Modeling the Effects Mix at the Hot Spot Surface in 1-D Simulations of Cryogenic All-DT Ignition Capsule Implosions



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Summary

1-D modeling of a cryogenic, all-DT ignition capsule approximates the expected modifications of ignition by mix at the hot-spot surface

- The mix model includes the transport of target constituents, thermal energy, momentum, and turbulent energy within the mix region.
- Applying this model to an all-DT ignition capsule shows familiar mix effects on gain, the size of the hot spot, and their sensitivity to the known perturbation sources.
- The results of 2-D hydrodyamic simulation can be approximated reasonably well, considering the simplicity and economy of the 1-D model.



- The diffusive in-line mix model in *LILAC*
- Modification of pre-ignition conditions
- Consistency with 2-D simulations
- Application: gain sensitivity
- Conclusions

The mix model treats mix as a diffusion transport mechanism within the 1-D hydrocode *LILAC*

- Mix regions evolve from initial surface and drive perturbations according to the saturable multimode perturbation model of Haan.¹
- Perturbation growth rates are obtained from the Betti formula² for the ablation surface and from a variational method³ for the vapor-ice interface with ablative stabilization at both surfaces.
- Mix transport is modeled as diffusion based on a diffusion coefficient obtained from the perturbation spectrum

$$\sigma = \alpha \mathbf{v}_{mix} \lambda \frac{4(\mathbf{r}_{b} - \mathbf{r}_{s})(\mathbf{r} - \mathbf{r}_{s})}{(\mathbf{r}_{b} - \mathbf{r}_{s})^{2}} \qquad \mathbf{v}_{mix} = \frac{d}{dt} |\mathbf{r}_{b} - \mathbf{r}_{s}| \qquad \lambda^{-2} = \left\langle \left(\frac{\ell}{R}\right)^{2} \right\rangle_{\ell}$$

- The hydrodynamic model includes turbulent pressure and viscosity P_T and $\mathsf{Q}_T.^4$

$$\rho \frac{dv}{dt} = -\frac{\partial}{\partial r} \left(\mathbf{P} + \mathbf{Q} + \mathbf{P}_{T} + \mathbf{Q}_{T} \right)$$

- 1. S. W. Haan, Phys. Rev. A <u>39</u>, 5812 (1989).
- 2. R. Betti et al., Phys. Plasmas 5, 1446 (1998).
- 3. K. O. Mikaelian, Phys. Rev., A 33, 1216 (1986).
- 4. C. E. Leith, UCRL-96036 (1986).

Mix motion energy is computed as turbulent energy in a "k- λ " model

• Turbulent energy density k:

$$\mathbf{P}_{\mathbf{T}} = \frac{2}{3}\rho\mathbf{k}, \quad \mathbf{Q}_{\mathbf{T}} = -\frac{4}{3}\frac{\sigma\rho^2}{\beta_q}\frac{\partial\mathbf{v}}{\partial\mathbf{m}}, \quad \sigma = \upsilon_{\text{mix}}\lambda \qquad (\beta_q = 1.0)$$

Buoyant force as source of k:

$$S = max \left(u \frac{dv}{dt}, 0 \right), \quad u = -\frac{\sigma}{\beta_m} \frac{\partial \rho}{\partial m}$$
 ($\beta_m = 0.7$)

• Dissipation rate:

$$\varepsilon = \mathbf{c}_{\varepsilon} \, \frac{\mathbf{k}^{3/2}}{\lambda} \tag{C}_{\varepsilon} = \mathbf{0.09}$$

• Evolution:

$$\frac{d\mathbf{k}}{dt} = \frac{\partial}{\partial \mathbf{m}} \left(\rho^2 \frac{\sigma}{\beta_k} \frac{\partial \mathbf{k}}{\partial \mathbf{m}} \right) - \left(\mathbf{P}_T + \mathbf{Q}_T \right) \frac{\partial \mathbf{v}}{\partial \mathbf{m}} + \mathbf{S} - \epsilon \qquad (\beta_k = 0.715)$$
$$\frac{d\mathbf{e}_i}{dt} = \frac{\partial}{\partial \mathbf{m}} \left(\rho^2 \frac{\sigma}{\beta_e} \frac{\partial \mathbf{e}_i}{\partial \mathbf{m}} \right) - \left(\mathbf{P} + \mathbf{Q} \right) \frac{\partial \mathbf{v}}{\partial \mathbf{m}} + \epsilon - \mathbf{S} + \dots \text{ etc} \qquad (\beta_e = 0.9)$$

Mix-enhanced thermal transport reduces ignition yield by reducing the size and temperature of the hot spot



Gain reduction depends on an effective nonuniformity of the ice/vapor interface, similar to 2-D simulation results



As expected, mix transport delays ignition and reduces the implosion energy margin

Margin = percent of peak inward kinetic energy remaining at ignition



The sensitivity of the gain to variations in the perturbation sources indicates their relative importance



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