

# The Absolute Calibration of the Streaked Optical Pyrometer at the Omega Laser Facility

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## System Response

## Temperature Dependence

The streaked optical pyrometer (SOP) was absolutely calibrated to infer temperatures of shocked targets

- The absolute calibration is performed using a NIST-traceable tungsten-filament lamp
- The wavelength-dependent system response function is measured in seven narrow wavelength regions
- The overall response function is accurately predicted from this narrowband construct
- Brightness temperature is inferred from self-emission intensity using the absolute calibration
- Uncertainty in brightness temperature is less than 10%

The wavelength-dependent system response was absolutely calibrated using a tungsten-filament lamp

Camera output  $I$  is related to a NIST-traceable source of known spectral radiant power  $\Phi_s(\lambda)$

$$I = \Delta t \int_{\text{all } \lambda} d\lambda T_x(\lambda) \Phi_s(\lambda) SR(\lambda)$$

Source with known spectral radiant power  $\Phi_s(\lambda)$

Removable filters with transmission  $T_x(\lambda)$

SOP optics

Streak camera

- System response  $SR(\lambda)$  includes S20 photocathode sensitivity and optical transmission of the system
- $SR(\lambda)$  is measured in seven wavelength regions by the addition of 40-nm-wide bandpass filters with transmissions  $T_x(\lambda)$

The shock-wave brightness temperature is inferred by assuming a Planckian source

- The source radiance in the 590- to 900-nm region is related to that of a blackbody
- The camera output  $I$  is predicted for a range of temperatures  $T$

$$I = \frac{X(W_s)A_0}{\eta} \int_{\text{all } \lambda} d\lambda \frac{T_x(\lambda)SR(\lambda)}{\lambda^5 (e^{hc/\lambda T} - 1)}$$

Temperature (eV)

SOP output ( $\times 10^4$ ) (ADU)

$W_s = 800 \mu\text{m}$   
 $\eta = 52.5 \text{ px/ns}$   
 (17-ns sweep)  
 ND 0.3

- $A_0$  is constant for all experimental configurations
- Adjustable parameters include
  - sweep speed  $\eta$
  - slit width  $W_s$
  - neutral density (ND) filter transmission  $T_x(\lambda)$
- Magnification (TCC\*  $\rightarrow$  slit):  $14.7\times$  ( $1.84 \mu\text{m/px}$  for  $2 \times 2$  binning)

The internal optics of the ROSS\* camera are aligned and focused prior to calibrations and experiments

- Center image on photocathode using secondary mirror
- Decrease iris size to confirm centering
- Verify focusing at the charge-coupled device (CCD)

External slit

Primary mirror

Secondary mirror with iris

Streak tube

Deflection plates

Photocathode

CCD

Time

Input signal  $f/48$   
Acceptance  $f/2.5$

The SOP measures self-emission from laser-driven shock waves

Image relay from target to interferometer

Self-emission from target

SOP

Streak camera

Beam splitter

Delay element

VISAR

Streak camera

Vacuum chamber

Probe laser (532 nm) delivered through multimode fiber

Velocity interferometer

- 590- to 900-nm light from the shock front is imaged onto a streak camera
- Spatial and temporal data are collected simultaneously with a velocity interferometer system for any reflector (VISAR)
- Brightness temperature is inferred from self-emission intensity using the absolute calibration

The calibration source is a NIST-traceable tungsten-filament lamp\* with known spectral radiance

- The tungsten ribbon filament was imaged onto the photocathode

SOP spectral response

Spectral radiance [ $\mu\text{W}/(\text{ster mm}^2 \text{ nm})$ ]

Wavelength (nm)

$T_{\text{lamp}} = 0.239 \text{ eV}$   
 $\epsilon_{\text{filament}} = 0.215$

Spectral radiant power:

$$\Phi_s(\lambda) = \int dA \int d\Omega_s \Omega_s(\lambda)$$

- $\Omega_s(\lambda)$  = source radiance
- $A_{\text{px}}$  = area of the filament that maps to a single pixel
- $\Omega_{\text{lens}}$  = solid angle of VISAR  $f/3.3$  telescope

The temperature calibration assumes a delta-function wavelength response to obtain a two-parameter fit

$$I = \frac{X(W_s)A_0}{\eta} \int_{\text{all } \lambda} d\lambda \frac{T_x(\lambda)SR(\lambda)}{\lambda^5 (e^{hc/\lambda T} - 1)} \rightarrow T = \frac{T_0}{\ln(1 + \frac{A}{I})}$$

SOP spectral response

Spectral radiance ( $\text{W}/\text{mm}^2 \text{ nm}$ )

Wavelength (nm)

4.5 eV

0.25 eV

Temperature (eV)

SOP output ( $\times 10^4$ ) (ADU)

$A = 3894 \text{ ADU}$   
 $T_0 = 1.91 \text{ eV}$

Parameters  $A$  and  $T_0$  are a convenient means to infer temperature from measured SOP output for a given experimental configuration.

An 800- $\mu\text{m}$ -wide slit provides optimal throughput, temporal resolution, and insensitivity to misalignment

Throughput correction  $X(W_s)$

Apparent slit width

Profile of photocathode

Normalized camera output

LSF FWHM ( $\mu\text{m}$ )

Normalized camera output

FWHM =  $540 \mu\text{m}$

- The camera output rises with the slit width until  $\sim 500 \mu\text{m}$
- The line spread function (LSF) full width at half maximum (FWHM) is smaller than the actual slit width
- Wide slit widths are less sensitive to photocathode alignment

An estimated system response function was corrected using the narrowband measurements

- The estimated system response was formulated from optical transmission and S20 photocathode sensitivity
- Narrowband responses were reproduced within 3% over three calibration sessions

Narrowband measurements

System response functions

Camera output (ADU) ( $\times 10^4$ )

Wavelength (nm)

Bandpass region (nm)

Normalized system response

Wavelength (nm)

— Estimated SR ( $\lambda$ )  
 — Corrected SR ( $\lambda$ )

The corrected system response function predicts wideband (590- to 900-nm) camera output within 4%.

A "gray-body" approximation is used to determine shock temperatures

- The emissivity of the shock front is related to its reflectivity through Kirchoff's law  $\epsilon = 1 - R$
- For measured camera output  $I$  and parameters  $A$  and  $T_0$ , gray-body temperature is calculated using

$$T = \frac{T_0}{\ln\left[1 + \frac{(1-R)A}{I}\right]}$$

- The gray-body temperature is calculated from the self-emission intensity (SOP) and reflectivity (VISAR)

OMEGA

VISAR

Velocity

Reflectivity

SOP

Temperature (black-body)

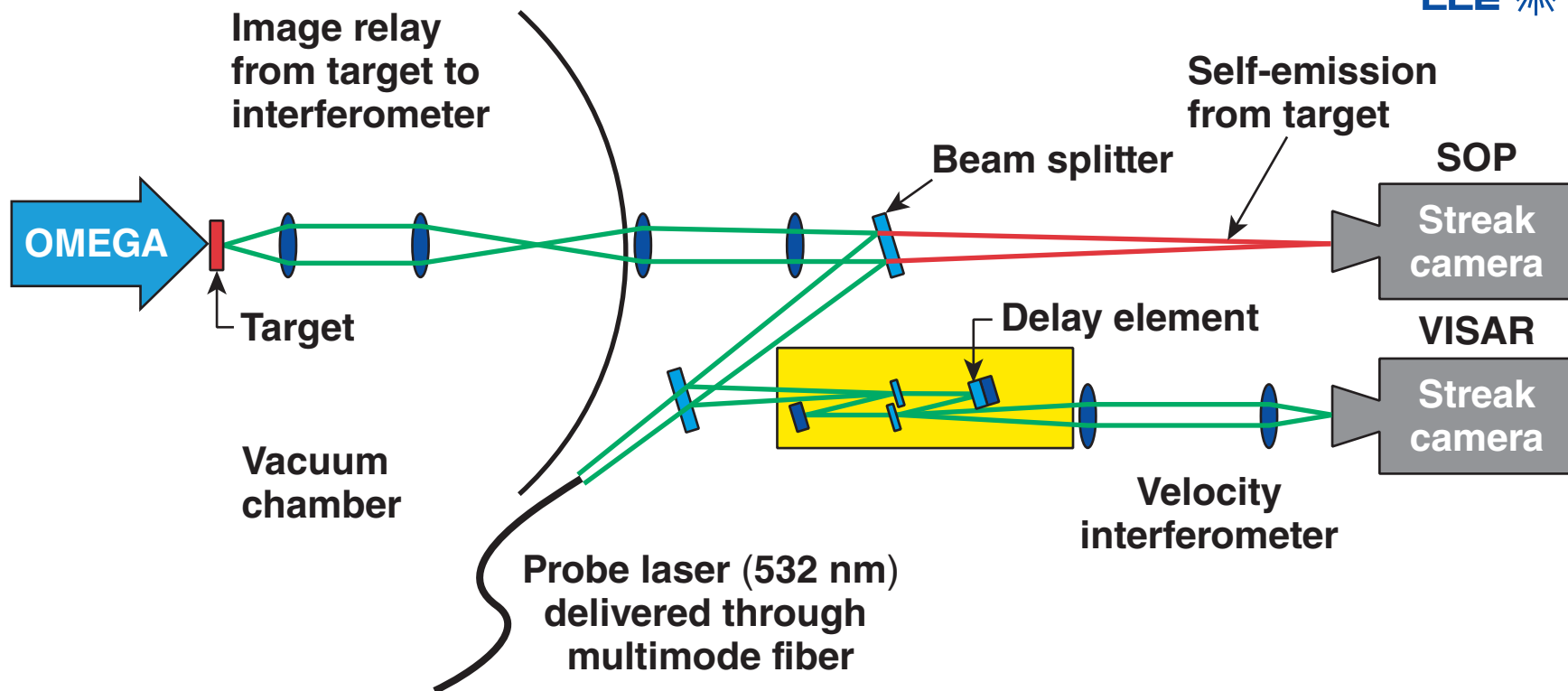
Temperature (gray-body)

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# The SOP measures self-emission from laser-driven shock waves

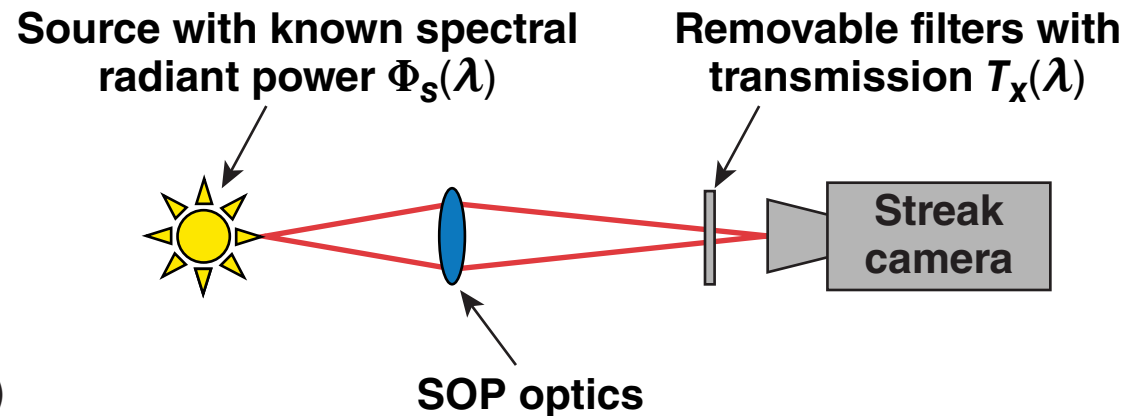


- 590- to 900-nm light from the shock front is imaged onto a streak camera
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# The wavelength-dependent system response was absolutely calibrated using a tungsten-filament lamp

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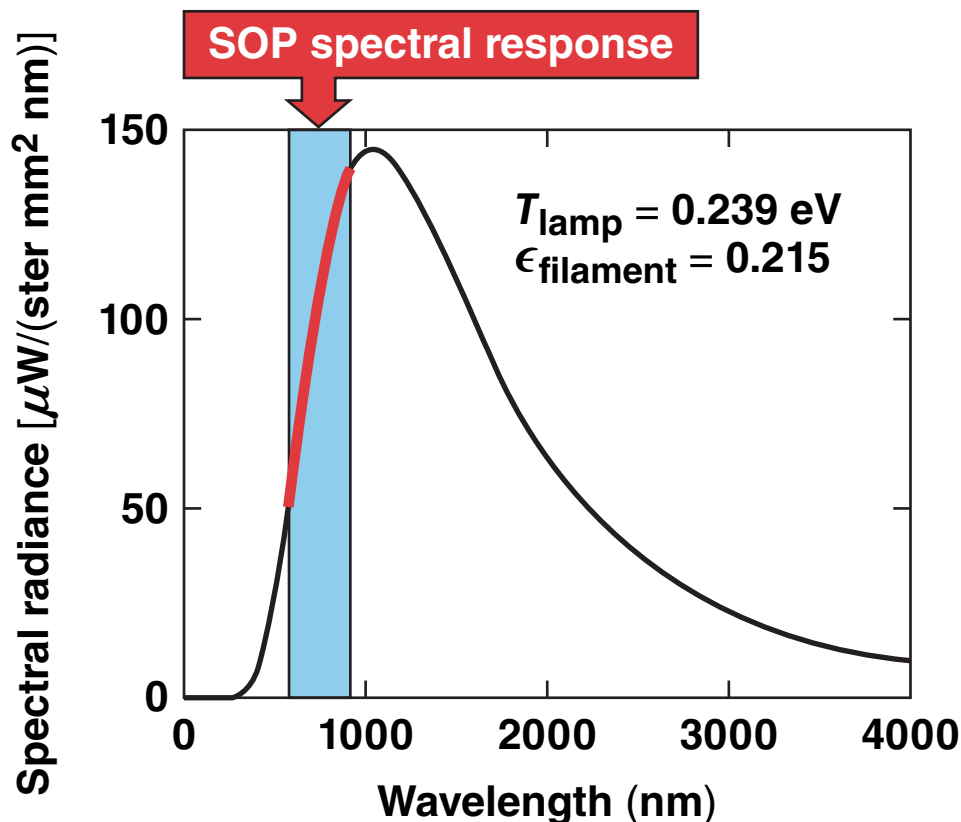
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# The calibration source is a NIST-traceable tungsten-filament lamp\* with known spectral radiance

- The tungsten *ribbon* filament was imaged onto the photocathode



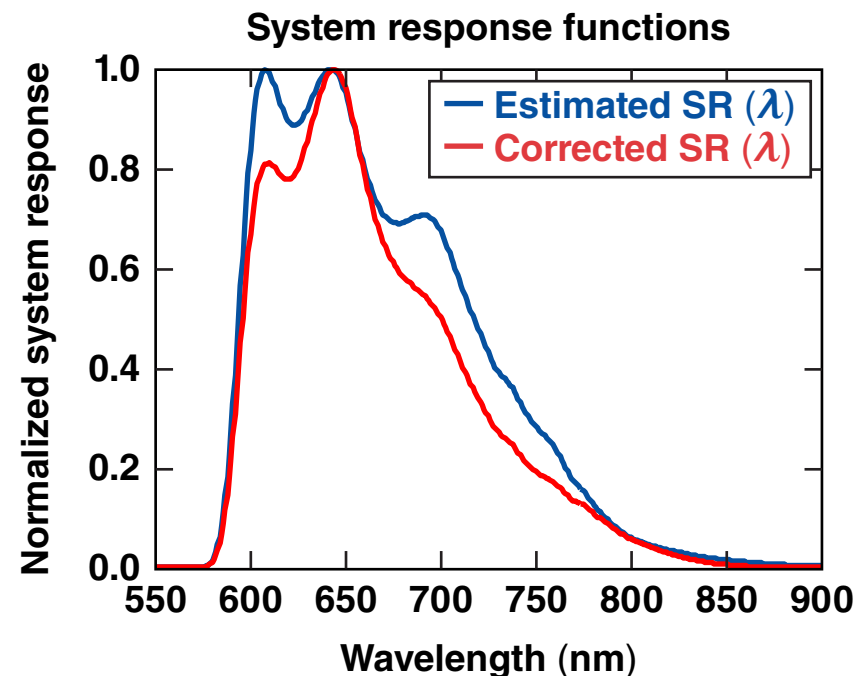
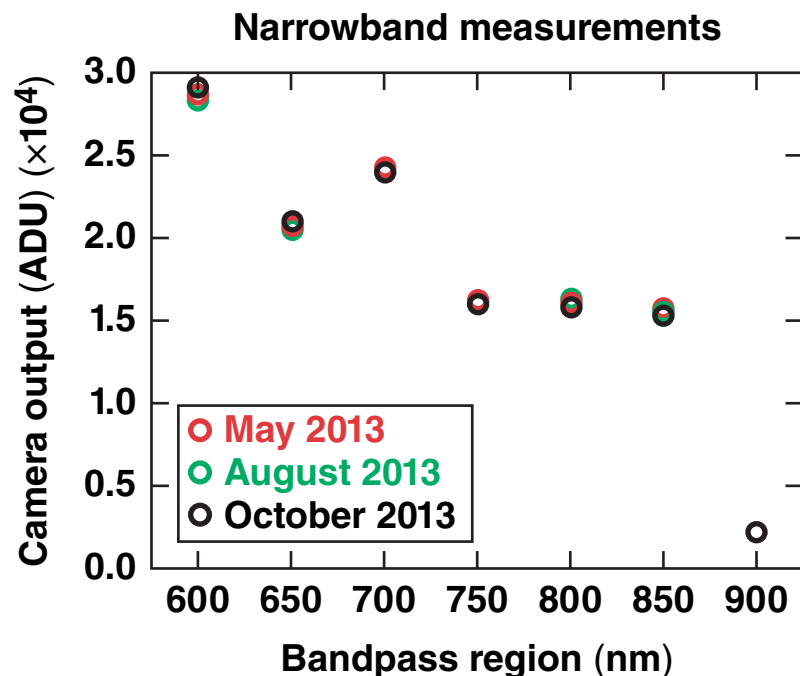
Spectral radiant power:

$$\Phi_s(\lambda) = \int_{A_{\text{px}}} dA \int_{\Omega_{\text{lens}}} d\Omega L_s(\lambda)$$

- $L_s(\lambda)$  = source radiance
- $A_{\text{px}}$  = area of the filament that maps to a single pixel
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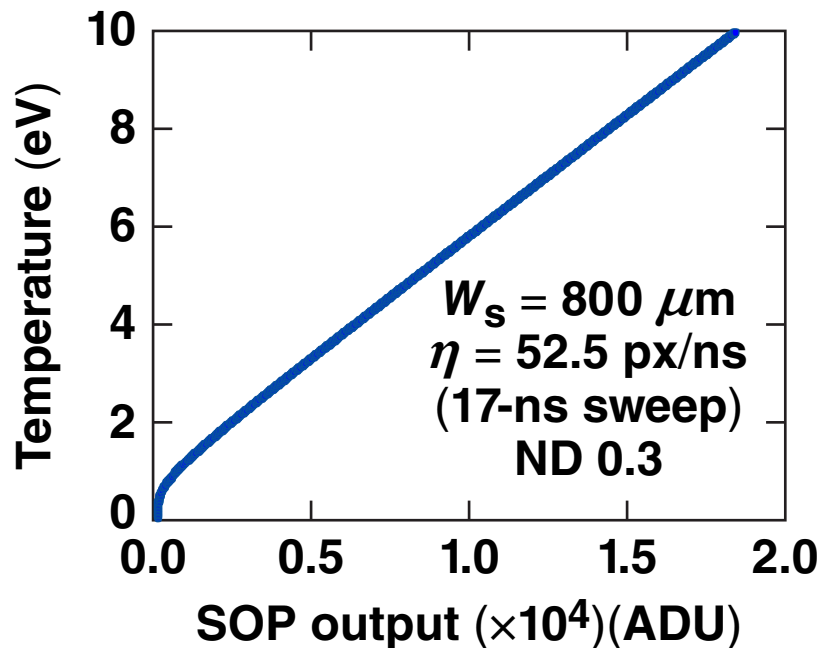


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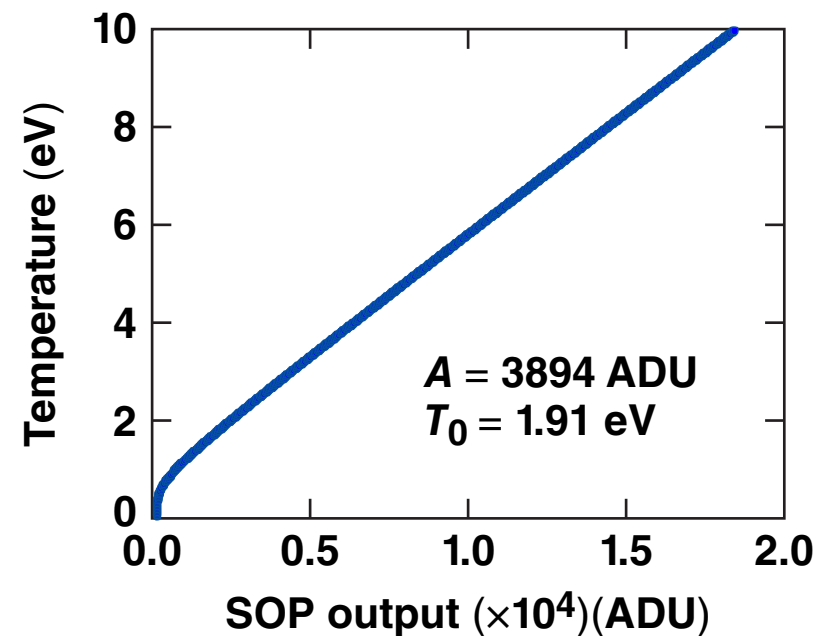
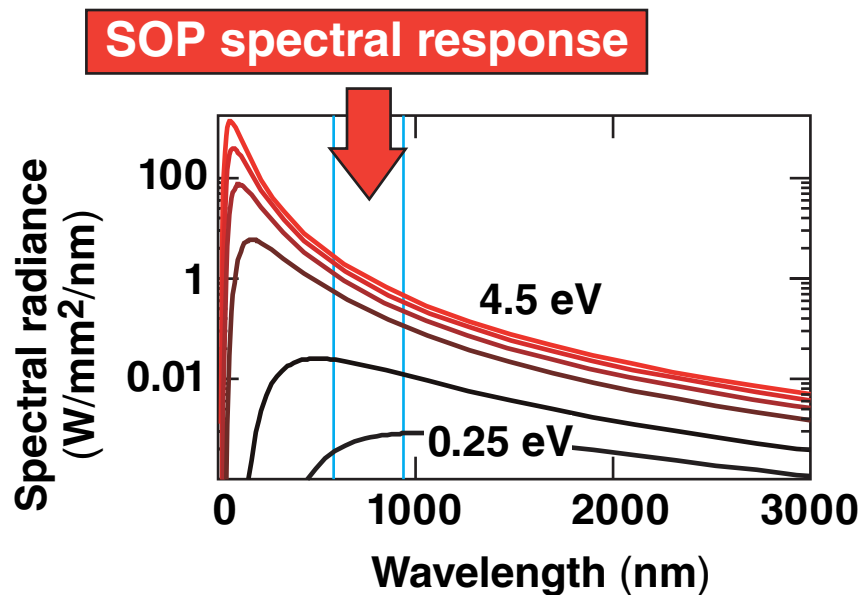
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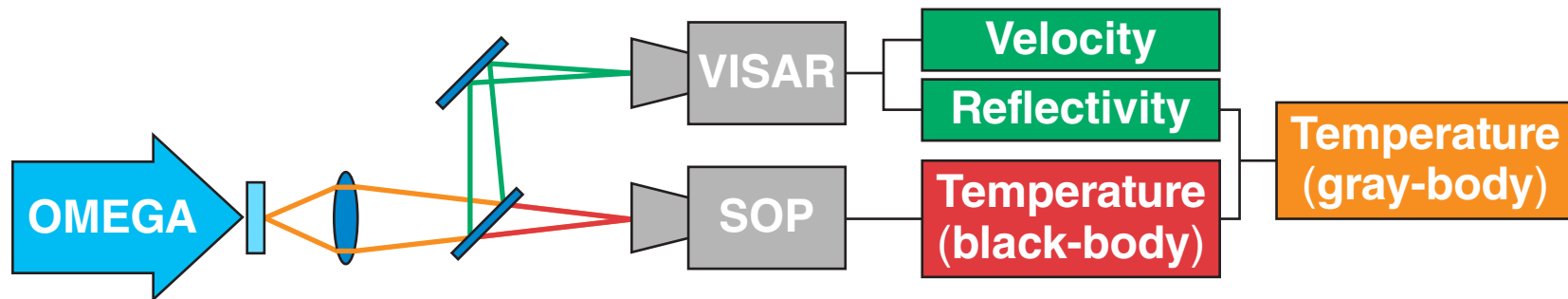


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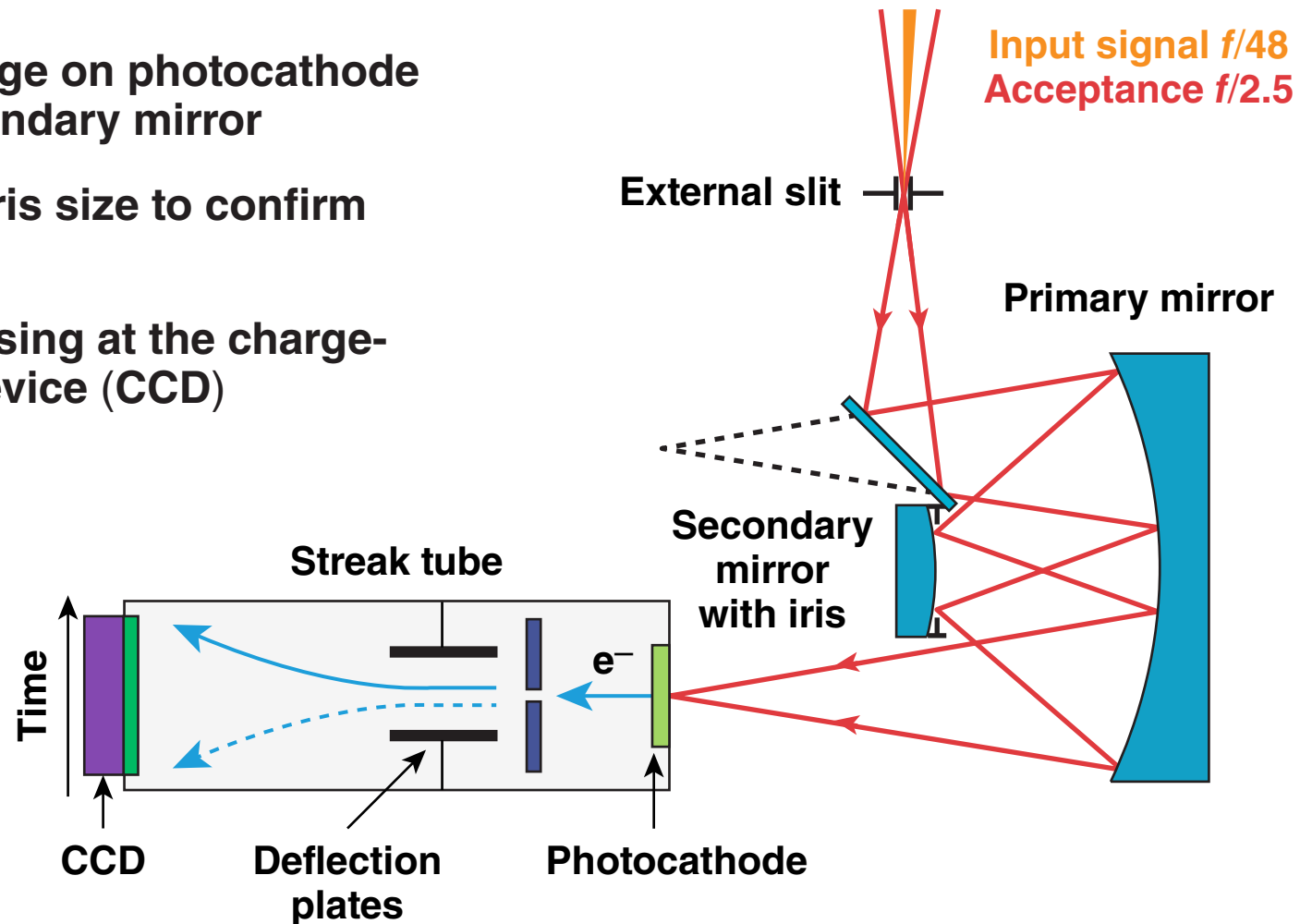
$$T = \frac{T_0}{\ln \left[ 1 + \frac{(1-R)A}{I} \right]}$$

- The gray-body temperature is calculated from the self-emission intensity (SOP) and reflectivity (VISAR)

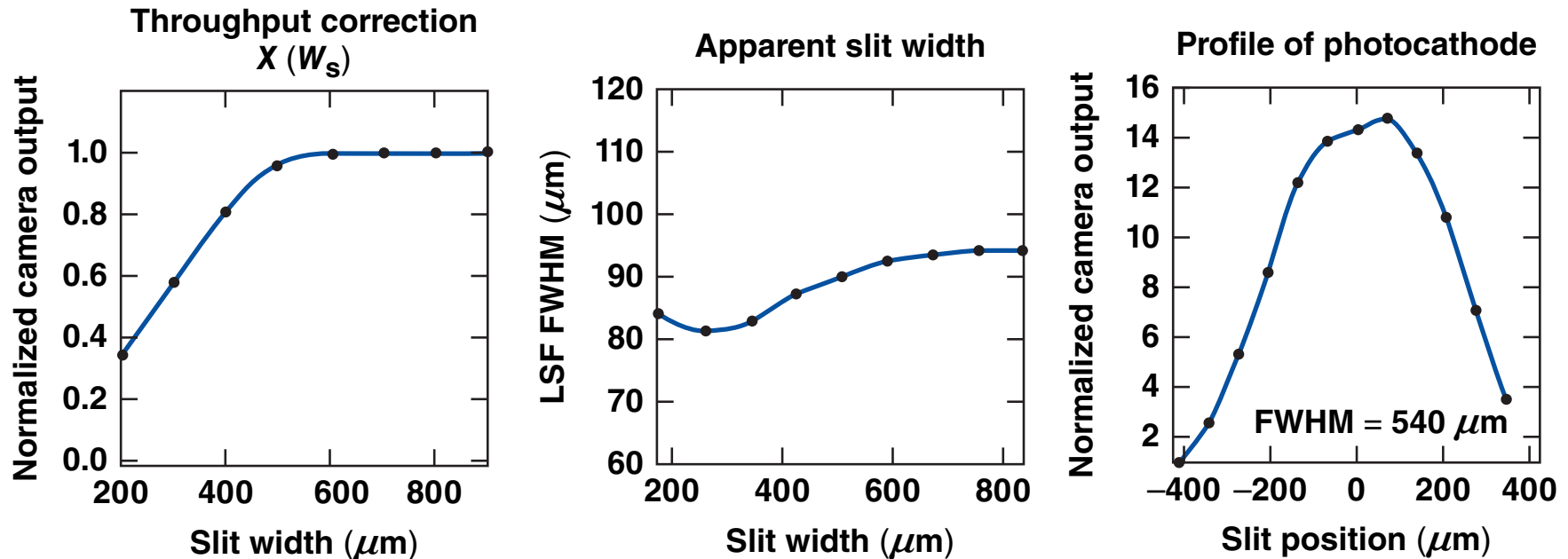


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