Controlling the symmetry of direct-drive implosions with target shimming



Fredrick H. Séguin et al., MIT

APS 2005



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Summary

1) Target shimming changes nuclear burn symmetry

- 2) Drive asymmetry results in burn asymmetry and reduced performance
- 3) Shimming could counteract drive asymmetry
 - Polar Direct Drive
 - Indirect Drive
- 4) A formula is proposed for estimating the amount of shimming necessary







Collaborators

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Neutron imaging of DT burn at OMEGA

- L. Disdier *et al.*
- C. Christensen, G. Grim *et al.*

Study of P₄ shimming in indirect drive at the Sandia Z pinch

• D. Callahan, G. Bennet *et al.*

Two types of target were illuminated symmetrically by 22-kJ, 1-ns square laser pulses at OMEGA



Orthogonal proton emission imaging cameras were used to study the spatial distribution of nuclear burn



The spherical target imploded symmetrically



The shimmed targets imploded with prolate asymmetry



Each image is now characterized by two different radii (for the long and short axes), as plotted on the next page

Burn measurements and x-ray measurements show similar distortion in core and shell due to shimming



Asymmetric drive leads to asymmetric burn and reduced yield



There are systematic connections between burn asymmetry and each of its causes



Let's vary the shell thickness to get uniform implosion velocity and radius after the acceleration phase



The shell thickness variation required to keep the implosion velocity symmetric can be estimated from the ablation-driven rocket equations

For direct drive (from J.D. Lindl, PoP **2**, p. 3933):

$$\stackrel{\bullet}{m} = \alpha \ I^{1/3}; \quad v_{imp} = \beta \ I^{1/3} \ln\left(\frac{m_0}{m}\right)$$

To lowest order, the angular thickness distribution that gives uniform implosion velocity after acceleration is

$$\frac{\delta \tau(\theta)}{\langle \tau \rangle} \approx \frac{2}{3} \left[1 - \frac{1}{4} \frac{\langle d\tau \rangle_{ablation}}{\langle \tau \rangle} \right] \frac{\delta I(\theta)}{\langle I \rangle}$$

We can estimate what this means for typical OMEGA shots

$$22 \text{ kJ} \Rightarrow \left\langle d\tau \right\rangle_{ablation} \approx 10 - 12 \,\mu\text{m} \quad \Rightarrow \frac{\delta \tau(\theta)}{\langle \tau \rangle} \approx \frac{2}{3} \left[1 - \frac{3 \,\mu\text{m}}{\langle \tau \rangle} \right] \frac{\delta I(\theta)}{\langle I \rangle}$$
From data, we speculated
$$\frac{\delta \tau}{\langle \tau \rangle} \approx 20 \,\mu\text{m} \Rightarrow \frac{\delta \tau(\theta)}{\langle \tau \rangle} \approx 0.6 \,\frac{\delta I(\theta)}{\langle I \rangle}$$

$$\frac{\delta \tau}{\langle \tau \rangle} \approx \frac{1}{2} \frac{\delta I}{\langle I \rangle}$$

The shell thickness variation required to counterbalance a 10% intensity variation is

δ*T* ≈ 1.2 μm

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