### Optimization of Low-Order Uniformity for Polar Direct Drive (PDD) on the National Ignition Facility (NIF)



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## Optimized pulse shapes compensate 2-D effects due to nonuniform beam incident angles

 PDD enables direct-drive ignition experiments while the NIF is in the x-ray drive configuration.

- The 48 quads are logically grouped into three rings based on their incident angles: 26°, 59°, and 82°.
- Rings with different incident angles lead to variations around the target.
  - laser absorption
  - hydrodynamic efficiency
  - lateral heat and mass flow
- A nonlinear optimization algorithm within a feedback loop generates compensated ring pulse shapes.



- Description of ray-trace algorithm
- Description of feedback loop
- Description of target and 2-D DRACO simulation results

### PDD enables direct-drive-ignition experiments while the NIF is in the x-ray-drive configuration



**Caveats:** 

- Repointing the x-ray-drive ports leads to variations in incident angles.
- The equator requires the highest incident intensity to compensate for higher refraction losses, lower hydrodynamic efficiency, etc.
- 2-D effects also become important: lateral mass flow, lateral heat flow, etc.
- The "pointing" changes as the target compresses.

### Each sector of a *DRACO* simulation is driven by an angular spectrum of rays

• The spectrum changes as a function of polar angle due to the nonuniform overlap of beams in the PDD configuration.

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 The rays propagate and deposit energy as if each sector is 1-D; exact temperature and density profiles are used.



### The "open-loop" model optimizes the ring energy to minimize the nonuniformity of absorbed energy



#### The "closed-loop" model incorporates feedback to predict the required compensating pulse shapes



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• Supplies higher intensity to regions on target that require compensation.

### The optimized ring pulse shapes drive the shell with improved low- $\ell$ -mode nonuniformity



Radius converged by a factor of 6

#### Evidence of hot-spot formation is seen near the end of the deceleration phase

 $\rho ~(\textbf{g/cc})$ t = 9.02 ns AKev **yl** (μm) of the 8 KeV 10 KeV **xl** (µ**m**)

## The optimizer compensates for 2-D effects by increasing the equatorial drive relative to the pole

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### The "closed-loop" model shows a dramatic improvement for $\ell = 2$

60  $\ell$  mode = 2 50 **Amplitude** (µm) 40 Without feedback 30 20 10 With feedback 0 6 7 0 2 3 5 Δ Time (ns)

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# The angular spectrum in the direct-drive configuration is more evenly distributed than PDD



### Feedback gains are selected using the following prescription\*



- Kd and Ki are set to 0
- Kp is varied until oscillation breaks out; note Kcr and Pcr
- Kp = 0.6 Kcr
- Ki = Kp/(0.5  $\times$  Pcr)
- Kd = Kp  $(0.125 \times Pcr)$

<sup>\*</sup>Ziegler-Nichols tuning rules, K. Ogata, *Modern Control Engineering*, 3rd ed. (Prentice Hall, New Jersey, 1997), pp. 672–674.

Summary/Conclusions

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