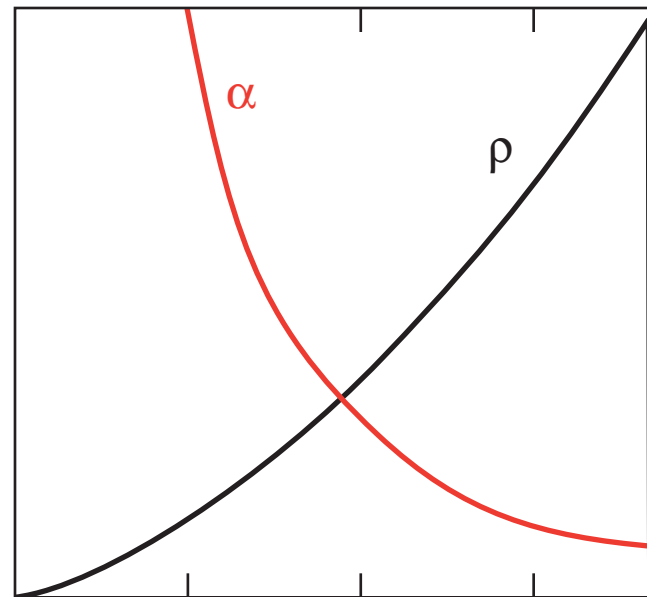


Adiabat Shaping of Direct-Drive OMEGA Capsules Using Ramped Pressure Profiles



Lagrangian coordinate

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Motivation

- A shaped adiabat combines
 1. High capsule adiabat at the ablation front, resulting in high ablative stabilization of the Raleigh–Taylor (RT) instability:¹

$$\gamma_{RT} \approx 0.94 \sqrt{kg} - 2.7 kV_{abl}, V_{abl} \sim \alpha^{3/5}$$

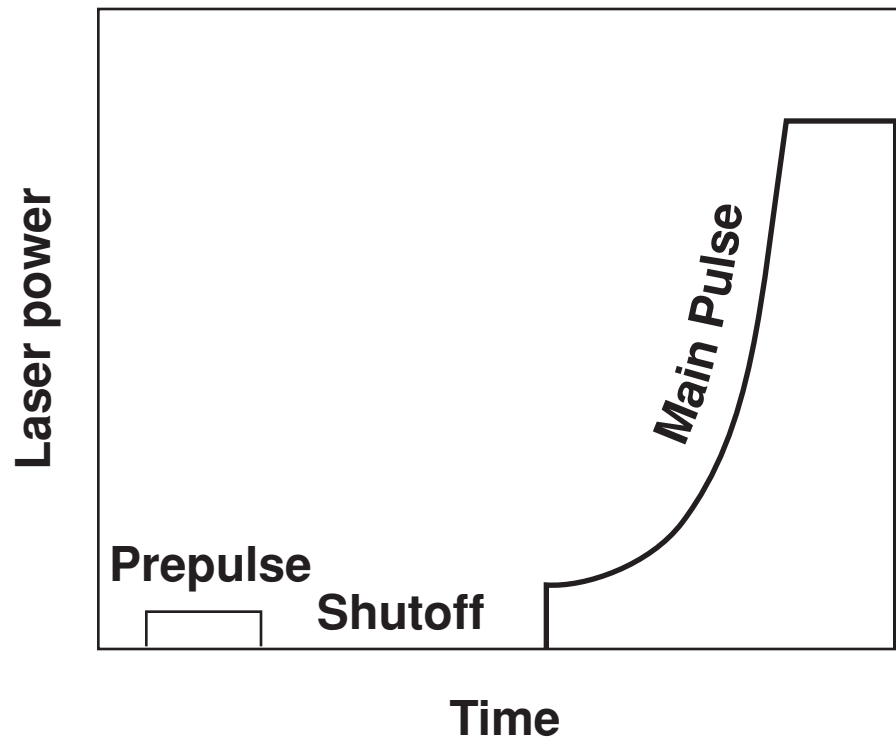
2. Low fuel adiabat, giving high compression and high yield
- Shaping with a ramped pressure profile lends flexibility to adiabat shaping

¹ R. Betti *et al.*, *Phys. Plasmas* 5, 5 (1998).

Outline

- **Explanation of adiabat-shaping physics using ramped pressure profiles**
- **Analysis of shock-timing constraints**
- **Comparison of adiabat shapes from various prepulses**

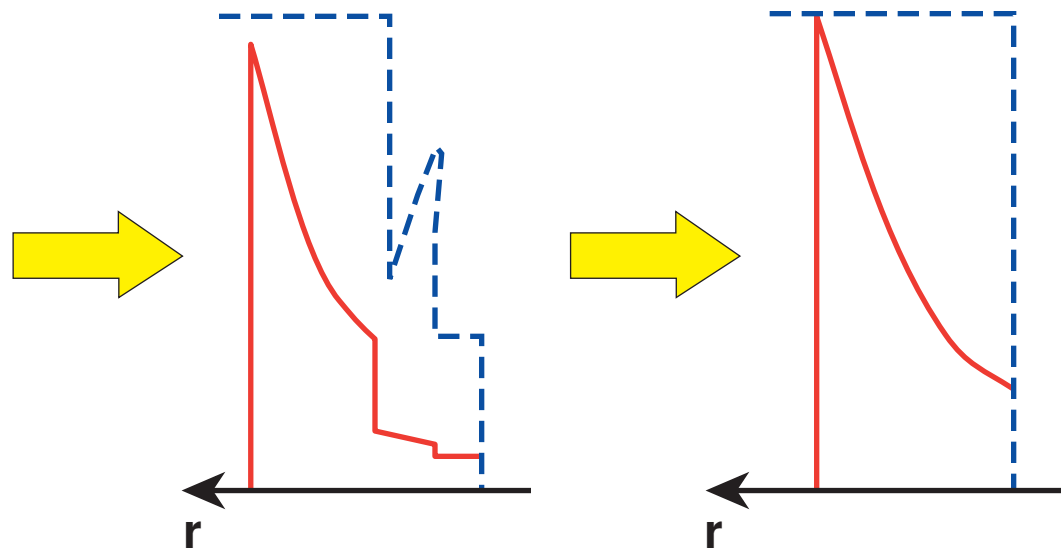
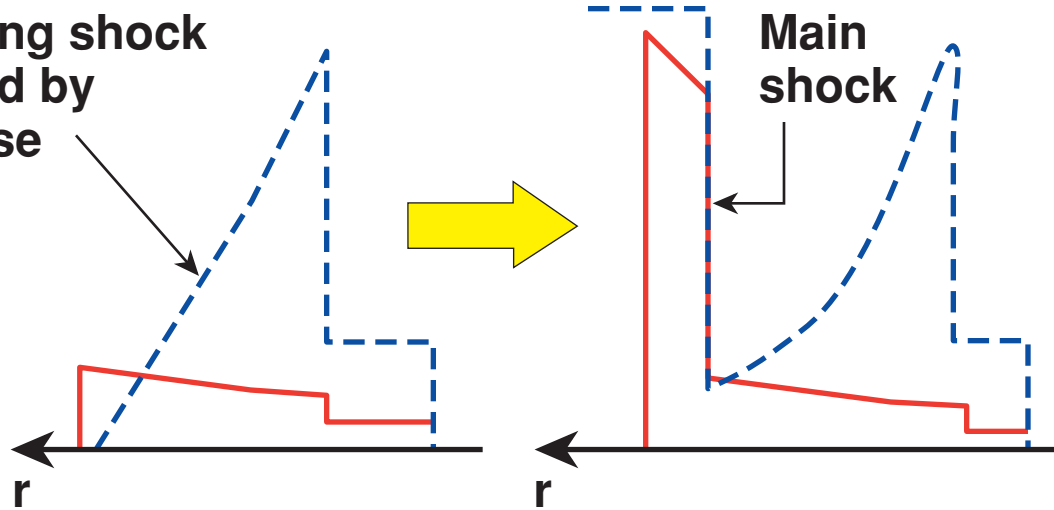
Shaping the adiabat with pressure relaxation requires a weak prepulse followed by a power shutoff and the main laser pulse



The main pulse sets the adiabat by launching a strong shock through a relaxed pressure profile.

The shock from the main pulse shapes the shell adiabat as it travels up the relaxed density and pressure profile

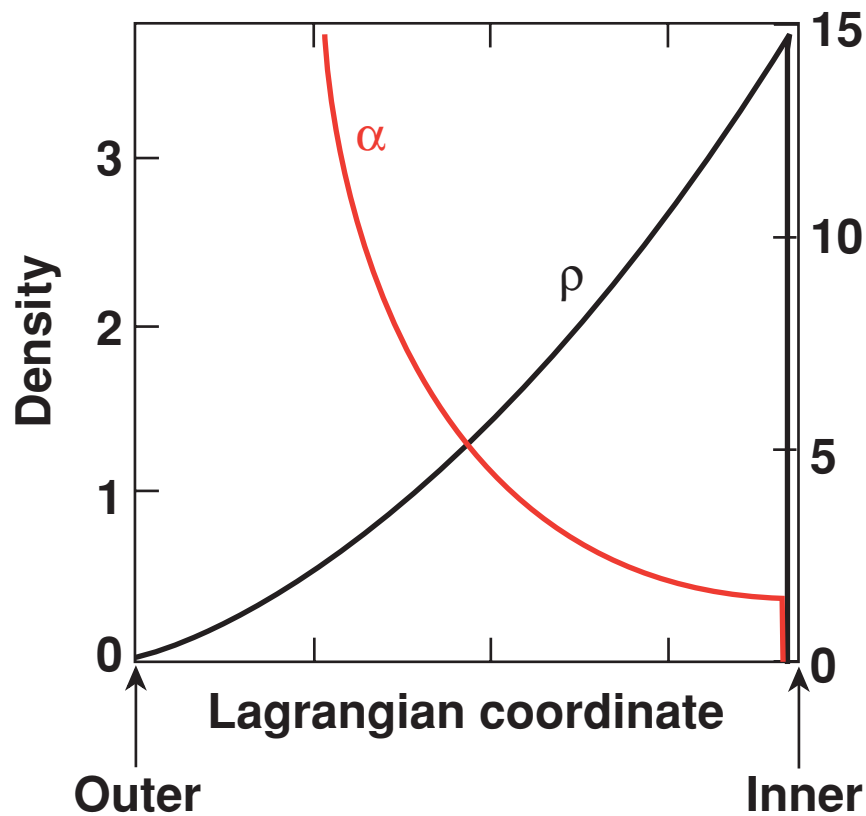
Decaying shock induced by prepulse



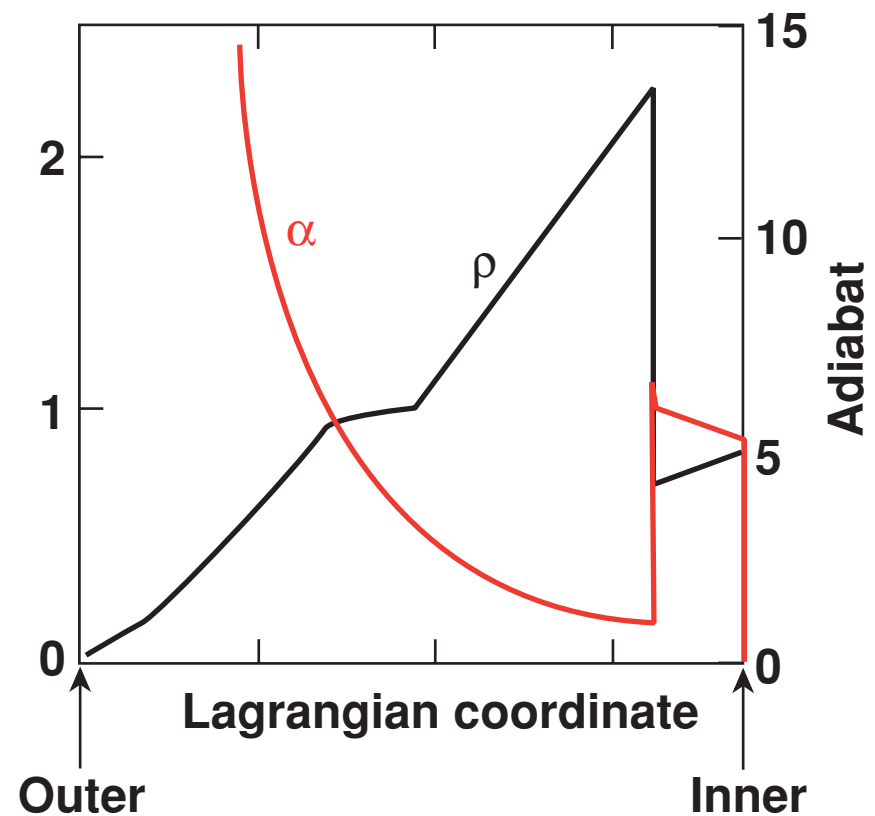
Shock timing must be within ~50 to 100 ps to avoid yield degradations of the order of 25%.

If the main pulse starts too soon, the shocks meet inside the shell, setting the rear surface on a high adiabat

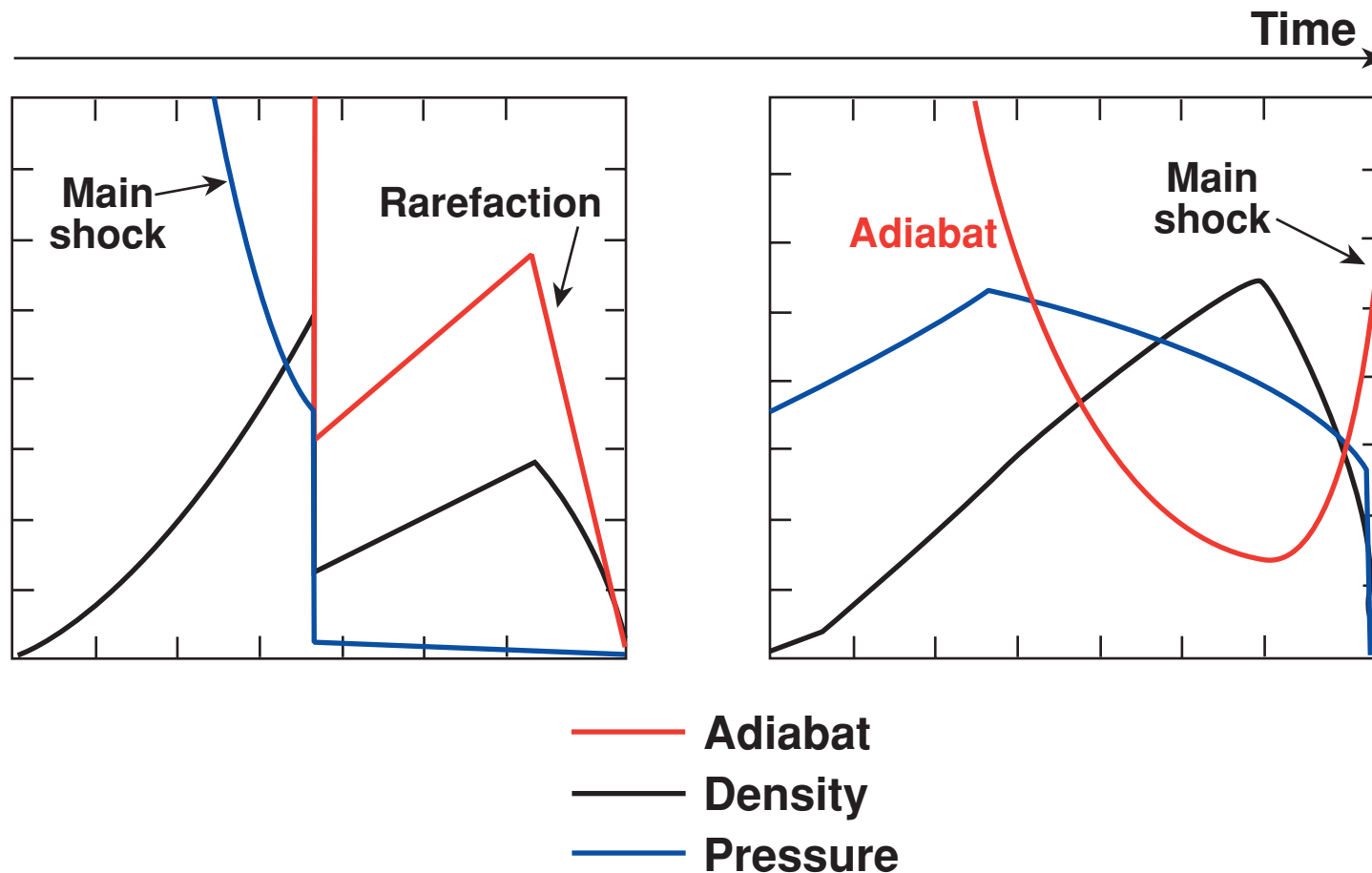
Shocks meet at back



Shocks meet inside the shell

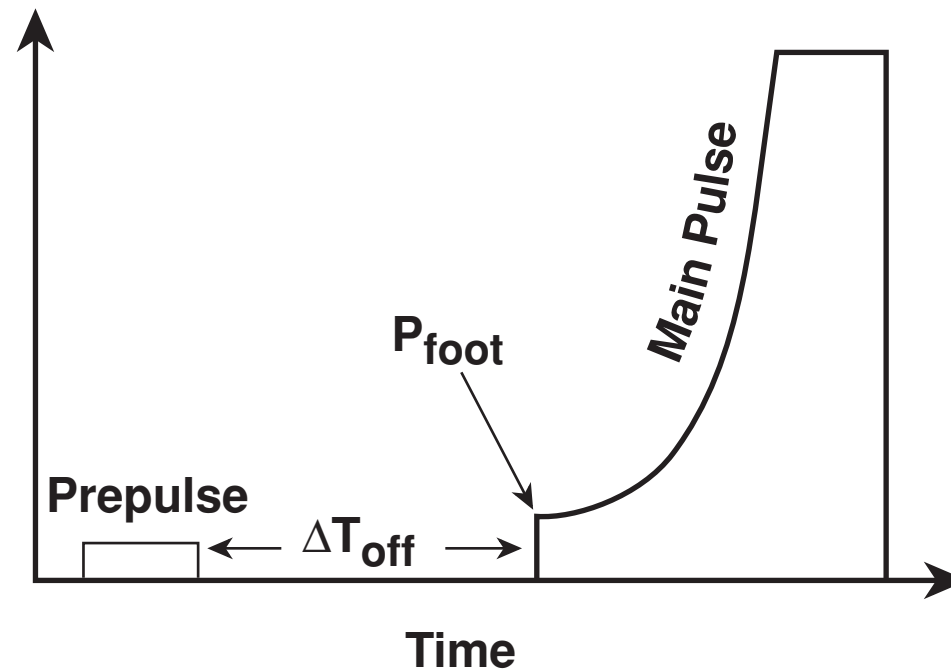


If the main pulse is delayed too much with respect to the prepulse, the back of the shell is set on a high adiabat



Late main pulse → The inner shell surface is set on a high adiabat .

Two constraints on the main pulse: (1) the main and prepulse shocks must meet at the shell's rear surface and (2) the rear-surface adiabat is an assigned design parameter



For a given prepulse (P_{prepulse} , $\Delta T_{\text{prepulse}}$) and rear adiabat, the laser shutoff time ΔT_{off} and main-pulse foot power P_{foot} are determined by these two constraints.

Dimensional analysis provides simple approximate formulas for the shutoff time and foot power

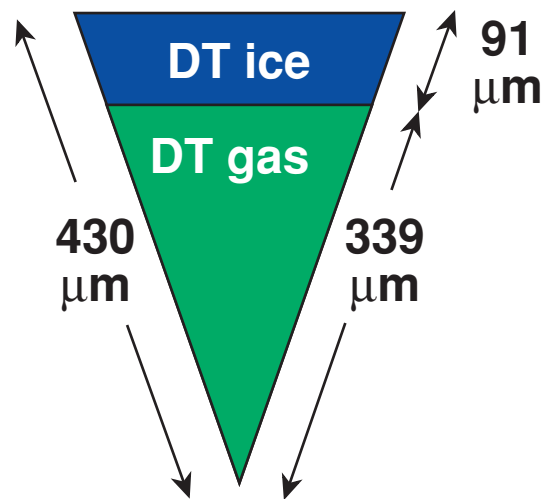
$$\frac{\Delta T_{\text{off}}}{\Delta T_{\text{prepulse}}} \approx \text{const} \cdot \left(\frac{m^*}{M_{\text{shell}}} \right)^{\mu} \left(\frac{P_{\text{back}}}{P_{\text{prepulse}}} \right)^{\omega}, \quad \frac{P_{\text{foot}}}{P_{\text{prepulse}}} \approx \text{const} \cdot \left(\frac{m^*}{M_{\text{shell}}} \right)^{\nu} \left(\frac{P_{\text{back}}}{P_{\text{prepulse}}} \right)^{\phi}$$

$$\Delta T_{\text{off}}(\text{ns}) \approx 1.6 \left[\frac{0.1}{\Delta T_{\text{prep}}(\text{ns})} \right]^{0.9} \left[\frac{\Delta_{\text{shell}}(\mu\text{m})}{90} \right]^{1.9} \left[\frac{10}{P_{\text{prep}}(\text{Mb})} \right]^{1.12} \left[\frac{\rho_0(\text{g/cm}^3)}{0.25} \right]^{1.23} \propto_{\text{back}}^{0.17}$$

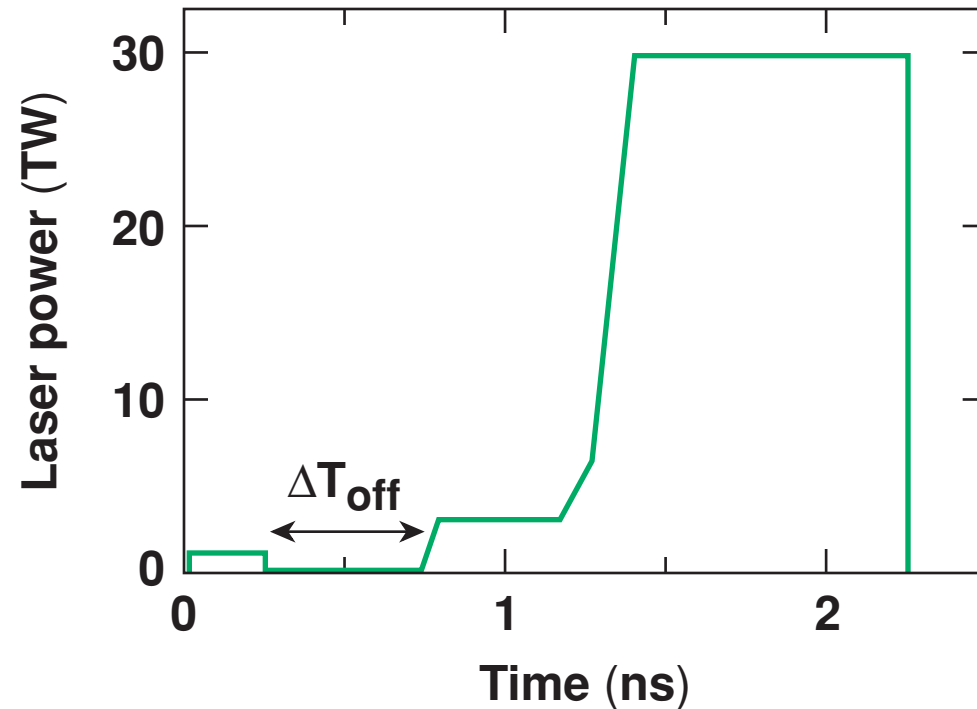
$$P_{\text{foot}}(\text{Mb}) \approx 9 \left[\frac{\Delta T_{\text{prep}}(\text{ns})}{0.1} \right]^{0.28} \left[\frac{90}{\Delta_{\text{shell}}(\mu\text{m})} \right]^{0.28} \left[\frac{P_{\text{prep}}(\text{Mb})}{10} \right]^{0.19} \left[\frac{\rho_0(\text{g/cm}^3)}{0.25} \right]^{1.44} \propto_{\text{back}}^{0.95}$$

Cryogenic DT OMEGA capsule design and sample laser pulse shape

Typical 1-D yields $\sim 10^{15}$



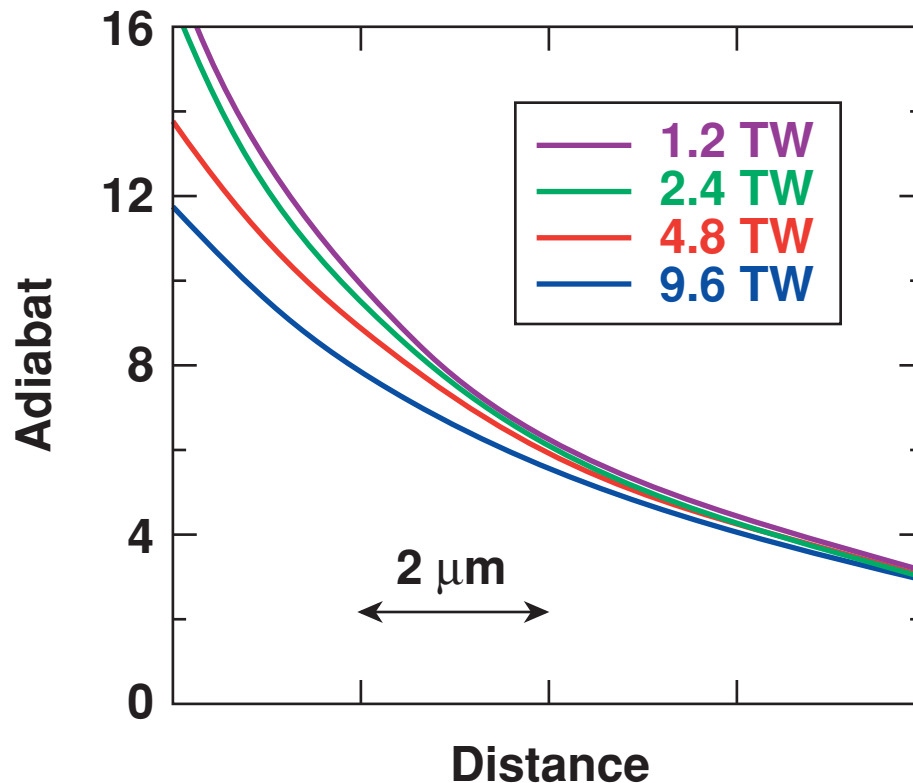
Pulse shape: 250 ps, 1.2 TW prepulse



- ΔT_{off} varies with prepulse pressure and duration and with capsule parameters.

Varying the intensity of the prepulse changes the steepness of the adiabat profile

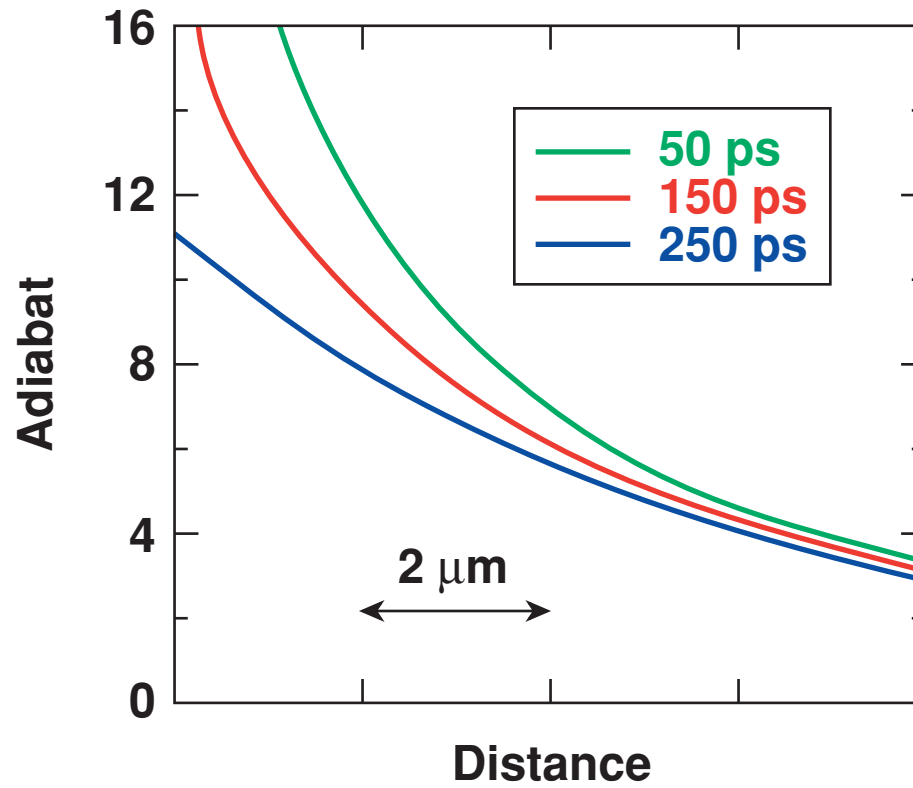
Results of varying the intensity of 50-ps square prepulses



- Lower-intensity prepulses give stronger shaping, shorter entropy-gradient scale length L_s .
- Convective instabilities are driven by entropy gradients with growth rates:

$$\gamma_{\text{conv}} \sim \frac{1}{\sqrt{L_s}}$$

A study of 1.2-TW square prepulses shows that varying the length of the prepulse also affects the steepness of the adiabat profile



Shorter prepulses give stronger shaping and shorter entropy-gradient scale length L_S .

Conclusion

- **Adiabat shaping combines high fuel compression with high ablative Rayleigh–Taylor stabilization.**
- **Adiabat shaping can be done using a short prepulse followed by a period of laser shutoff and the main drive pulse.**
- **1-D simulations have verified adiabat shaping for various prepulses.**
- **This method of adiabat shaping allows flexibility in setting adiabat shapes.**
- **Ongoing research:**
 - **2-D simulations to evaluate capsule stability for various adiabat shapes.**
 - **Effects of both Rayleigh–Taylor stabilization and convective instability will be studied.**