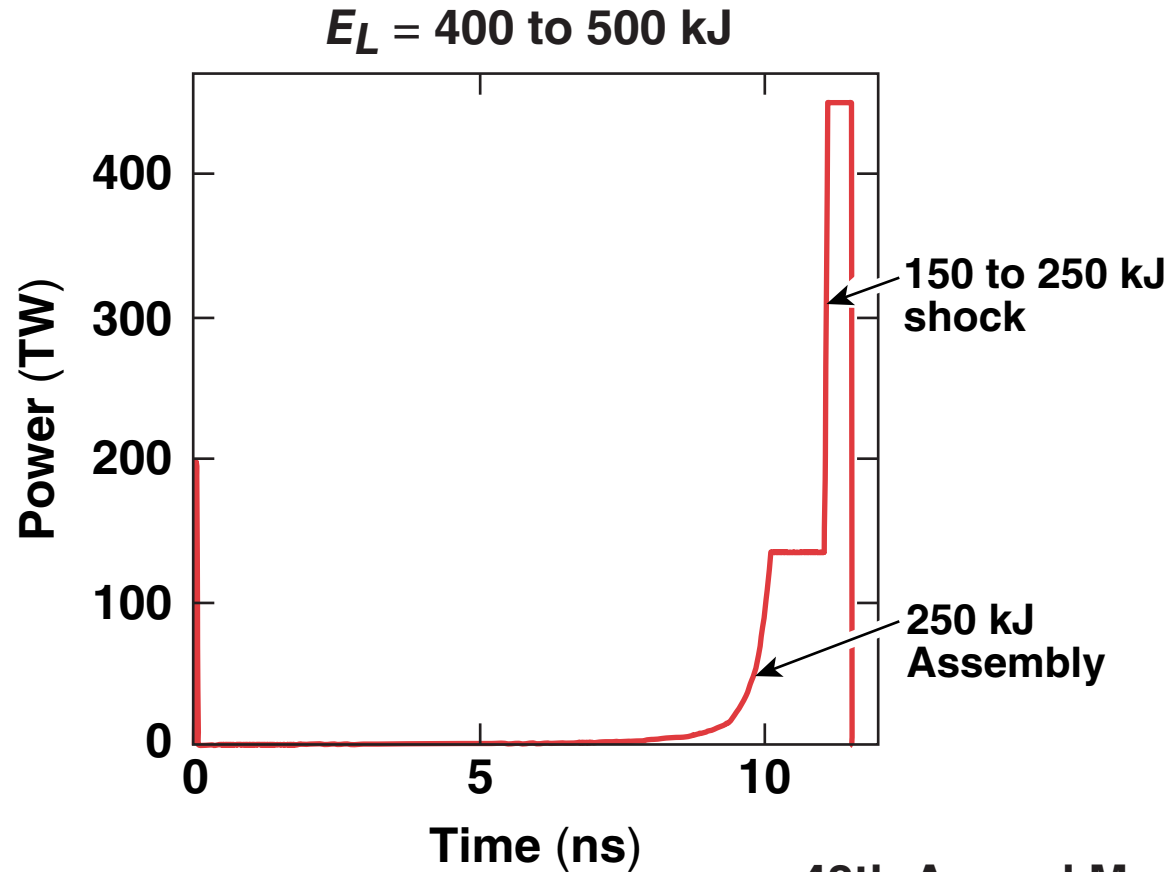


# Shock Ignition of Thermonuclear Fuel with High-Areal Density



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48th Annual Meeting of the  
American Physical Society  
Division of Plasma Physics  
Philadelphia, PA  
30 October–3 November 2006

## Summary

**Optimal targets for shock ignition are thick shells driven on a low adiabat at low implosion velocities (and low IFAR ~20)**



- **A convergent shock launched by a spike in the laser intensity leads to an adiabatic compression of the hot spot and reduction of the energy required for ignition.**
- **The robustness of the SI scheme is measured by the size of the shock-launching-time ignition window.**
- **2-D simulations indicate that shock ignition may survive the detrimental effects of laser imprinting at a relatively low driver energy (~400 to 500 kJ) leading to gains of ~50 to 80.**
- **Applications of SI to the NIF in following talk U02.00011 by L. J. Perkins**

**Significant gains are predicted with moderate driver energies.**

# Collaborators



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**High areal densities ( $\rho R$ ) and low-implosion velocities ( $V_i$ ) lead to high-energy gains (assuming that ignition occurs)**



$$G = \frac{E_{\text{fusion}}}{E_{\text{laser}}} \sim \frac{\theta}{V_i^{1.2}}$$

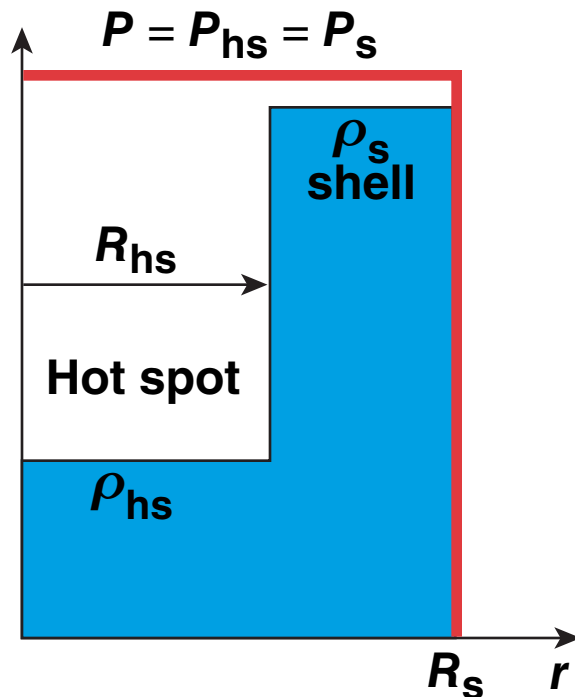
$$\theta = \frac{1}{1 + 7/\rho R} = \text{burnup fraction}$$

- Higher  $\rho R \rightarrow$  longer burn time
- Lower  $V_i \rightarrow$  more fuel mass for the same kinetic/laser energy

# The hot-spot ignition condition is given by the balance of alpha heating with energy losses, including expansion losses



Isobaric fuel assembly



$$\frac{\dot{E}_{hs}}{E_{hs}} = \frac{1}{\tau_{\alpha}} - \frac{1}{\tau_{rad}} - \frac{1}{\tau_{exp}} > 0$$

$$1/\tau_{\alpha} \sim n_{hs}^2 \langle \sigma v \rangle / P_{hs} \quad \text{alpha heating}$$

$$1/\tau_{rad} \sim n_{hs}^2 \sqrt{T_{hs}} / P_{hs} \quad \text{radiation cooling}$$

$$1/\tau_{exp} \sim \sqrt{\ddot{R}_{hs}} / R_{hs} \quad \text{expansion}$$

$$M_s \ddot{R}_{hs} = 4\pi P_{hs} R_{hs}^2 \quad \text{shell Newton's law}$$

# For isobaric fuel assemblies, the ignition condition depends only on velocity and shell areal density



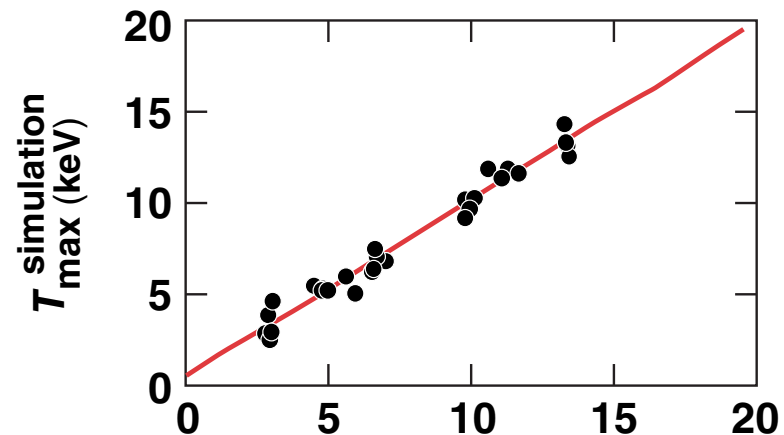
$$(\rho_s \Delta_s)^2 V^2 (T_{\text{keV}}^{\text{isob}} - 4.4) > \text{const}$$

- $V_{\text{min}}$  is the minimum velocity required to overcome radiative losses  $\sim 1.5 \times 10^7$  cm/s.

$$(\rho_s \Delta_s)^2 V^2 \left[ \left( \frac{V}{V_{\text{min}}} \right)^{1.4} - 1 \right] > \text{const}$$

For  $V \gg V_{\text{min}}$

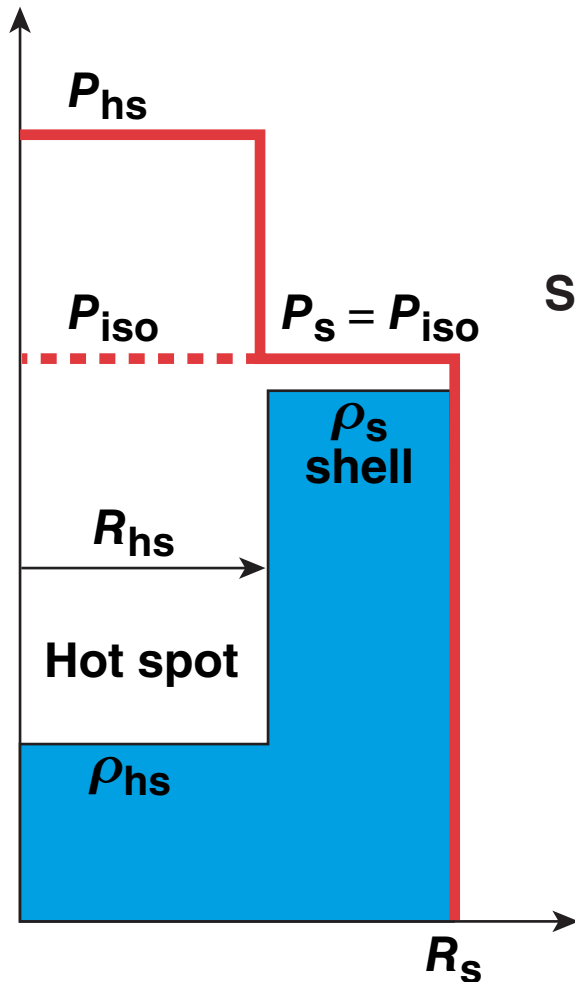
$$(\rho_s \Delta_s) > \frac{\text{const}}{V^{1.7}}$$



$$T_{\text{hot spot}}^{\text{max}} (\text{keV})^{\text{fit}} = 7 \left[ \frac{V_i (\text{cm/s})}{3 \times 10^7} \right]^{1.4}$$

Ignition requirements set a threshold for the shell areal density.

# The ignition condition can be modified to include the effect of a non-isobaric fuel assembly



$$\hat{\phi} (\rho_s \Delta_s)_{iso}^2 v^2 \left( \hat{\phi}^{0.3} \left( \frac{v}{v_{min}} \right)^{1.4} - 1 \right) > const$$

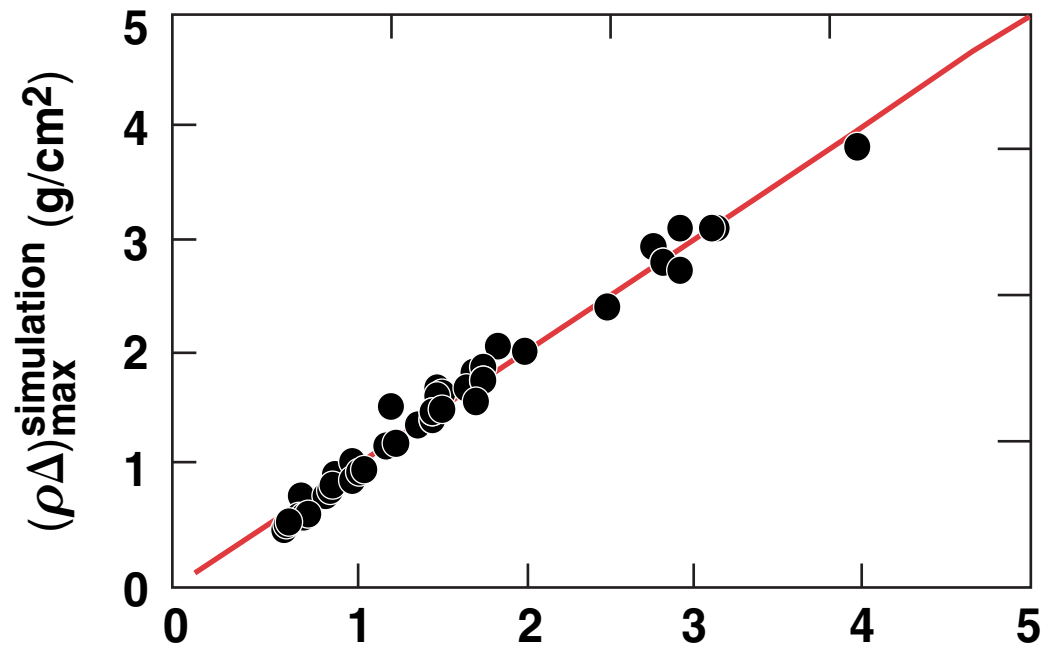
Shell areal density

Implosion velocity

Non-isobaric enhancement

$$\hat{\phi} \equiv \frac{P_{hs}/R_{hs}}{P_{iso}/R_{iso}}$$

# The areal density depends on energy and adiabat



$$(\rho\Delta)_{\max}^{\text{fit}} = \frac{1.2}{\alpha^{0.57}} \left( \frac{E_L (\text{kJ})}{100} \right)^{0.33} \left( \frac{V (\text{cm/s})}{3 \times 10^7} \right)^{0.1} \text{g/cm}^2$$

R. Betti and C. Zhou, Phys. Plasmas 12, 110702 (2005).  
C. Zhou, BO3.00003



# The ignition threshold can be lowered in non-isobaric fuel assemblies



$$E_{\text{ign}}^{\text{min}} = \text{const} \times \frac{\alpha^{1.8}}{V^{5.4}} \frac{1}{\hat{\phi}^2} + E^{\text{non-isob}}$$

← Recover Herrmann *et al.* scaling for  $\hat{\phi} = 1$ ,  $E^{\text{non-isob}} = 0$

$$\hat{\phi}^2 \sim \left( \frac{P_{\text{hs}}/R_{\text{hs}}}{P_{\text{iso}}/R_{\text{iso}}} \right)^2 \sim \left( \frac{R_{\text{iso}}}{R_{\text{hs}}} \right)^{12}$$

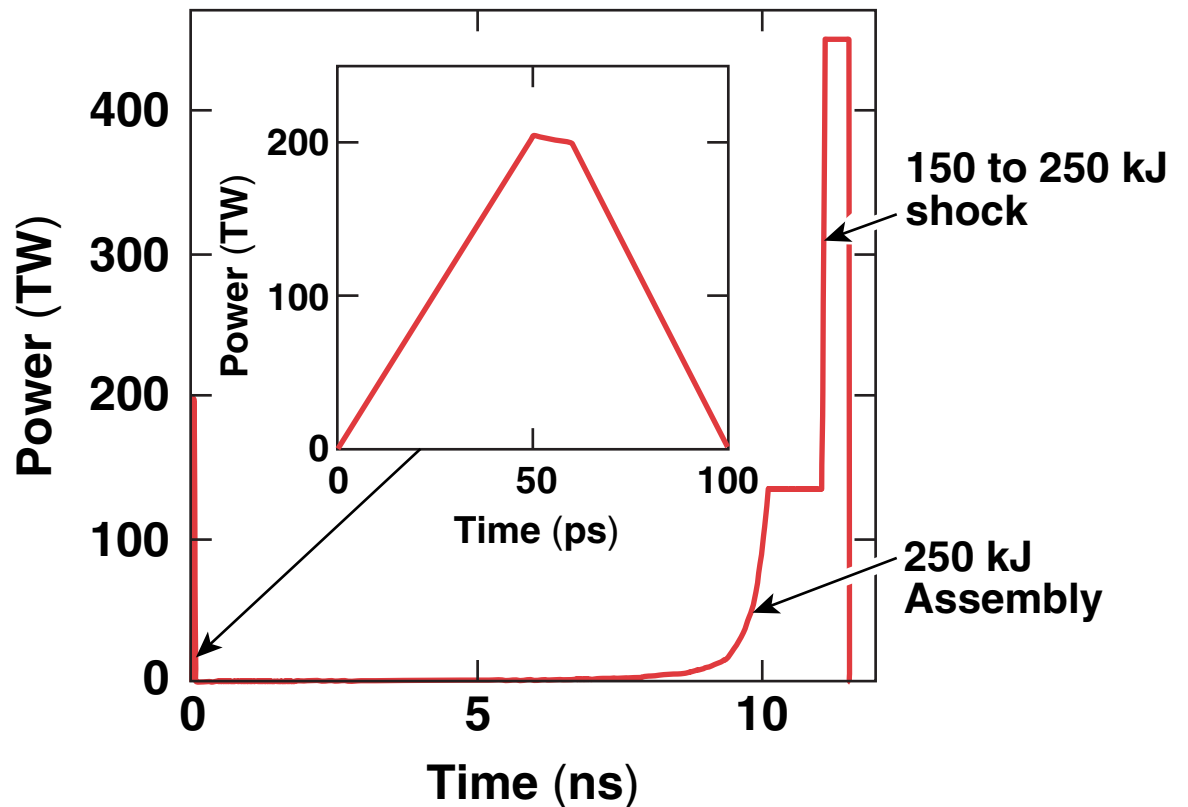
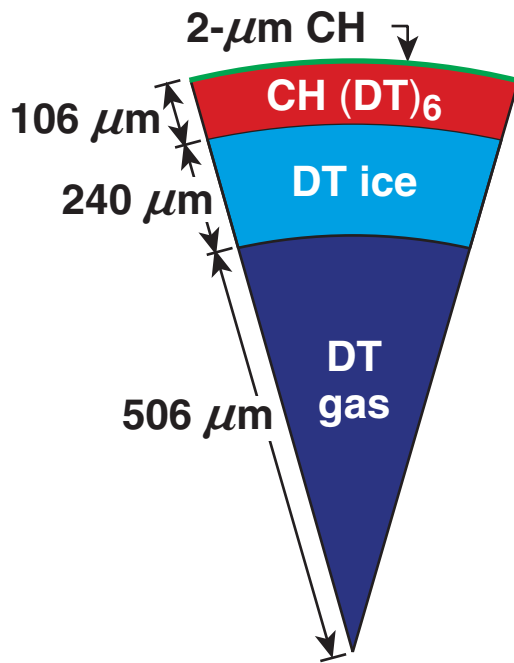
← For adiabatic compression of the hot spot

Large improvements for small reductions of the hot-spot radius.

# Non-isobaric enhancement is achieved through a convergent shock; the ignitor shock is launched by a spike of the laser intensity



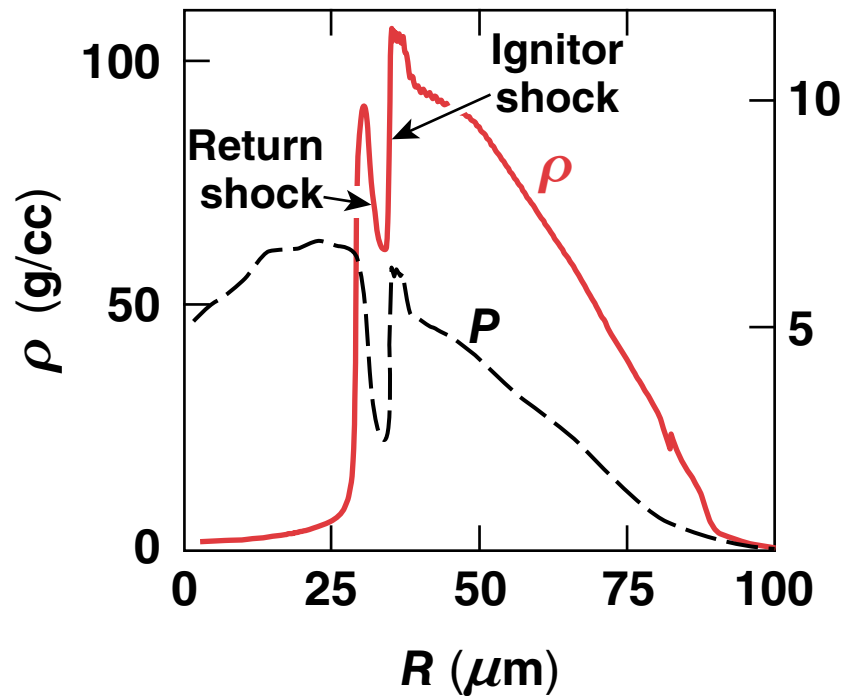
$$E_L = 400 \text{ to } 500 \text{ kJ}, V_i = 2.4 \times 10^7 \text{ cm/s}, \alpha = 0.7 \text{ to } 1.0$$



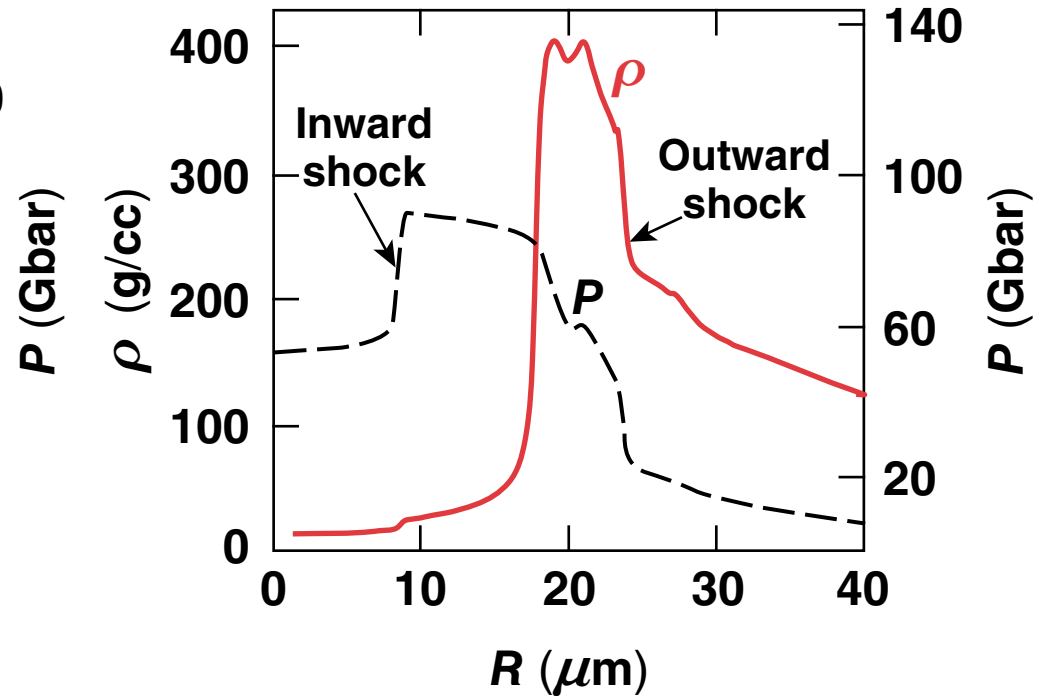
IFAR  $\approx 18$

Minimum shock energy for ignition = 50 kJ

# The shock resulting from the collision of the ignitor and return shock compresses the hot spot

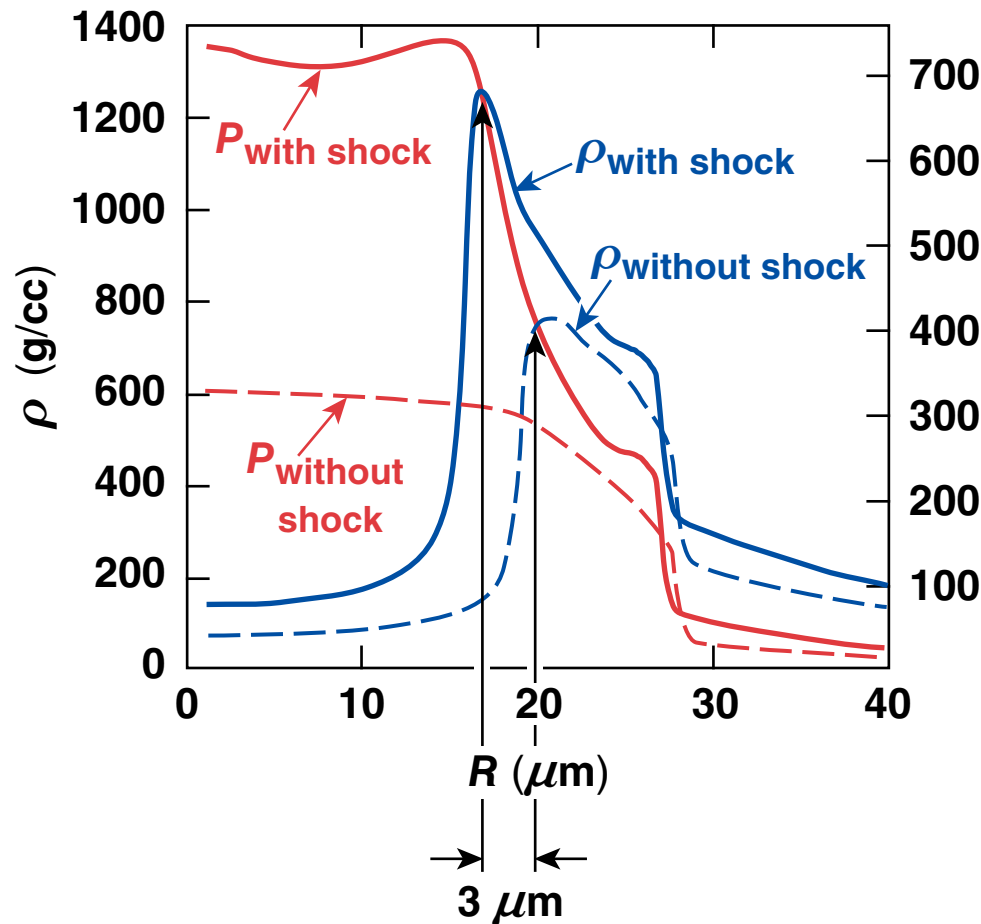


Before collision



After collision

# The shock-induced compression of the hot spot is adiabatic; the ignition condition is improved



The shock compression is adiabatic

$$P_{\text{shock}} = P_{\text{no shock}} \left( \frac{R_{\text{no shock}}}{R_{\text{shock}}} \right)^5$$

340      20      17

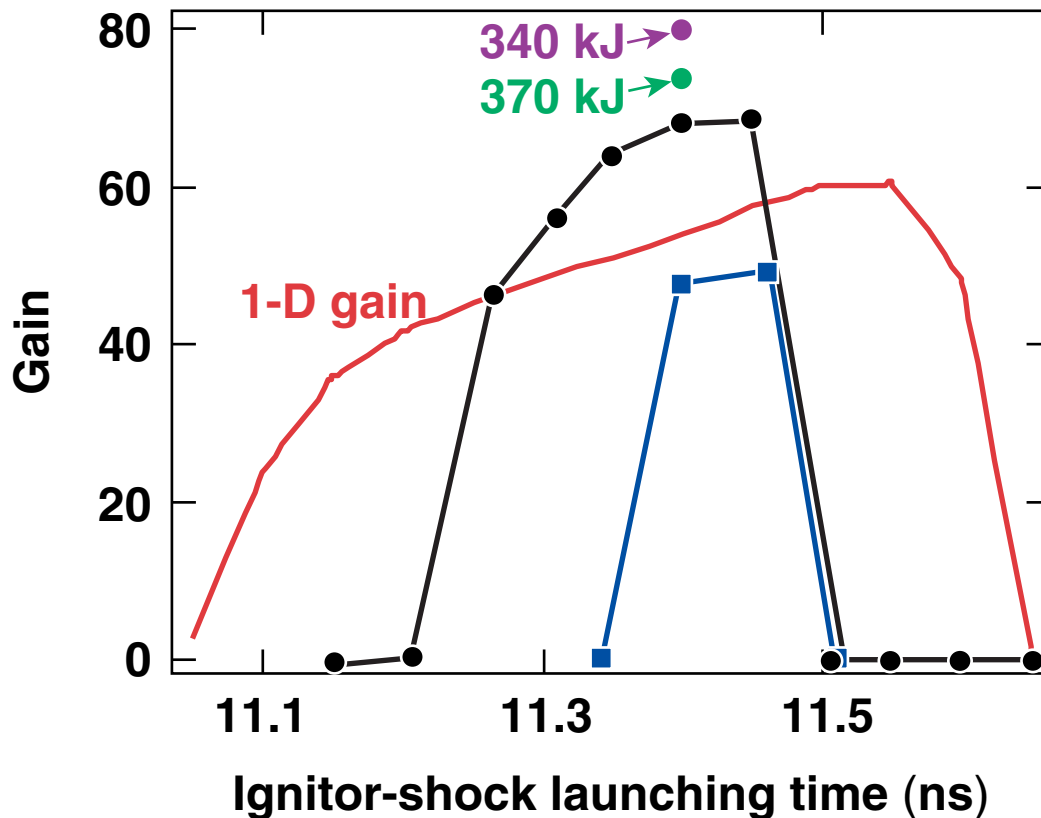
$$P_{\text{shock}} = 720 \text{ Gbar}$$

Non-isobaric enhancement

$$\hat{\phi}^2 = 7$$

Reduction of the energy required for ignition for a "free" shock

# The robustness of the ignition is measured by the size of the shock-ignition window



- 2-D simulations
  - modes  $\ell = 4$  to 100
  - NIF 2-D SSD
  - energy = 400 kJ
  - normal incidence
  - Thomas–Fermi EOS
  - no radiation
- 2-D simulations
  - modes  $\ell = 4$  to 100
  - energy = 500 kJ
  - 12-group radiation

## Summary/Conclusions

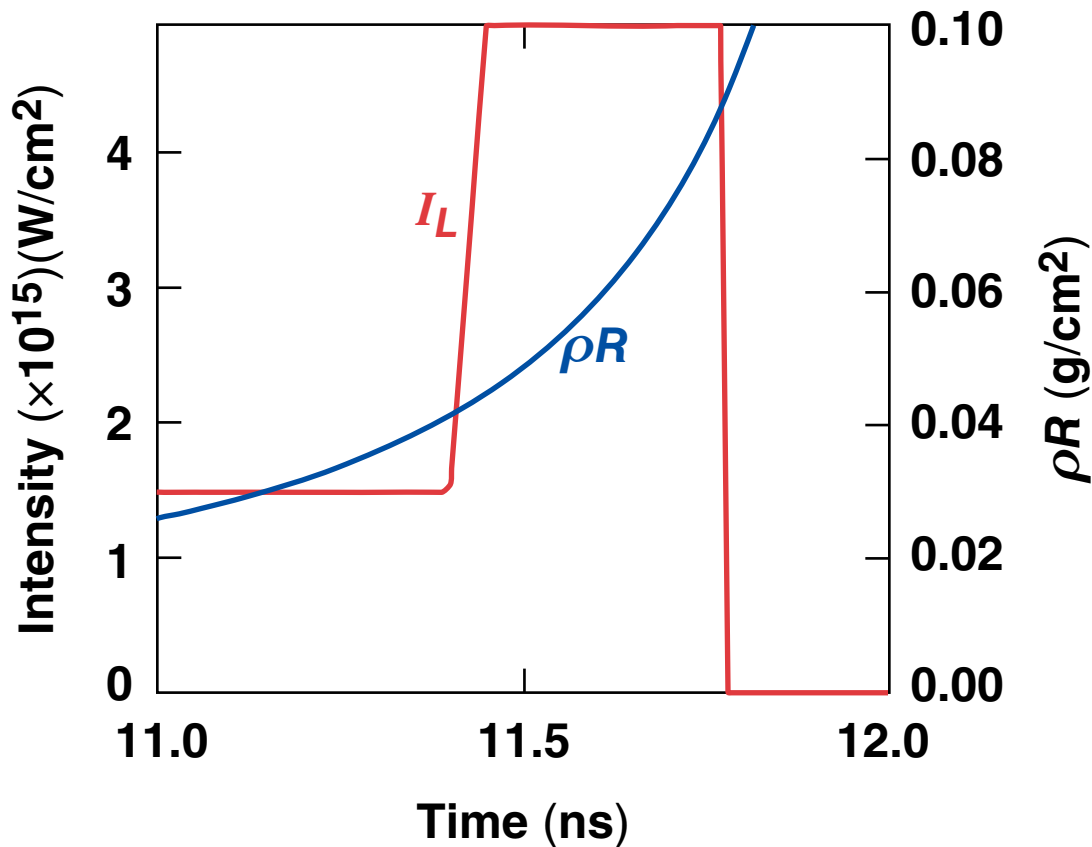
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# Hot electrons with energies $<100$ keV slow down on the shell's outer surface



Electron penetration

