ignition model through a clean volume analysis



- Nonuniformities reduce the volume where fusion reactions occur:*

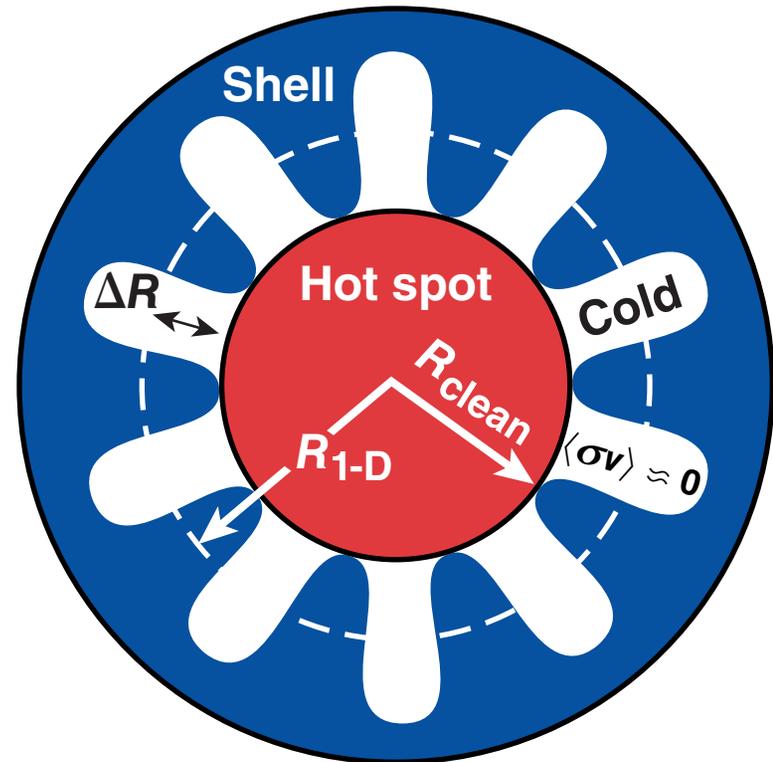
$$V_{\text{fusion}} \approx V_{\text{clean}} = \frac{4\pi}{3} R_{\text{clean}}^3$$

- The hot spot energy balance is affected by a reduced “clean” volume

$$\frac{d}{dt}(PR^3) = -2PR^2 \frac{dR}{dt} + \frac{\epsilon_\alpha}{8\pi} \int_0^{V_{\text{clean}}} \langle \sigma v \rangle n^2 dv$$

$$\epsilon_\alpha = 3.5 \text{ MeV}$$

- $\langle \sigma v \rangle \approx C_\alpha T^3 \leftarrow$ valid for $T \sim 4$ to 8 keV



Fusion reactions occur only within the clean volume.

Zhou* and Betti's model is modified to include the clean radius in the hot-spot energy balance



- The hot-spot formation and ignition model is governed by three ODE's

Hot-spot energy balance

$$\frac{d}{dt}(PR^3) = \underbrace{-2pR^2 \frac{dR}{dt}}_{\text{Compression/expansion}} + \underbrace{\frac{\epsilon_\alpha}{8} C_\alpha P^2 R_{\text{clean}}^3 T}_{\alpha\text{-particles deposition}}$$

Temperature equation (from hot-spot mass conservation)

$$\frac{d}{dt}\left(\frac{PR^3}{T}\right) = \underbrace{0.87 \kappa_0 RT^{5/2}}_{\text{Heat conduction}} + \underbrace{\cancel{C_{\text{rad}} \frac{P^2 R^3}{T^{5/2}}}}_{\text{Radiation}}$$

$\kappa_{\text{sp}} = \kappa_0 T^{5/2}$

Neglected in this talk

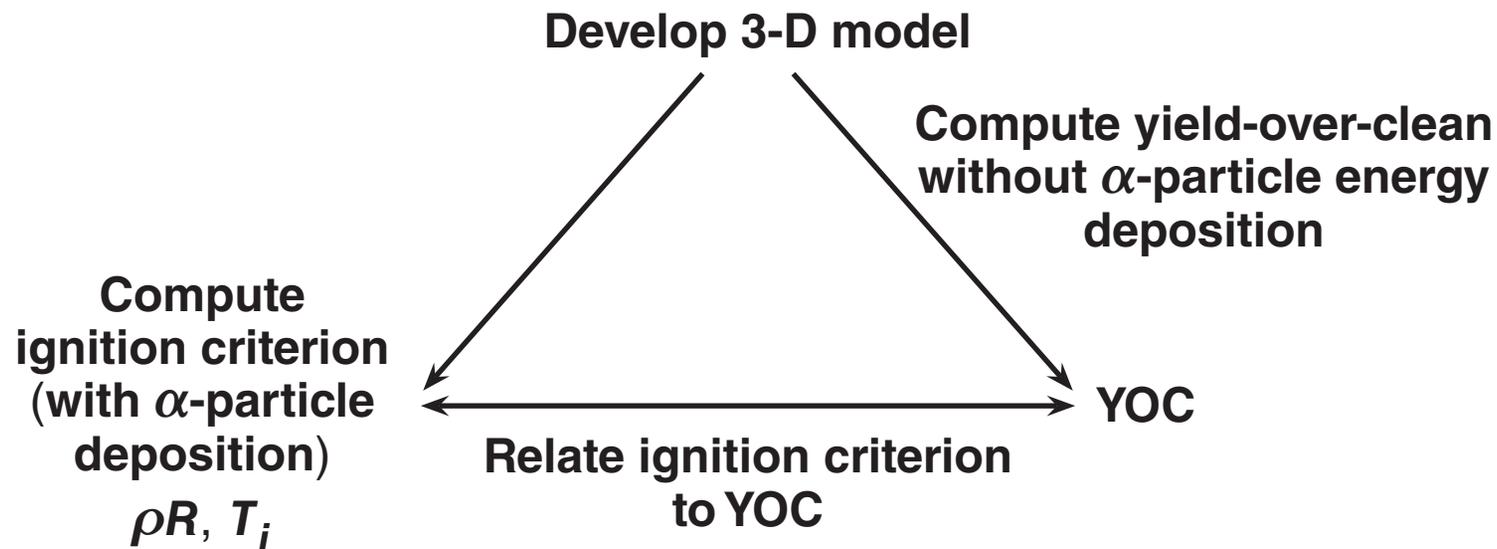
Shell Newton's law

$$\underbrace{M_{\text{sh}}}_{\text{Shell mass}} \frac{d^2 R}{dt^2} = 4\pi PR^2$$

The yield-over-clean (YOC) is used as a measure of the implosion uniformity



$$\text{YOC} = \left[\frac{\text{Yield}_{3\text{-D}}}{\text{Yield}_{1\text{-D}}} \right] \sim \frac{R_{\text{clean}}^3}{R_{1\text{-D}}^3}$$

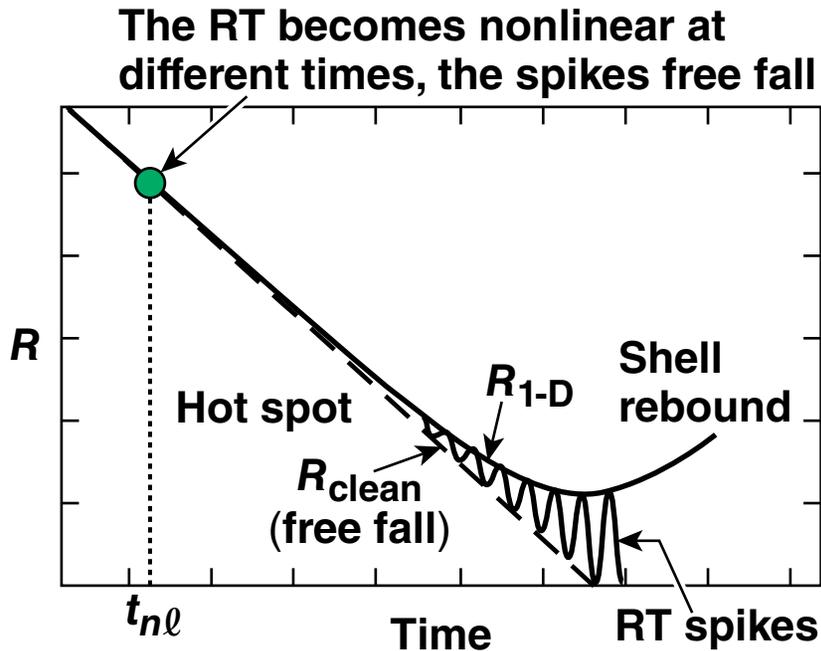


$$\text{Ignition criterion } f(\rho R, T_i, \text{YOC}) = 0$$

Multiple models are used to assess the sensitivity of the ignition conditions to the hot-spot model



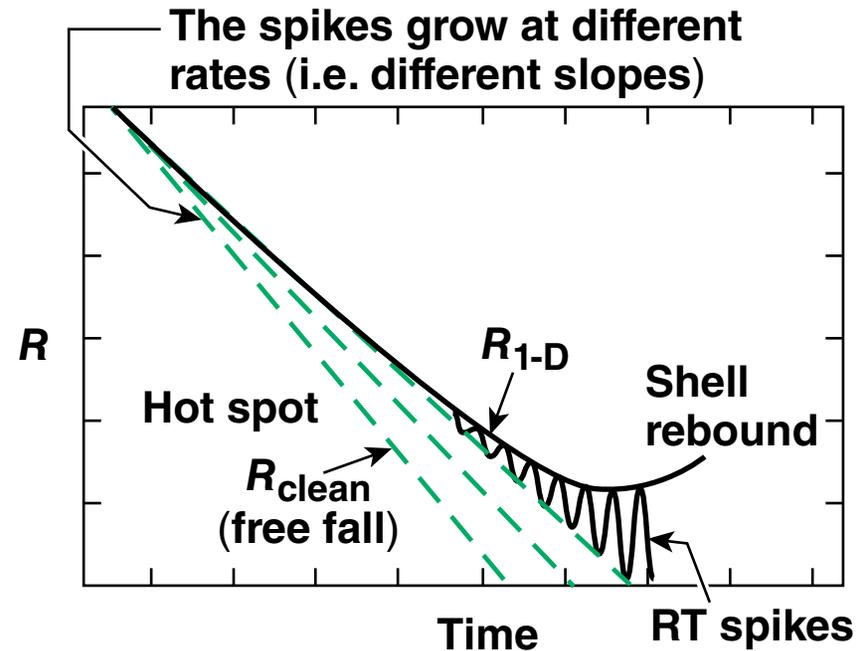
Model I



$$YOC^{\text{no-}\alpha} = YOC^{\text{no-}\alpha} (t_{n\ell})$$

$$t_{n\ell} = t_{n\ell} (YOC^{\text{no-}\alpha})$$

Model II



$$YOC^{\text{no-}\alpha} = YOC^{\text{no-}\alpha} (\text{slope})$$

$$\text{slope} = \text{slope} (YOC^{\text{no-}\alpha})$$

$$R_{\text{clean}} = R_{\text{clean}} (YOC^{\text{no-}\alpha})$$

The ignition model is cast in a dimensionless form using stagnation properties calculated without α -particle deposition



- Ignition depends on two parameters: γ_α and $YOC^{no-\alpha}$

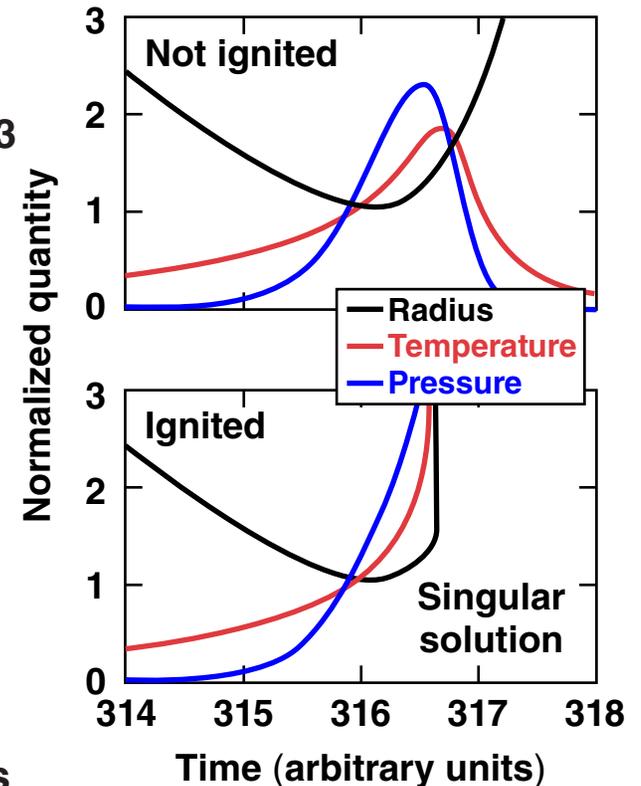
Dimensionless equations

$$\begin{cases} \frac{d}{d\tau} (\hat{P}\hat{R}^3) = -2\hat{P}\hat{R}^2 \frac{d\hat{R}}{d\tau} + \gamma_\alpha \hat{T} \hat{P}^2 \left[\hat{R}_{\text{clean}} (YOC^{no-\alpha}) \right]^3 \\ \frac{d}{d\tau} \left(\frac{\hat{P}\hat{R}^3}{\hat{T}} \right) = \hat{R}\hat{T}^{5/2} \\ \frac{d^2 \hat{R}}{d\tau^2} = \hat{P}\hat{R}^2 \end{cases}$$

$$\gamma_\alpha = 0.07 (\rho R)^{3/4} (T_{\text{stag}}^{no-\alpha})^{15/18} *$$

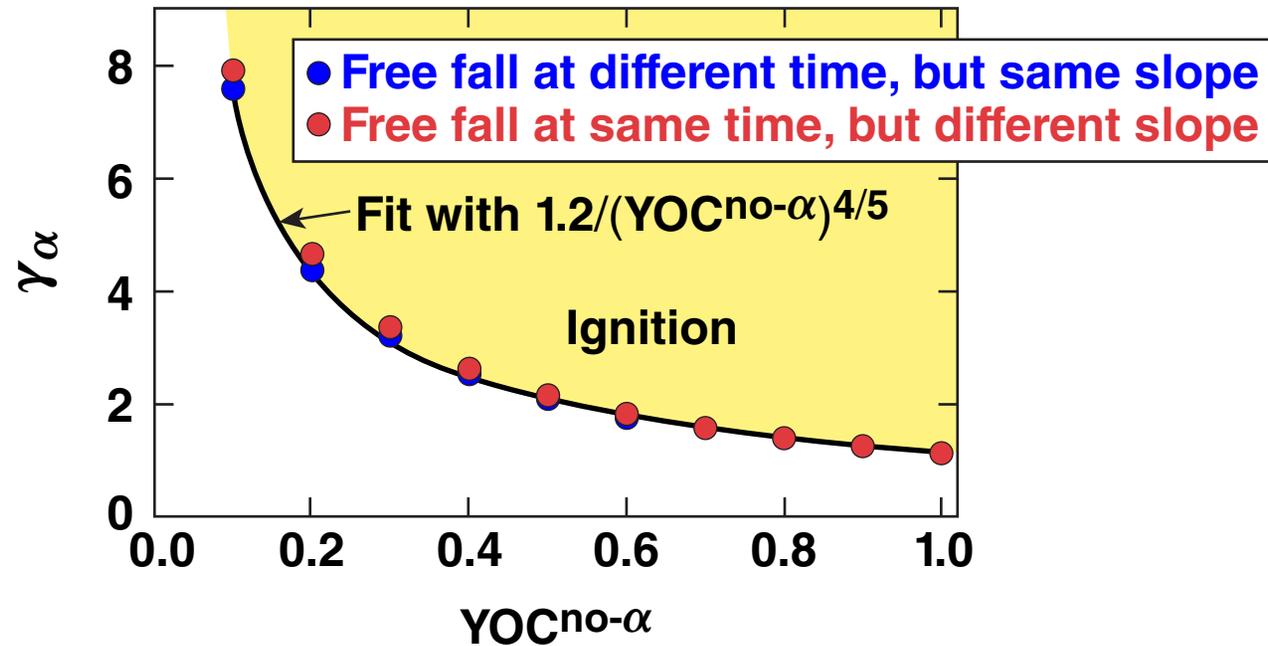
$$\tau = \frac{tV_i}{R_{\text{stag}}^{no-\alpha}}, \quad \hat{R} = \frac{R}{R_{\text{stag}}^{no-\alpha}}, \quad \hat{P} = \frac{P}{P_{\text{stag}}^{no-\alpha}}, \quad \hat{T} = \frac{T}{T_{\text{stag}}^{no-\alpha}}$$

Stagnation properties calculated without α 's

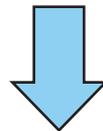


Ignition condition: for a fixed $YOC^{no-\alpha}$, find critical γ_α leading to singular solutions.

The 3-D ignition condition is approximately independent of the hot-spot models



Model independent ignition criterion $\gamma_\alpha (YOCC^{no-\alpha})^{4/5} > 1.2$

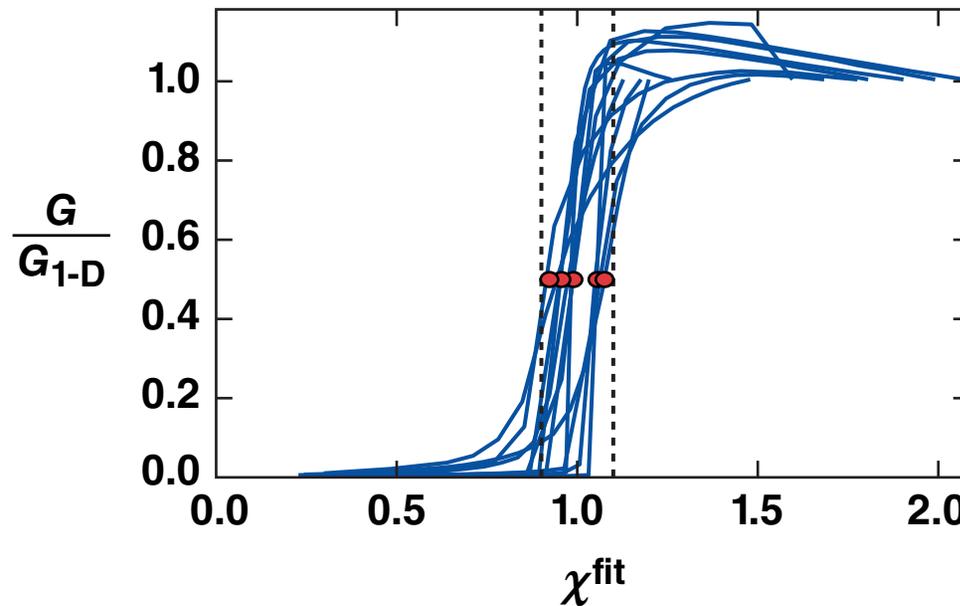


Ignition parameter: $\chi = \rho R_{tot}^{no-\alpha} \left(\frac{T^{no-\alpha}}{4.6} \right)^{5/2} (YOCC^{no-\alpha})^{16/15} > 1$

The clean volume model is implemented in *LILAC* and is used to generate a database of gain curves. The ignition condition is tuned with the simulation database



- In the 1-D code *LILAC*, $\langle \sigma v \rangle$ is replaced by $\langle \sigma v \rangle \text{YOC} \approx \langle \sigma v \rangle \frac{V_{\text{clean}}}{V_{1-D}}$



Find exponents and constant (μ, δ, T_0) in ignition conditions to minimize the spread at $1/2 G_{1-D}$

$$\chi^{\text{fit}} = (\rho R)^{\text{no} - \alpha} \left(\frac{T^{\text{no} - \alpha}}{T_0} \right)^{\mu} (\text{YOC}^{\text{no} - \alpha})^{\delta}$$

Ignition parameter:

$$\chi^{\text{fit}} = (\rho R)^{\text{no} - \alpha} \left(\frac{T^{\text{no} - \alpha}}{4.7} \right)^2 (\text{YOC}^{\text{no} - \alpha})^{0.7} > 1$$

Cryogenic implosions on OMEGA have achieved $\chi^{\text{fit}} \approx 0.008$;
hydro-equivalent ignition on OMEGA requires $\chi \approx 0.04$



- For cryogenic implosions on OMEGA (have achieved)

$$(\rho R)_{\text{stag}}^{\text{no-}\alpha} \approx 0.2 \text{ g/cm}^2, \quad T_{\text{stag}}^{\text{no-}\alpha} \approx 2.1 \text{ keV}, \quad \text{YOC} = 0.1^*$$

$$\chi^{\text{fit}} = 0.008$$

- Hydro-equivalent ignition on OMEGA requires

$$(\rho R)_{\text{stag}}^{\text{no-}\alpha} \approx 0.3 \text{ g/cm}^2, \quad T_{\text{stag}}^{\text{no-}\alpha} \approx 3.4 \text{ keV}, \quad \text{YOC} = 0.15$$

$$\chi^{\text{fit}} = 0.04^{**}$$

An analytic model of the hot-spot evolution provides a measurable 3-D ignition criterion for ICF and is in good agreement with simulation results



- **The one-dimensional (1-D) measurable Lawson criterion of Zhou and Betti* is extended to 3-D using the Yield-Over-Clean (YOC) as a measure of the implosion uniformity**
- **The ignition parameter from the analytic theory depends on areal density, ion temperature, and yield-over-clean**
- **The analytic model is in reasonable agreement with a simulation database yielding**
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