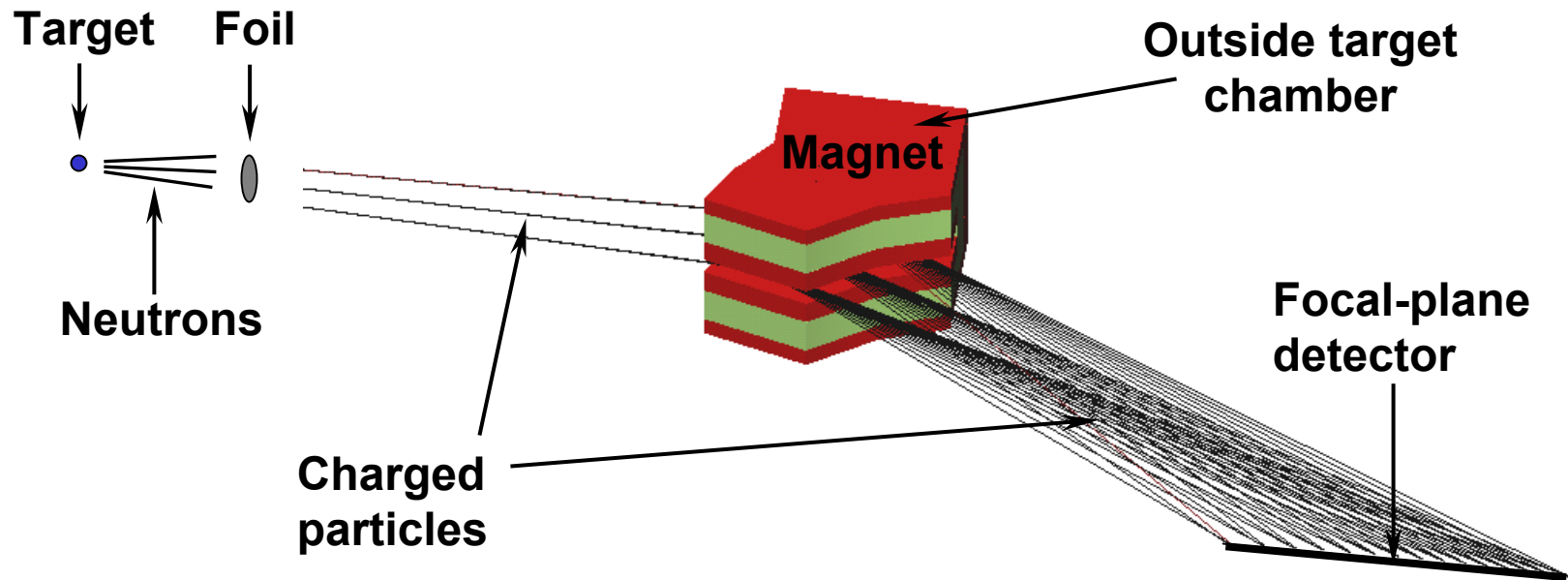


# A Magnetic Recoil Spectrometer (MRS) for precise $\rho R_{fuel}$ and $T_i$ measurements of warm and cryo targets at OMEGA and the NIF



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45<sup>th</sup> Annual Meeting of the  
Division of Plasma Physics  
Albuquerque , NM  
October 27-31, 2003

# Collaborators

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# Abstract

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**A method for determining  $\rho R_{\text{fuel}}$  of cryogenic deuterium-tritium plasmas involves measurement of the energy spectrum of elastically-scattered, primary neutrons. A spectrometer has been designed for doing this at OMEGA and the NIF, using scattered neutrons in the energy range 7-10 MeV to determine  $\rho R_{\text{fuel}}$  and primary neutrons to measure  $T_i$ . The instrument utilizes a magnet and a conversion foil for production of charged particles. A large dynamic range ( $>10^6$ ) will allow operation at yields as low as  $10^{12}$ . This will allow  $\rho R_{\text{fuel}}$  and  $T_i$  measurements of warm and cryogenic DT targets at OMEGA, and fizzle and ignited cryogenic DT targets at the NIF.**

This work was supported in part by the US DoE (contract W-7405-ENG-48 with LLNL, grant DE-FG03-99DP00300 and Cooperative Agreement DE-FC03-92SF19460), LLE (subcontract P0410025G), and LLNL (subcontract B313975).



# MRS strengths at OMEGA and the NIF

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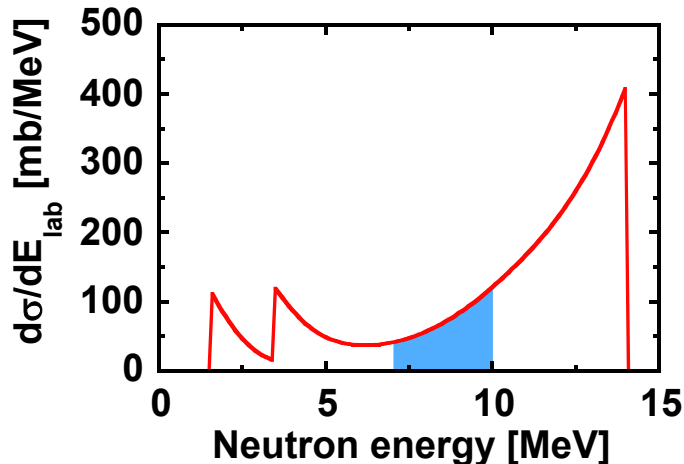
- $\rho R_{\text{fuel}}$  of warm, fizzle and ignited implosions can be measured at the NIF, and similarly for warm and cryo DT at OMEGA.
- Large dynamic range is achievable. ( $Y_{1n} \sim 10^{12} - 10^{19}$ )
- Flexible instrument:
  - Two different types of detectors can be used.
  - Recoils of either p or d can also be used.
- Authenticate the data through the primaries.
- A trade off can be made between high resolution and high efficiency, depending on exp.
- Large signal-to-background ratio for most applications.
- Wide-band spectrometer (6-24 MeV p); (3-12 MeV d).
- High-resolution spectrometer ( $\Delta E_1/E = 1.8\%$ ).

# $\rho R_{\text{fuel}}$ can be determined by measuring number of primary neutrons elastically scattered ( $Y_{\text{scatt}}$ ) from fuel ions

The relationship between  $\rho R_{\text{fuel}}$  and  $Y_{\text{scatt}}$  is

$$\rho R_{\text{fuel}} = \frac{(2\gamma + 3)m_p}{(\gamma\sigma_d + \sigma_t)} \frac{Y_{\text{scatt}}}{Y_{1n}} \quad (1)$$

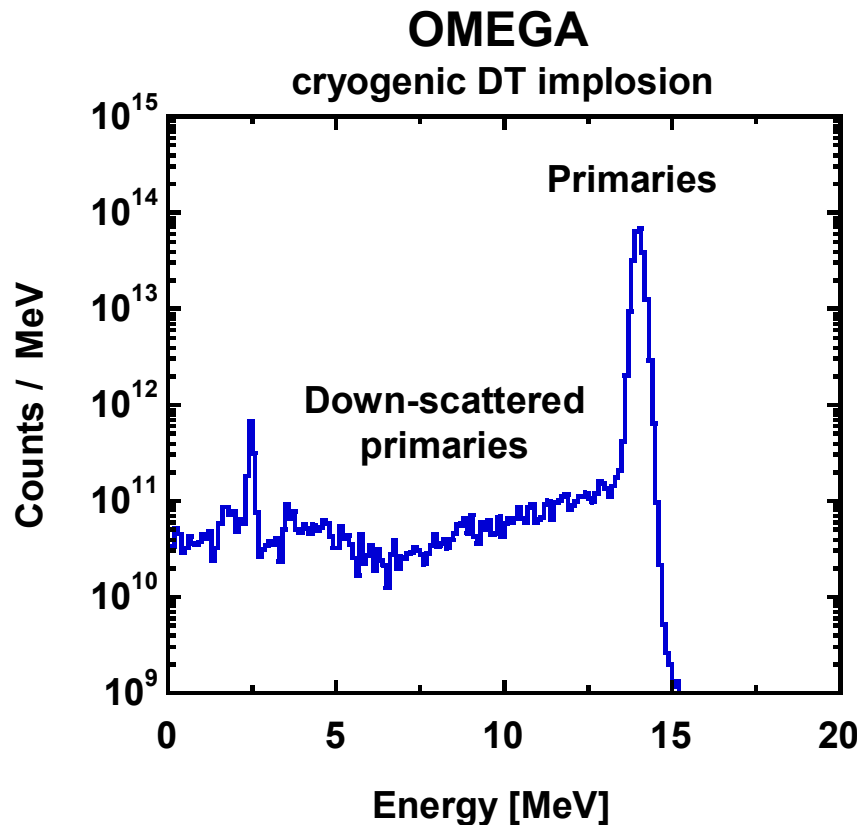
$m_p$  = protons mass,  $\gamma = n_d/n_t$ ,  $\sigma_d$  ( $\sigma_t$ ) = elastic cross section for deuterons (tritons), and  $Y_{1n}$  is primary yield. For specificity, we'll focus on the energy range 7 to 10 MeV for the scattered neutrons); the total cross sections used in Eq. (1) must then be replaced by the effective cross sections for generating scattered neutrons in this energy range.



$$\rho R_{\text{fuel}} \approx 40 \frac{Y_{\text{scatt}}}{Y_{1n}} \quad [\text{g/cm}^2] \quad (2)$$

# Nature of relevant neutron spectra at OMEGA and NIF

To illustrate the nature of relevant spectra, and to provide a basis for evaluating the practical utility of the MRS on OMEGA and the NIF, following spectra were used in this work.



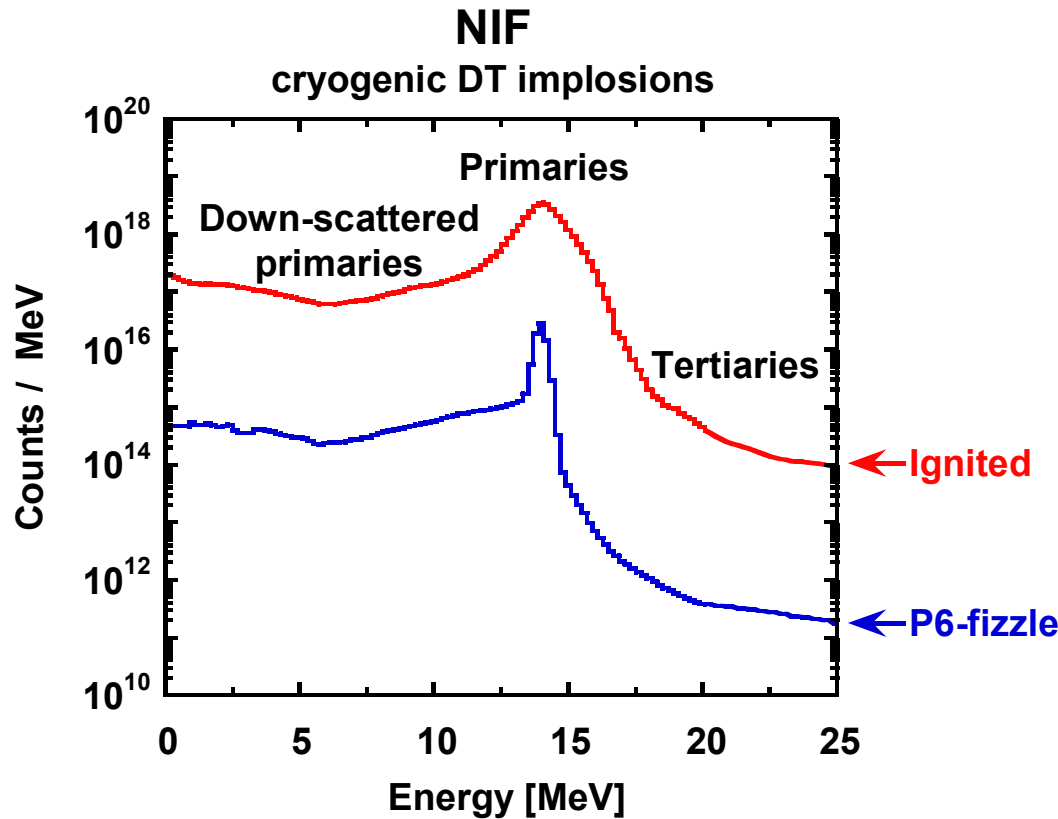
$$\rho R_{\text{fuel}} = 128 \text{ mg/cm}^2$$

$$Y_{1n} = 2.3 \times 10^{13}$$

$$Y_{\text{scatt}} (7-10 \text{ MeV}) = 1.3 \times 10^{11}$$

Calculated by Steve Hatchett

## Nature of relevant neutron spectra at OMEGA and NIF, continued



**Ignited**

$$\rho R_{\text{fuel}} = 1850 \text{ mg/cm}^2$$

$$Y_{1n} = 7.4 \times 10^{18}$$

$$Y_{\text{scatt}} (7-10 \text{ MeV}) = 3.2 \times 10^{17}$$

**P6-fizzle**

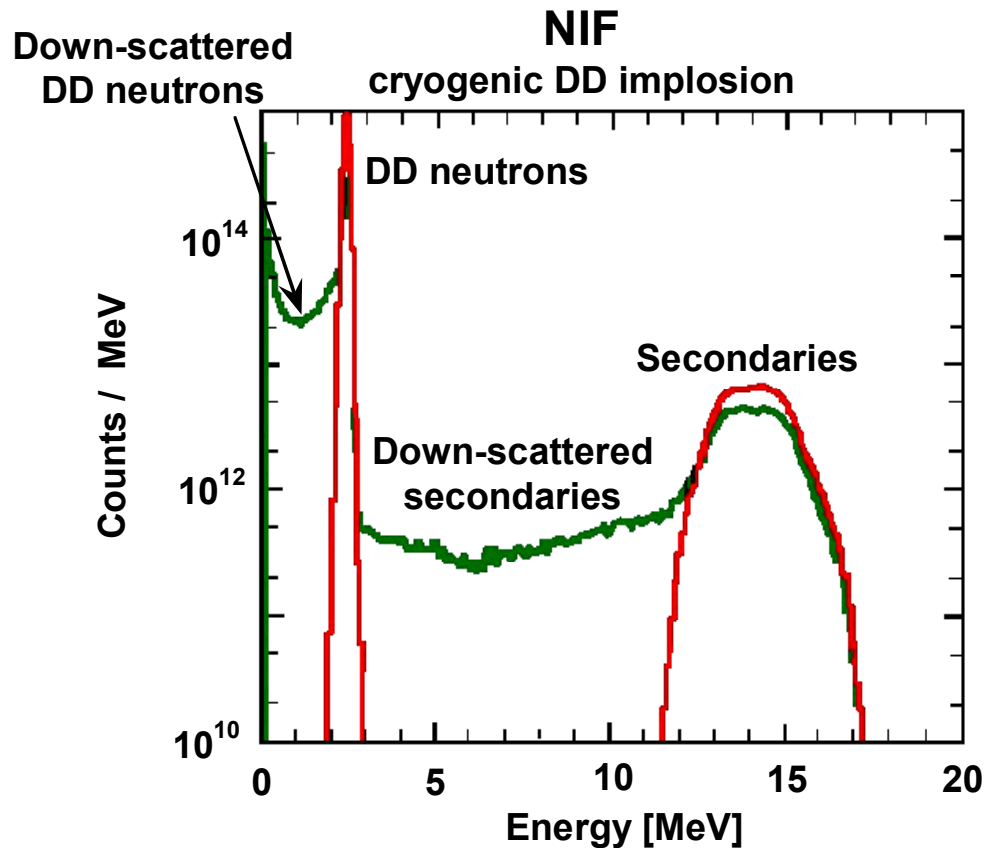
$$\rho R_{\text{fuel}} \sim 2000 \text{ mg/cm}^2$$

$$Y_{1n} = 2.1 \times 10^{16}$$

$$Y_{\text{scatt}} (7-10 \text{ MeV}) = 1.3 \times 10^{15}$$

Calculated by Steve Haan

## Nature of relevant neutron spectra at OMEGA and NIF, continued



$$\rho R_{\text{fuel}} = 1500 \text{ mg/cm}^2$$

$$Y_{1n} = 2 \times 10^{14}$$

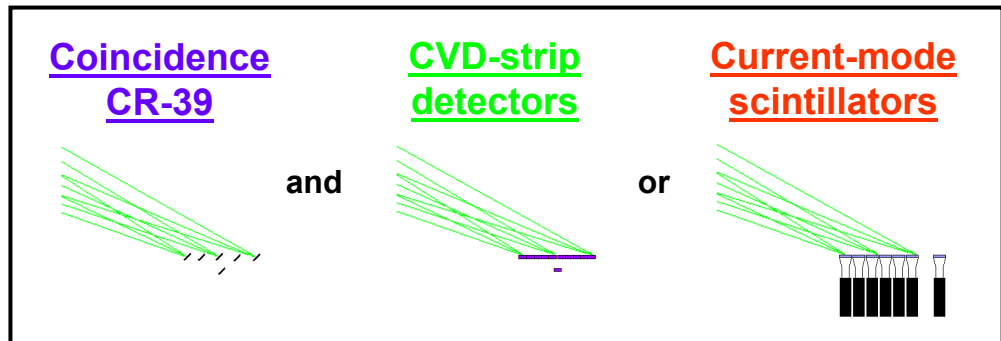
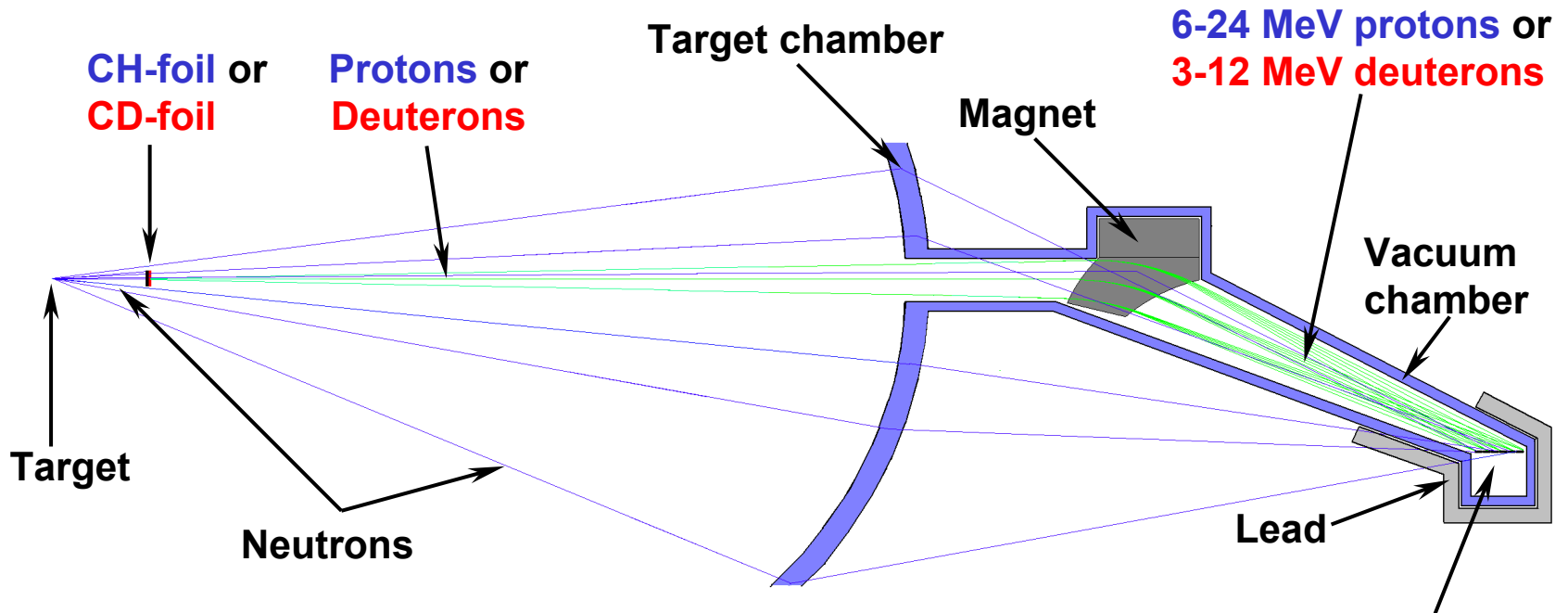
$$Y_{2n} = 2 \times 10^{13}$$

$$Y_{\text{scatt}} (7\text{-}10 \text{ MeV}) = 1.2 \times 10^{12}$$

Calculated by Steve Hatchett



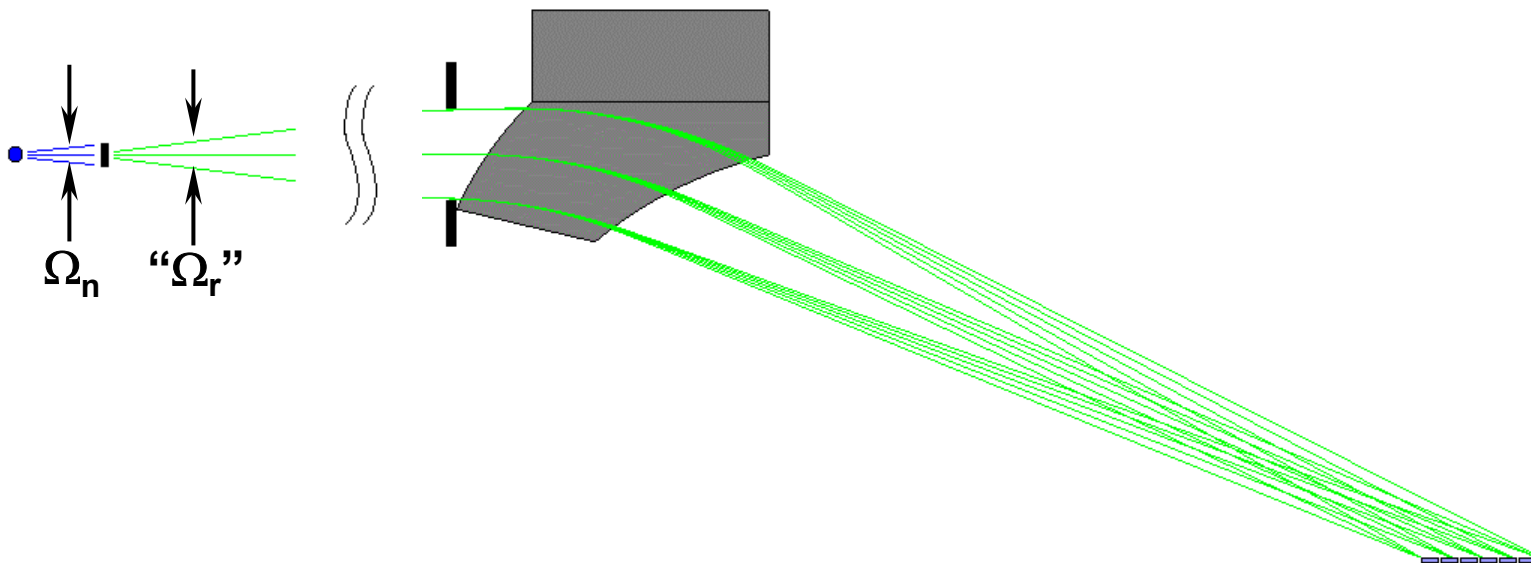
# MRS principle



# MRS principle - Detection efficiency ( $\varepsilon_n$ )

- The detection efficiency can be expressed as

$$\varepsilon_n \propto \Omega_n \int^{\Omega_r} \frac{d\sigma}{d\Omega_{lab}} d\Omega$$



- Maximum differential cross section at forward scattering angles, focusing aspects and large aperture significantly enhances  $\varepsilon_n$ .

## MRS principle - Resolution ( $\Delta E_I$ )

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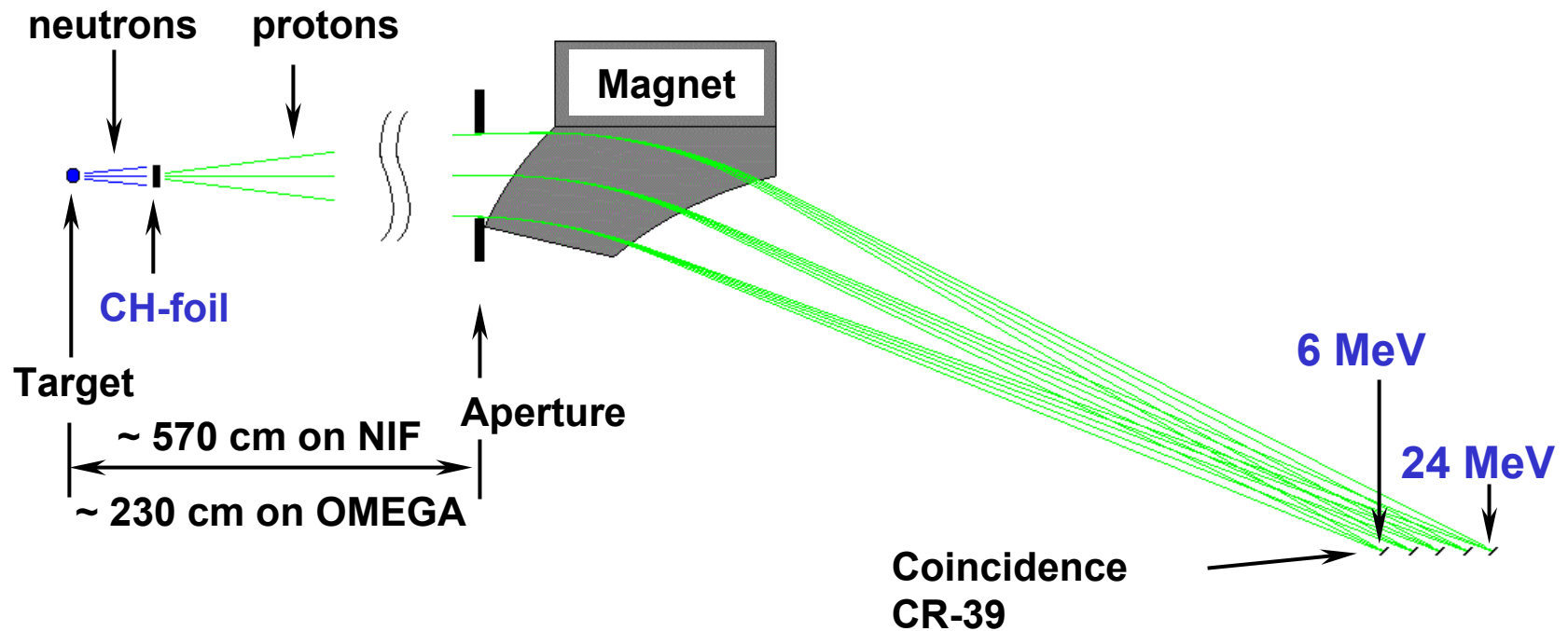
- Resolution ( $\Delta E_I$ ) of the spectrometer is defined as the energy distribution at the focal plane when viewing a fluence of mono-energetic neutrons. The resolution can be written as

$$\Delta E_I \approx \sqrt{\Delta E_f^2 + \Delta E_k^2 + \Delta E_s^2}$$

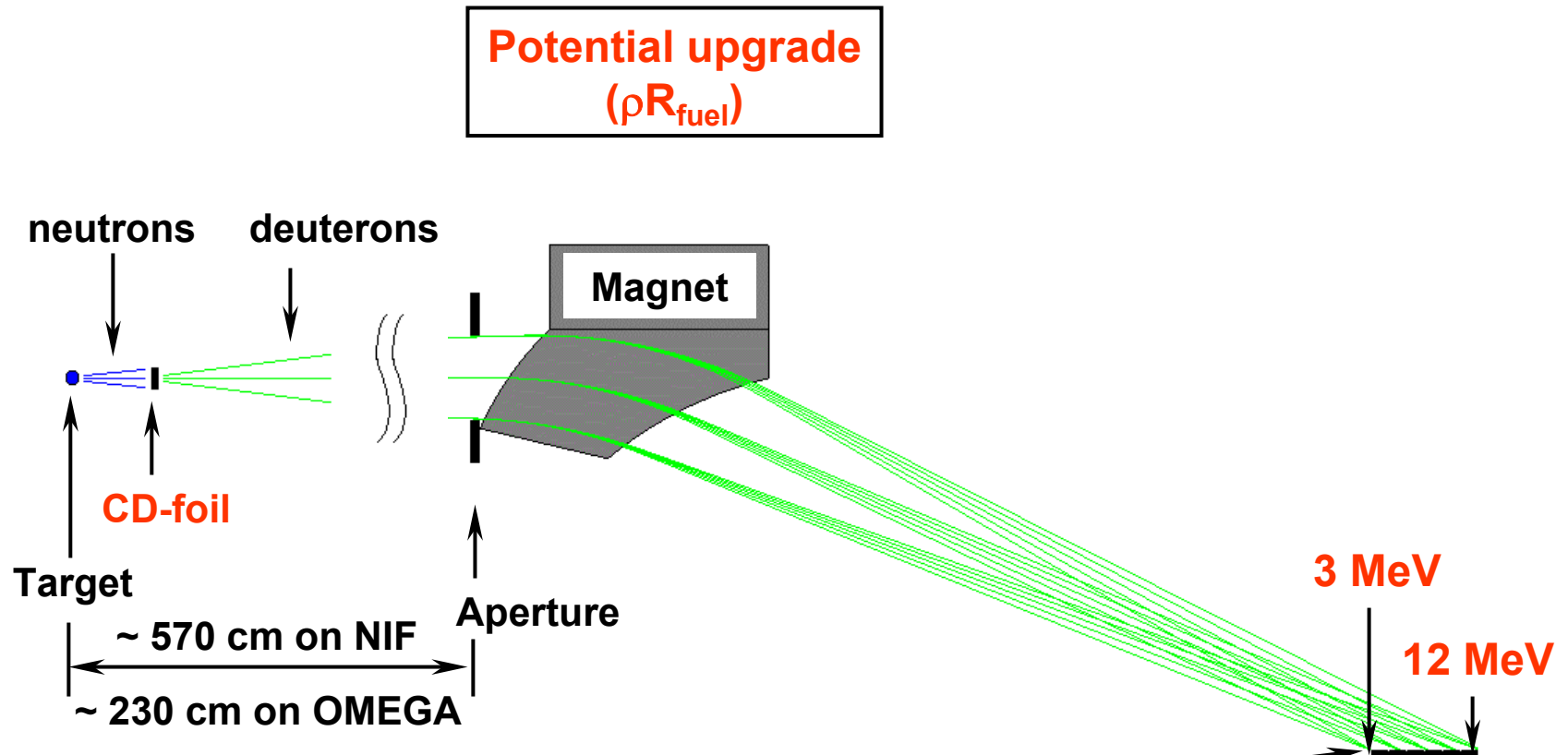
$\Delta E_f$	=	Energy loss in foil	$\propto$	foil thickness
$\Delta E_k$	=	Kinematic energy broadening	$\propto$	foil and aperture size
$\Delta E_s$	=	Ion optical energy broadening	$\propto$	magnet performance

# Design philosophy

Initial and potentially the final implementation  
( $\rho R_{\text{fuel}}$  and  $T_i$ )

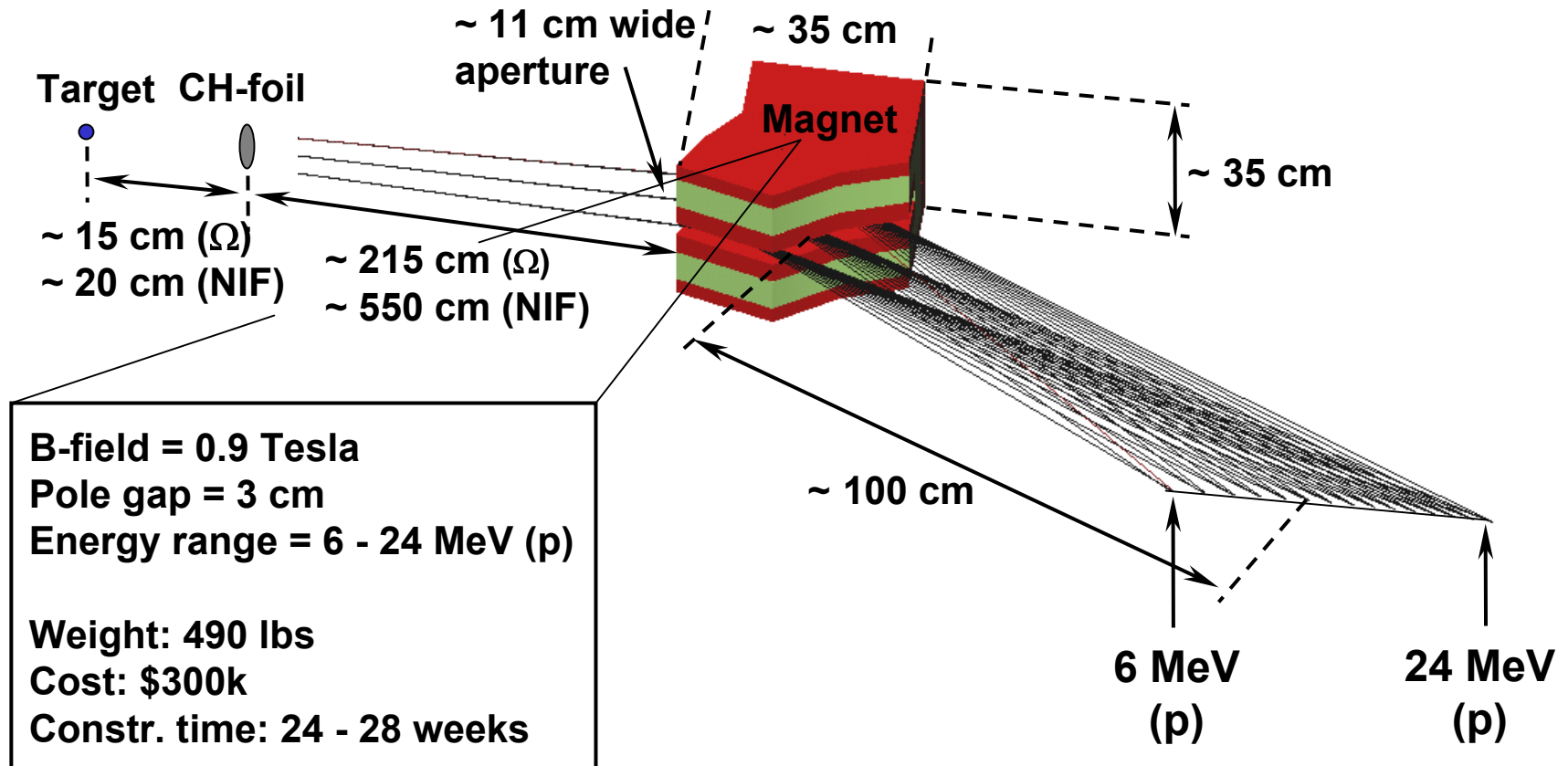


# Design philosophy



1. Coincidence CR-39
2. CVD detectors or Current-mode scintillators

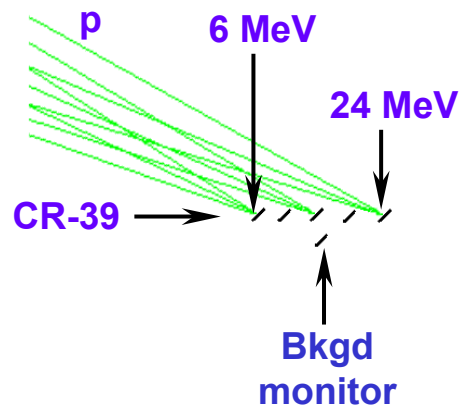
# Design of the MRS at OMEGA and the NIF



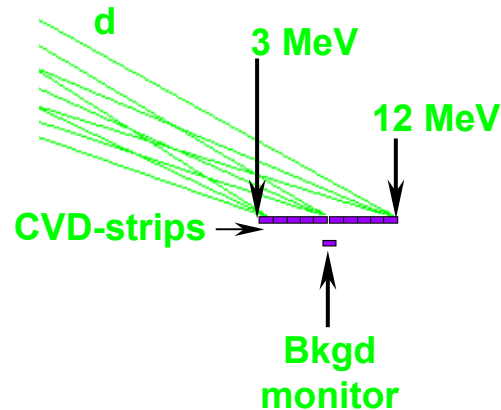
J. A. Frenje et al., Rev. Sci. Instrum. 72 (2001) 854.

# We will develop coincidence CR-39 and one of two electronic detector systems

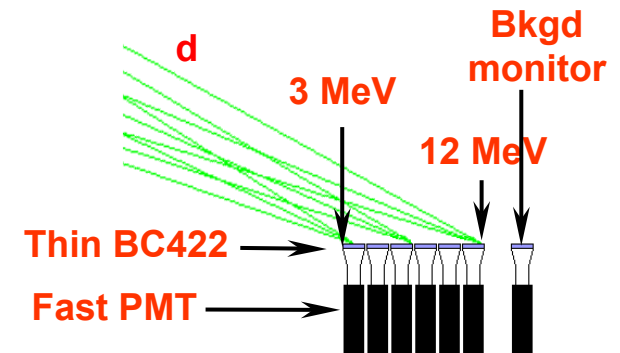
## Coincidence CR-39



## CVD-strip detectors



## Current-mode scintillators



# We will develop coincidence CR-39 and one of two electronic detector systems

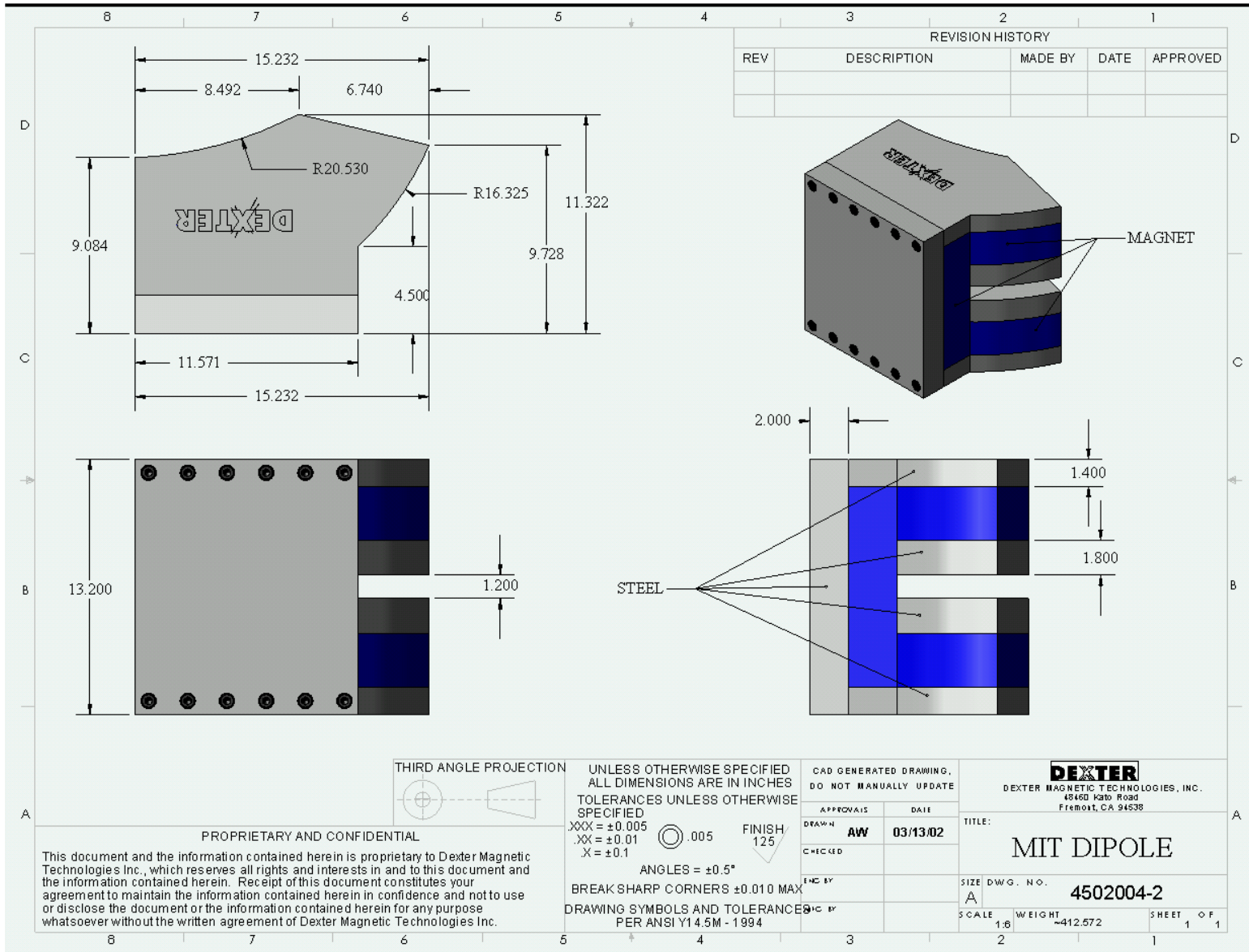
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<b>Detector</b>	<b>Advantages</b>	<b>Disadvantages</b>
<b>Coincidence CR-39**</b>	<b>Totally insensitive to EMP, X-rays &amp; <math>\gamma</math>-rays Shielding not required Robust technology</b>	<b>9-12 hour turn around</b>
<b>CVD-strip detector</b>	<b>Large dynamic range Fast Insensitive to <math>\gamma</math>'s Radiation hardened</b>	<b>Sensitive to EMP</b>
<b>Current-mode scintillator</b>	<b>Fast Well-known technology</b>	<b>Sensitive to <math>\gamma</math>' Sensitive to EMP</b>

**\*\* At Vulcan, only CR-39, radiochromic film, and film can be reliably used.**

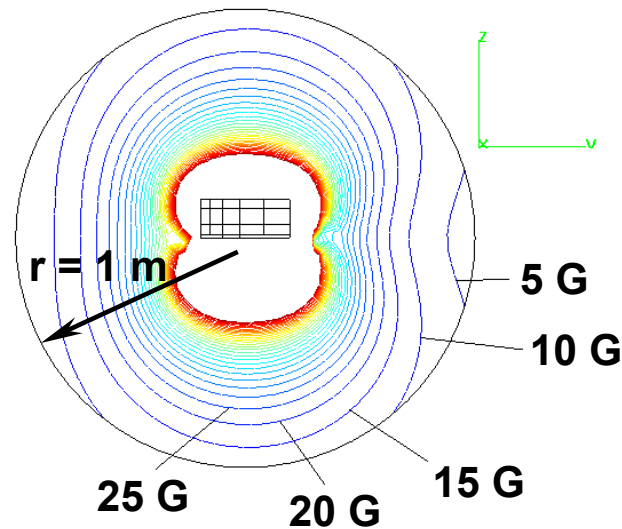
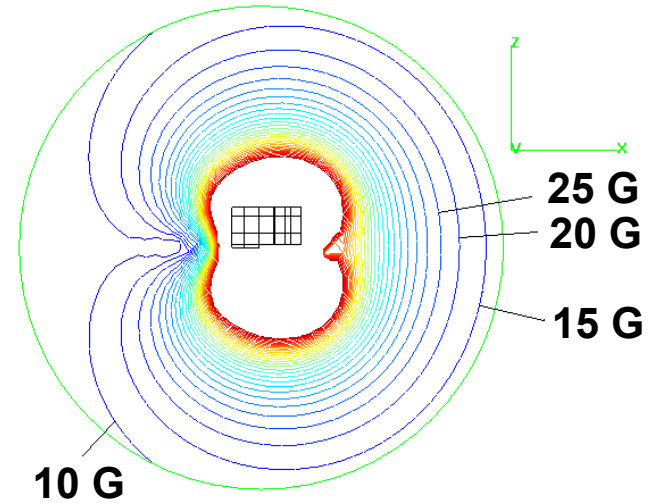
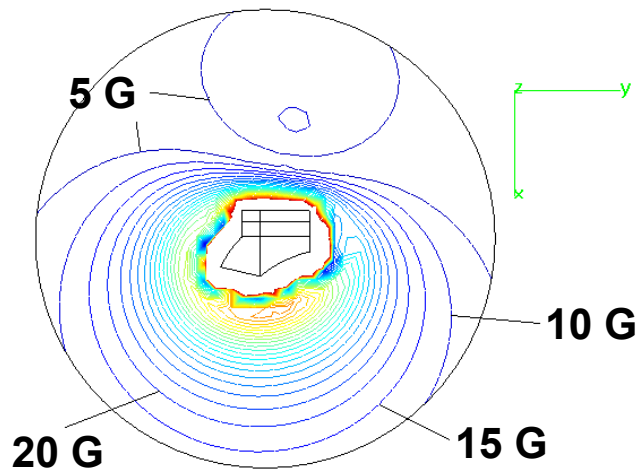
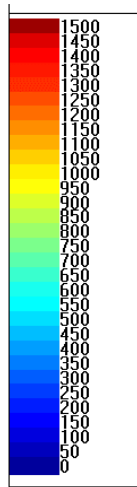


# MRS-conceptual design



# External B-fields from MRS are negligible

B [Gauss]

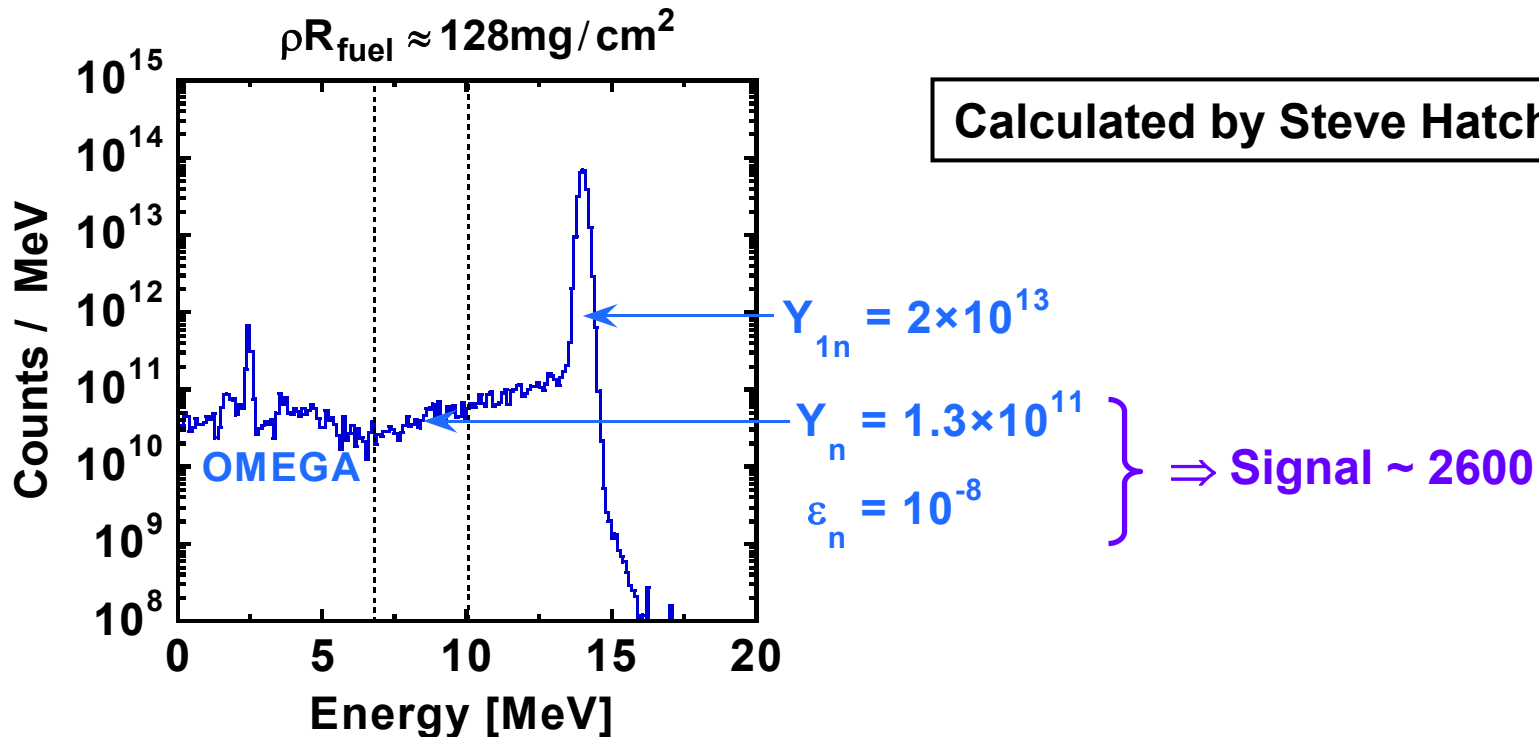


## Performance of MRS at OMEGA and the NIF

Facility	Type of measurement	Foil	$\varepsilon_n$	$\Delta E_1$ [keV]
OMEGA	$\rho R_{\text{fuel}} \& T_i$	CH	$5 \times 10^{-10}$	250
“	$\rho R_{\text{fuel}} \& T_i$	“	$6 \times 10^{-9}$	3000
“	$\rho R_{\text{fuel}}$	CD	$8 \times 10^{-10}$	250
“	$\rho R_{\text{fuel}}$	“	$1 \times 10^{-8}$	3000

At the NIF,  $\varepsilon_n$  is about one order of magnitude smaller for the same  $\Delta E_1$ .

# Predicted signal (S) for $\rho R_{fuel}$ measurements of a cryo DT target at OMEGA



- How many photons are produced in the thin BC422 scintillator (0.25 mm thick) by these 2600 fully stopped deuterons?

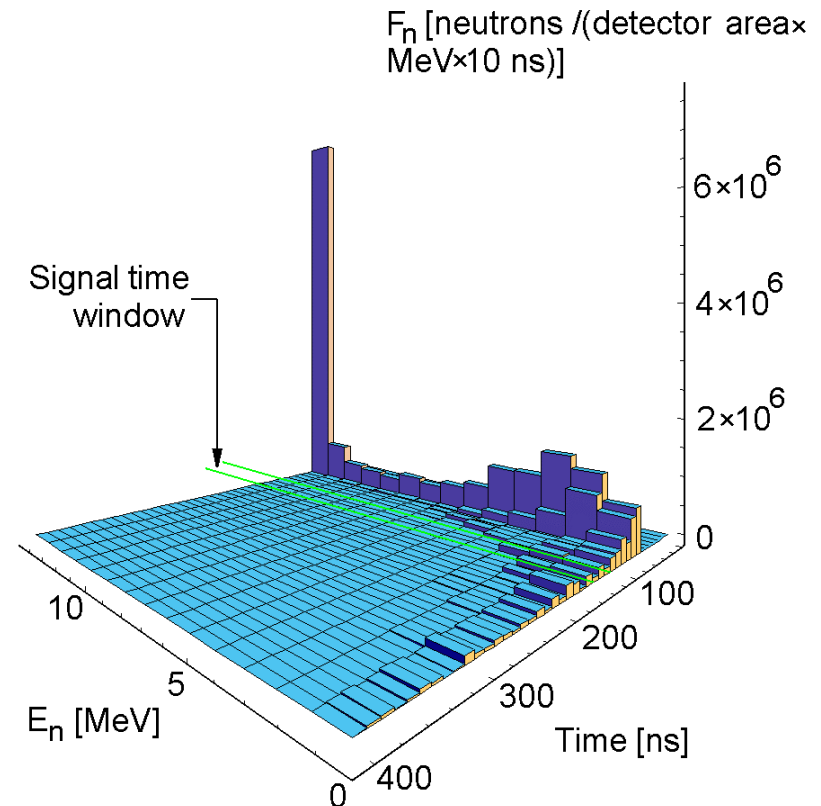
$$S \sim \frac{2600 \times 2 \text{ MeV}_{ee}}{100 \text{ eV/photon}} \sim 5 \times 10^7 \text{ photons}$$

# Predicted Background (B) for $\rho R_{fuel}$ measurements of a cryo DT target at OMEGA

## Background (B)

- Neutron transport codes COG and TART2000 were used to predict neutron flux and spectrum at detector.

- About  $5 \times 10^5$  neutrons ( $E_n = 0 - 4$  MeV) pass the detector in the signal time window (which is about 55 – 81 ns after the primary neutrons hit the detector).



Calculated by Greg Schmid

# Predicted S/B ratio for $\rho R_{fuel}$ measurements of a cryo DT target on OMEGA

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- About 1800 neutrons interact with the scintillator.
- A benchmarked Monte Carlo code predicted total number of produced photons by modeling scintillator geometry and response to the neutrons.

$$B \sim \frac{1800 \times 0.2 \text{ MeV}_{ee}}{100 \text{ eV/photon}} \sim 3.6 \times 10^6 \text{ photons}$$

$$\Rightarrow \boxed{S/B \sim \frac{5 \times 10^7}{3.6 \times 10^6} \sim 14}$$

$$\boxed{\frac{S}{B} \propto \frac{\rho R_{fuel} \times Y_{1n}}{Y_{1n}} = \rho R_{fuel}}$$

## Predicted signal-to-background (S/B) ratio for the different measurements at OMEGA and the NIF

Implosion	$\rho R_{fuel}$ [mg/cm <sup>2</sup> ]	Facility	S/B (CR-39)	S/B (BC422)
Warm DT	~ 30*	OMEGA	~ 14	~ 9
Cryo DT	~ 128	OMEGA	~ 27	~ 14
Warm DT	~ 30*	NIF	~ 6	~ 9
Cryo DT P2-fizzle (9x10 <sup>14</sup> )	~ 1500	NIF	~ 112	~ 170
Cryo DT P6-fizzle (9x10 <sup>14</sup> )	~ 2000	NIF	~ 113	~ 220
Ignited (9x10 <sup>14</sup> )	~ 1850	NIF	~ 79	~ 205
Cryo D <sub>2</sub>	~ 1500	NIF	~ 2	~ 200

## The remaining detected background can be separately characterized...

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- by moving the foil out of the spectrometer line of sight.
- by background monitors beside the focal plane detector.



# Accuracy analysis of $\rho R_{fuel}$ measurements using the MRS at OMEGA

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The relative statistical uncertainty in the number of measured signal events (S), which are generated by down-scattered neutrons, can be expressed as

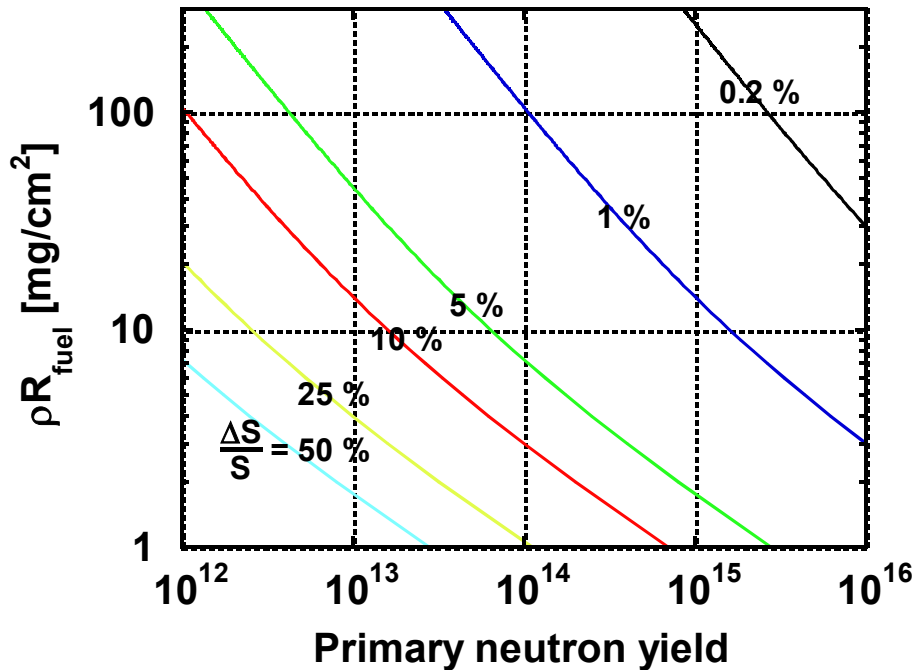
$$\frac{\Delta S}{S} = \sqrt{\frac{\rho R_{fuel} + 6}{10^{-12} \rho R_{fuel}^2 Y_{1n}}} \quad (2)**$$

when operating the MRS at  $\Delta E_i = 3000$  keV.  $\rho R_{fuel}$  is given in mg/cm<sup>2</sup>. Eq. (2) can be rewritten as

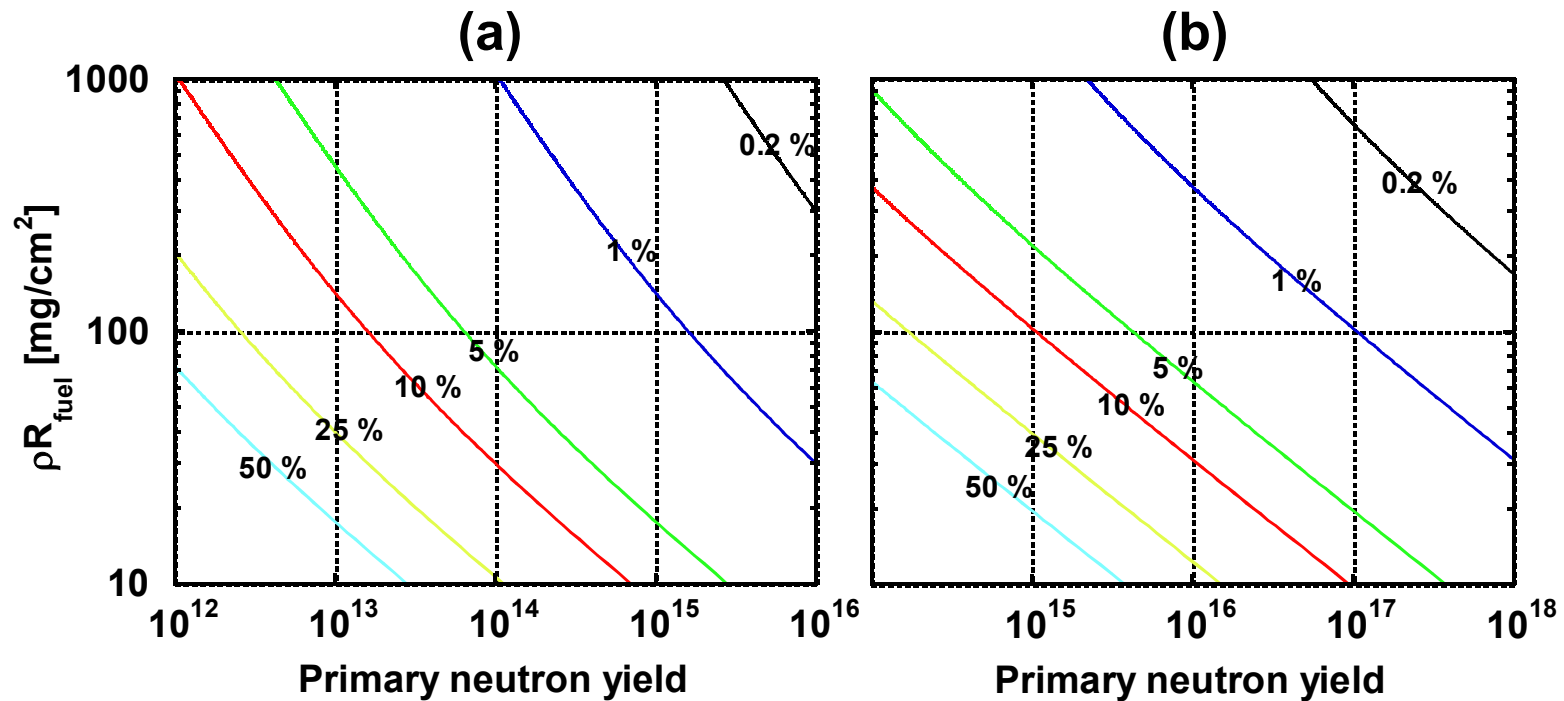
$$\rho R_{fuel} = \frac{1}{2 \times 10^{-12} Y_{1n} \left(\frac{\Delta S}{S}\right)^2} + \sqrt{\left(\frac{1}{2 \times 10^{-12} Y_{1n} \left(\frac{\Delta S}{S}\right)^2}\right)^2 + \frac{6}{2 \times 10^{-12} Y_{1n} \left(\frac{\Delta S}{S}\right)^2}} \quad (3)$$

\*\* Eq. (2) assumes that S/B scales linearly with  $\rho R_{fuel}$ , which is the case for electronic detection.

# $\rho R_{\text{fuel}}$ vs Yield at OMEGA for different $\Delta S/S$ when operating the MRS at $\Delta E_1 = 3000$ keV

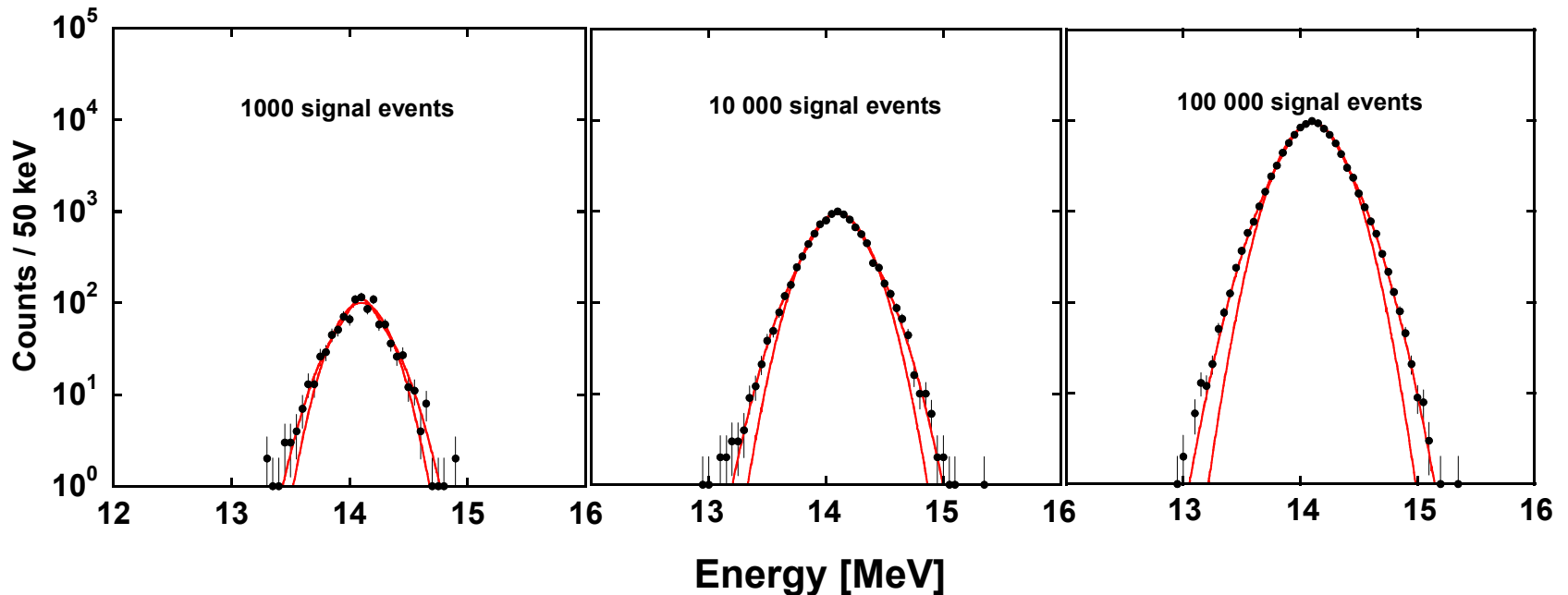


# $\rho R_{\text{fuel}}$ vs Yield at NIF for different $\Delta S/S$ when operating the MRS at $\Delta E_1 = 3000$ keV (a), and $\Delta E_1 = 250$ keV (b)



# Using the CH-foil, the MRS can measure deviations from Maxwellian distributions when operated at $\Delta E_i = 250$ keV

A hot spot at 10 keV and surrounding cold plasma at 2 keV was assumed.  
(A model was used which resulted in comparable yields from the two regions.)



# $T_i$ measurement is affected by $\Delta E_i$ , $\Delta E_D$ and number of counts in spectrum

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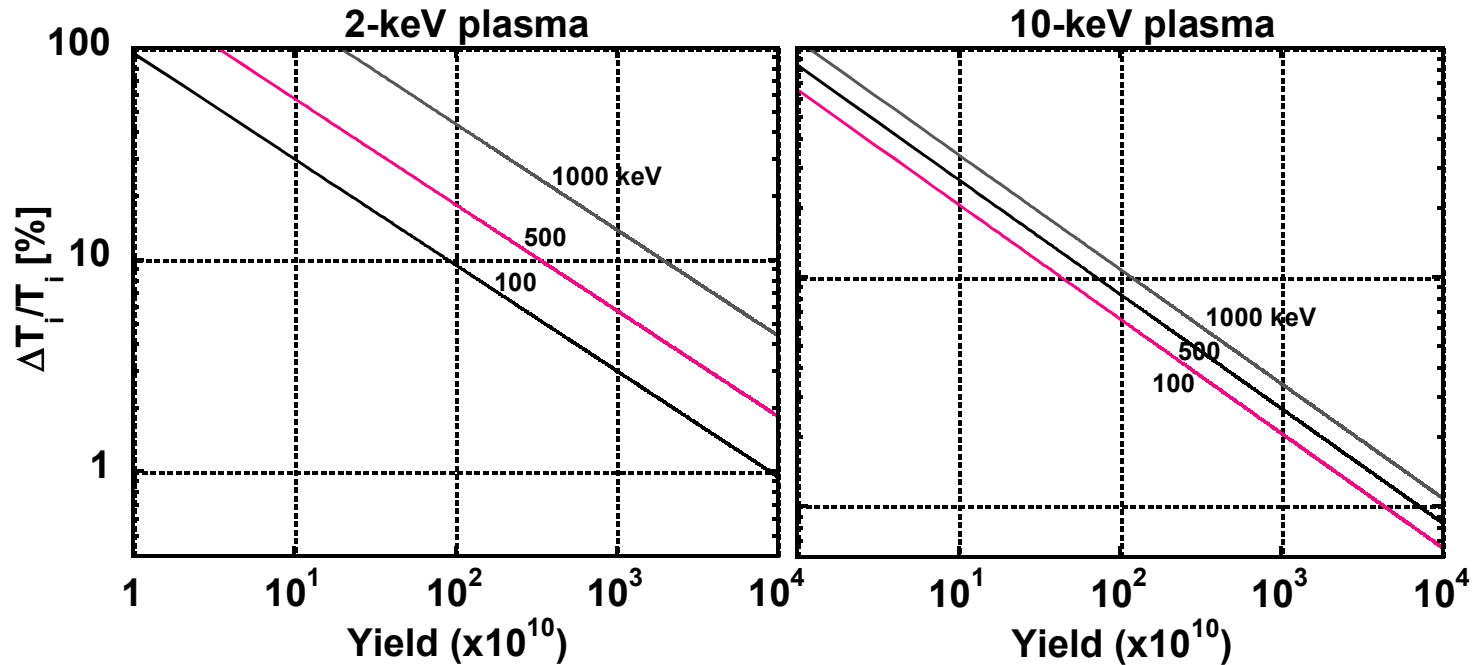
The relative statistical uncertainty in the  $T_i$  measurement can be expressed as

$$\frac{\Delta T_i}{T_i} = \left[ 1 + \left( \frac{\Delta E_i}{\Delta E_D} \right)^2 \right] \sqrt{\frac{2}{N}} \quad (1) **$$

$\Delta E_i$  is the instrumental response function,  $\Delta E_D$  is the Doppler broadening, and  $N$  is the number of counts in the spectrum.

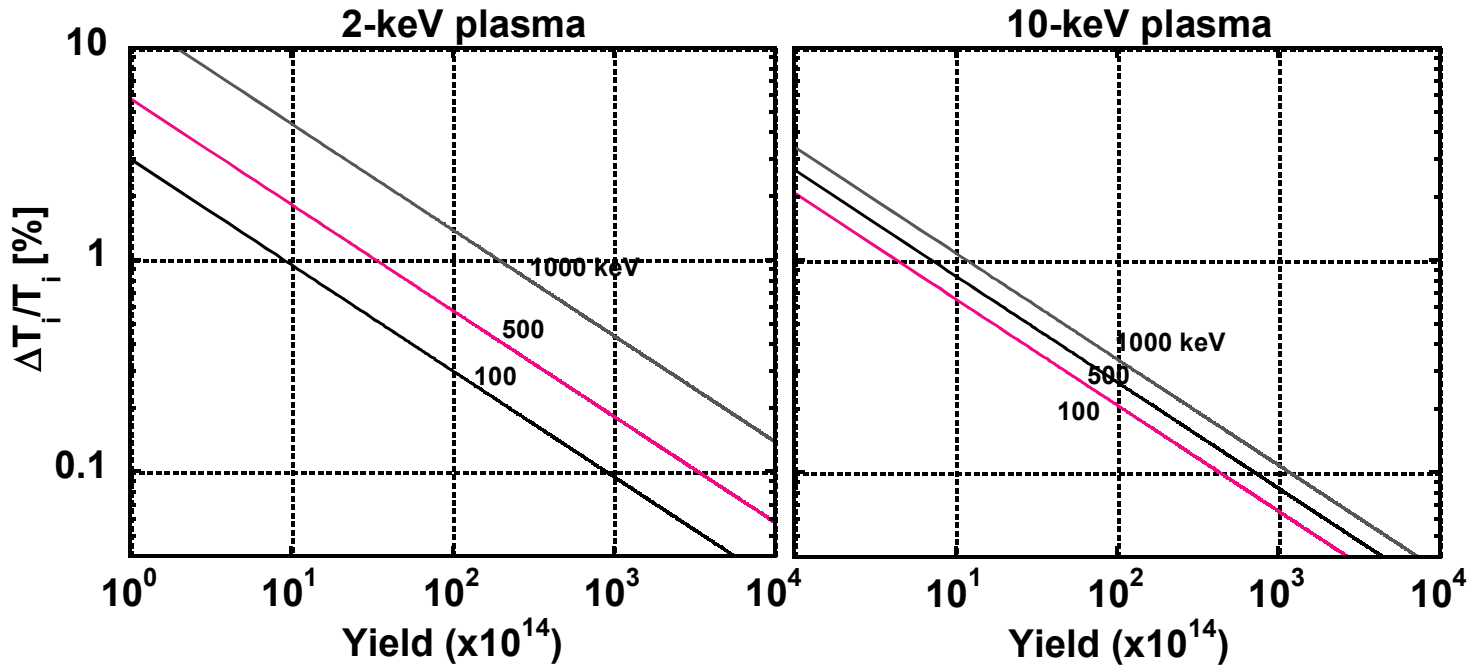
\*\* Eq. (1) assumes that the spectrometer response function is characterized very well, ie,  $\Delta(\Delta E_i) = 0$ . The equation also assumes that background is negligibly small.

# $\Delta T_i/T_i$ vs Yield at OMEGA for different $\Delta E_i$



$$\frac{\Delta T_i}{T_i} = \left[ 1 + \left( \frac{\Delta E_i}{\Delta E_D} \right)^2 \right] \sqrt{\underbrace{\frac{2}{3.3 \times 10^{-10} \text{Yield} \frac{\Delta E_D}{100 \text{keV}}}}_{= N}}$$

# $\Delta T_i/T_i$ vs Yield at the NIF for different $\Delta E_i$



$$\frac{\Delta T_i}{T_i} = \left[ 1 + \left( \frac{\Delta E_i}{\Delta E_D} \right)^2 \right] \sqrt{\underbrace{\frac{2}{3.3 \times 10^{-11} \text{Yield} \frac{\Delta E_D}{100 \text{keV}}}}_{= N}}$$