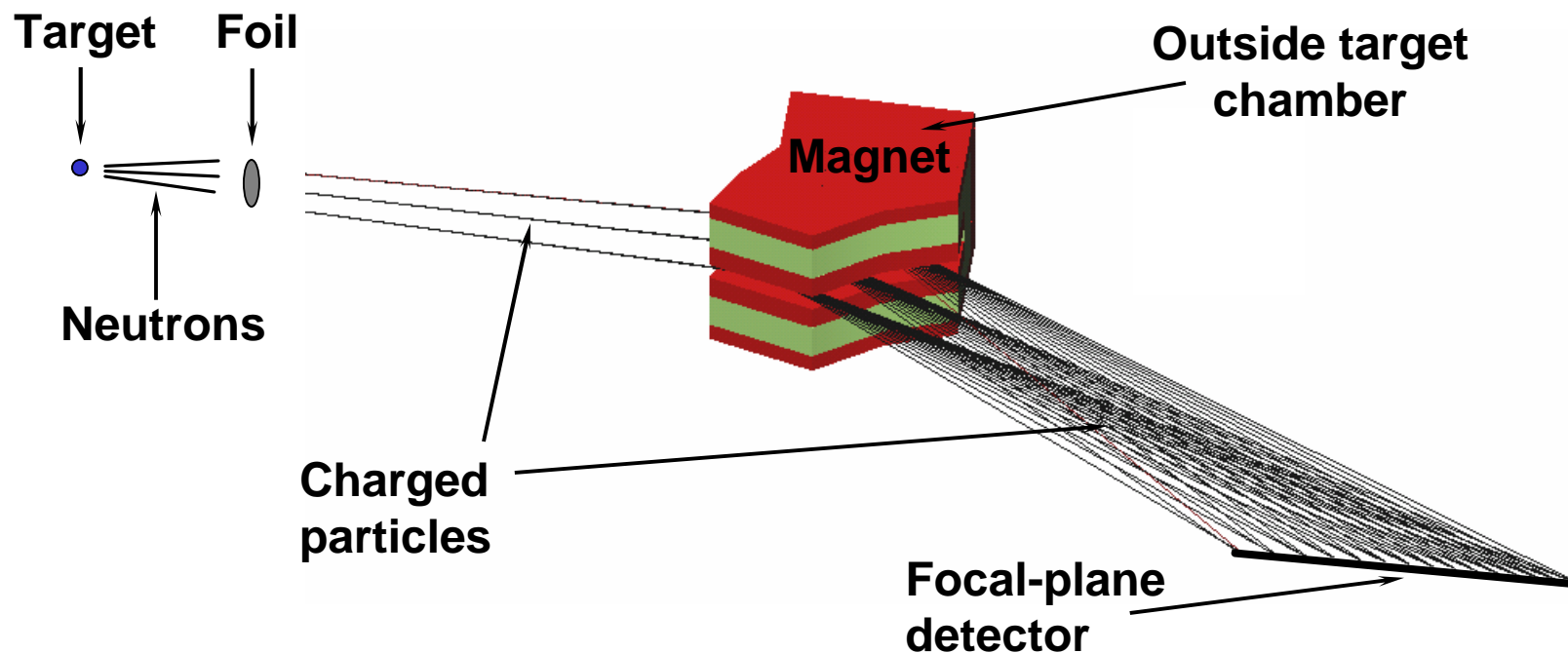


# Introduction

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# A Magnetic Recoil Spectrometer (MRS) for precise $rR_{fuel}$ and $T_i$ measurements of warm and cryo targets at OMEGA and the NIF



Johan Frenje  
MIT - Plasma Science  
and Fusion Center

33<sup>rd</sup> Anomalous  
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## Collaborators

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**R. D. Petrasso\*, C. K. Li, F. H. Séguin, J. DeCiantis,  
S. Kurebayashi, J. R. Rygg and B.E. Schwartz**

**Plasma Science and Fusion Center  
Massachusetts Institute of Technology**

**J. Delettrez, V. Yu. Glebov, D. D. Meyerhofer, T. C. Sangster,  
C. Stoeckl and J. M. Soures**

**Laboratory for Laser Energetics  
University of Rochester**

**S. Hatchett, S. Haan, G. Schmid, N. Landen and N. Izumi  
Lawrence Livermore National Laboratory**

**D. Stelter  
Dexter Magnetic Technologies Inc.**

**\* Visiting senior scientist at LLE**



## Abstract

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A method to determine  $\rho R_{\text{fuel}}$  of cryogenic deuterium-tritium (DT) plasmas is to measure the energy spectrum and yield of elastically scattered primary neutrons. Minimizing the effect of the background is critical for successful implementation, and to accomplish this, a novel spectrometer for measurements of neutrons has been designed for OMEGA and the NIF. From scattered neutrons in the energy range (7-10 MeV), the  $\rho R_{\text{fuel}}$  will be measured; from primary neutrons,  $T_i$  measurements will be performed besides final characterization of the spectrometer. The instrument is based on a magnetic spectrometer with a conversion foil for production of charged particles at nearly forward scattered angles. In its initial, and perhaps final, phase of implementation, a thin CH-foil in combination with CR-39 track detectors positioned in the focal plane of the spectrometer will be used to detect recoil protons, produced by 14.1-MeV primary neutrons, with high spatial resolution. The CR-39, operated in coincidence mode, will facilitate a highly accurate  $\rho R_{\text{fuel}}$  and  $T_i$  measurements, and accurate energy calibration of the system. In the later implementation, current mode detectors, such as CVD-strip detectors or scintillators, might be used for detection of deuteron recoils for  $\rho R_{\text{fuel}}$  measurements. The spectrometer has a large dynamic range ( $>10^6$ ), and can operate at yields as low as  $10^{12}$ . This will allow  $\rho R_{\text{fuel}}$  measurements of warm and cryo DT targets at OMEGA, and fizzle and ignited cryo DT targets at the NIF. Using LASNEX and neutron transport calculations, the signal-to-noise (S/N) ratio is estimated to be of the order 100 for measurements of cryo DT targets at OMEGA and the NIF, irrespective detection scheme.



# MRS strengths at OMEGA and the NIF

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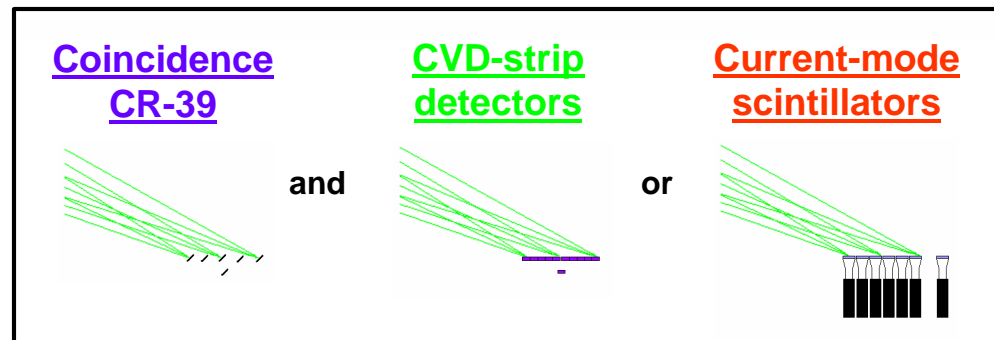
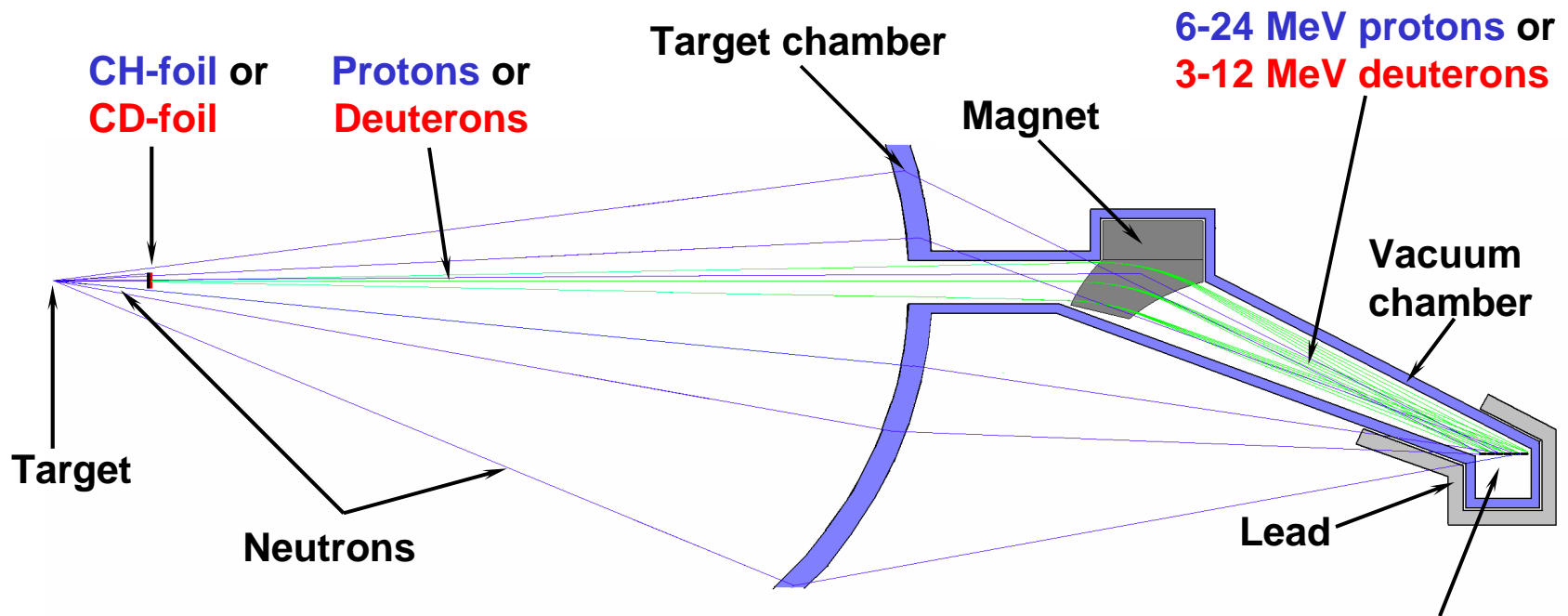
- $rR_{\text{fuel}}$  of warm, fizzle and ignited implosions can be measured at the NIF, and similarly for warm and cryo DT at OMEGA.
- $rR_{\text{fuel}}$  asymmetries can be potentially measured on NIF.
- Large dynamic range is achievable. ( $Y_{1n} \sim 10^{12} - 10^{19}$ )
- Flexible instrument: - 2 different types of detectors can be used advantageously.  
- Recoils of either p or d can also be used advantageously.
- Authenticate the data through the primaries.
- A trade off can be made between high resolution and high efficiency, depending on exp.
- Large signal-to-noise (S/N  $\sim 100$ ) ratio for most applications.
- Wide-band spectrometer (6-24 MeV p); (3-12 MeV d).
- High-resolution spectrometer ( $DE_i/E = 1.8\%$ ).
- Accurately measure  $T_i$  ( $DT_i = \pm 30$  eV).
- Background spectra can be separately characterized.
- The MRS is outside target chamber, which makes mechanical interface straight forward.
- For CR-39 detection, shielding is not required.



# MRS principle

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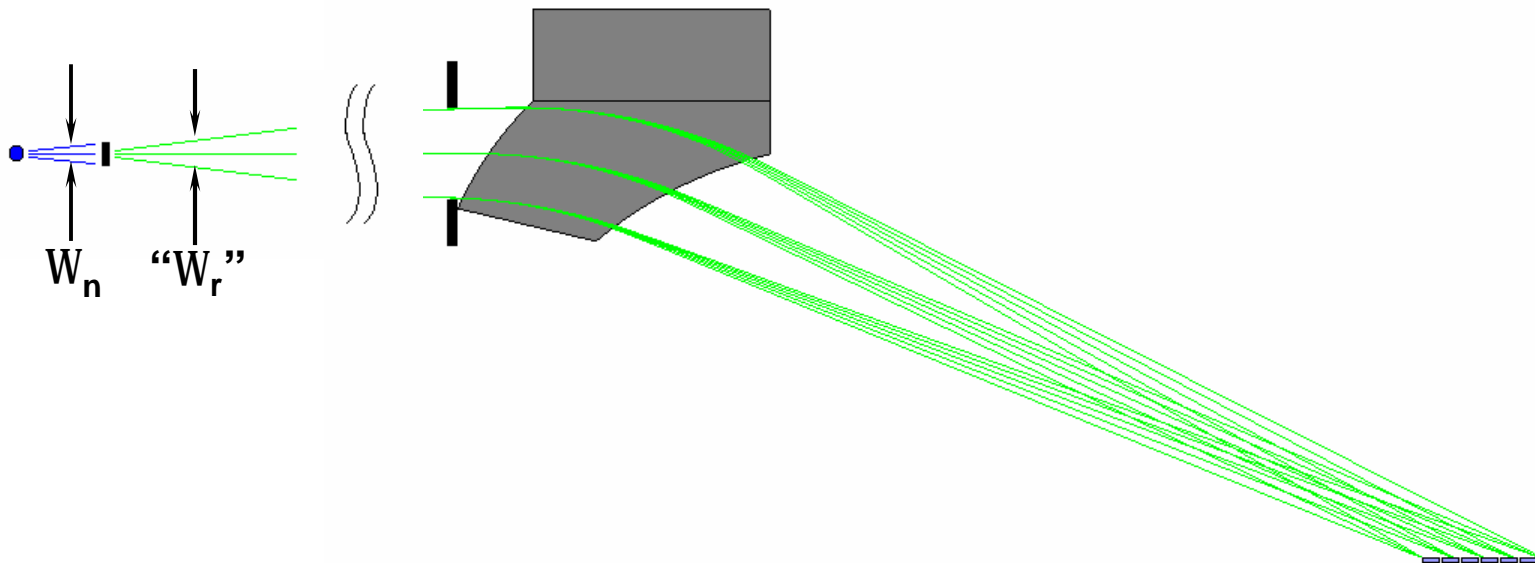
# MRS principle



## MRS principle - Detection efficiency ( $e_n$ )

- The detection efficiency can be expressed as

$$e_n \propto W_n \int_0^{\theta} \frac{d\sigma}{dW_{lab}} dW$$



- Maximum differential cross section at forward scattering angles, focusing aspects and large aperture significantly enhances  $e_n$ .



## MRS principle - Resolution ( $DE_I$ )

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- Resolution ( $DE_I$ ) of the spectrometer is defined as the energy distribution at the focal plane when viewing a fluence of mono-energetic neutrons. The resolution can be written as

$$DE_I \gg \sqrt{DE_f^2 + DE_k^2 + DE_s^2}$$

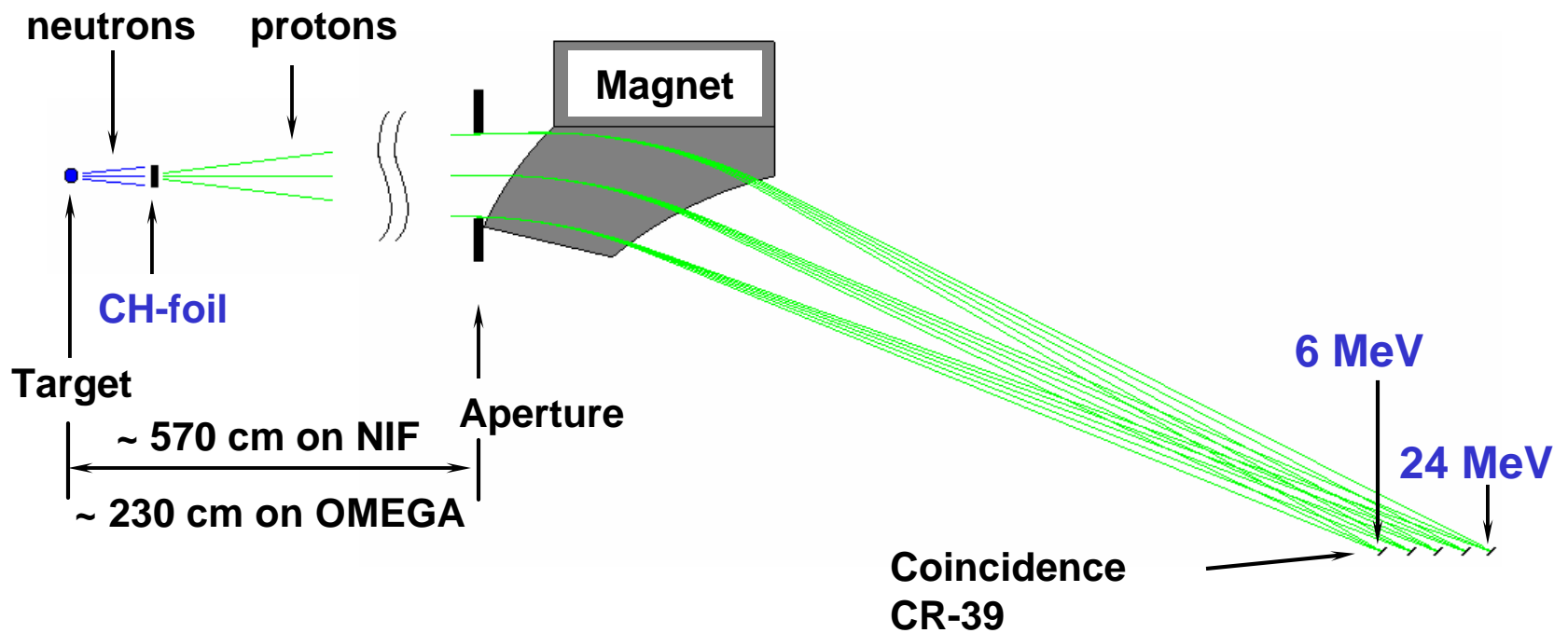
$DE_f$	=	Energy loss in foil	$\mu$	foil thickness
$DE_k$	=	Kinematic energy broadening	$\mu$	foil and aperture size
$DE_s$	=	Ion optical energy broadening	$\mu$	magnet performance

# MRS design

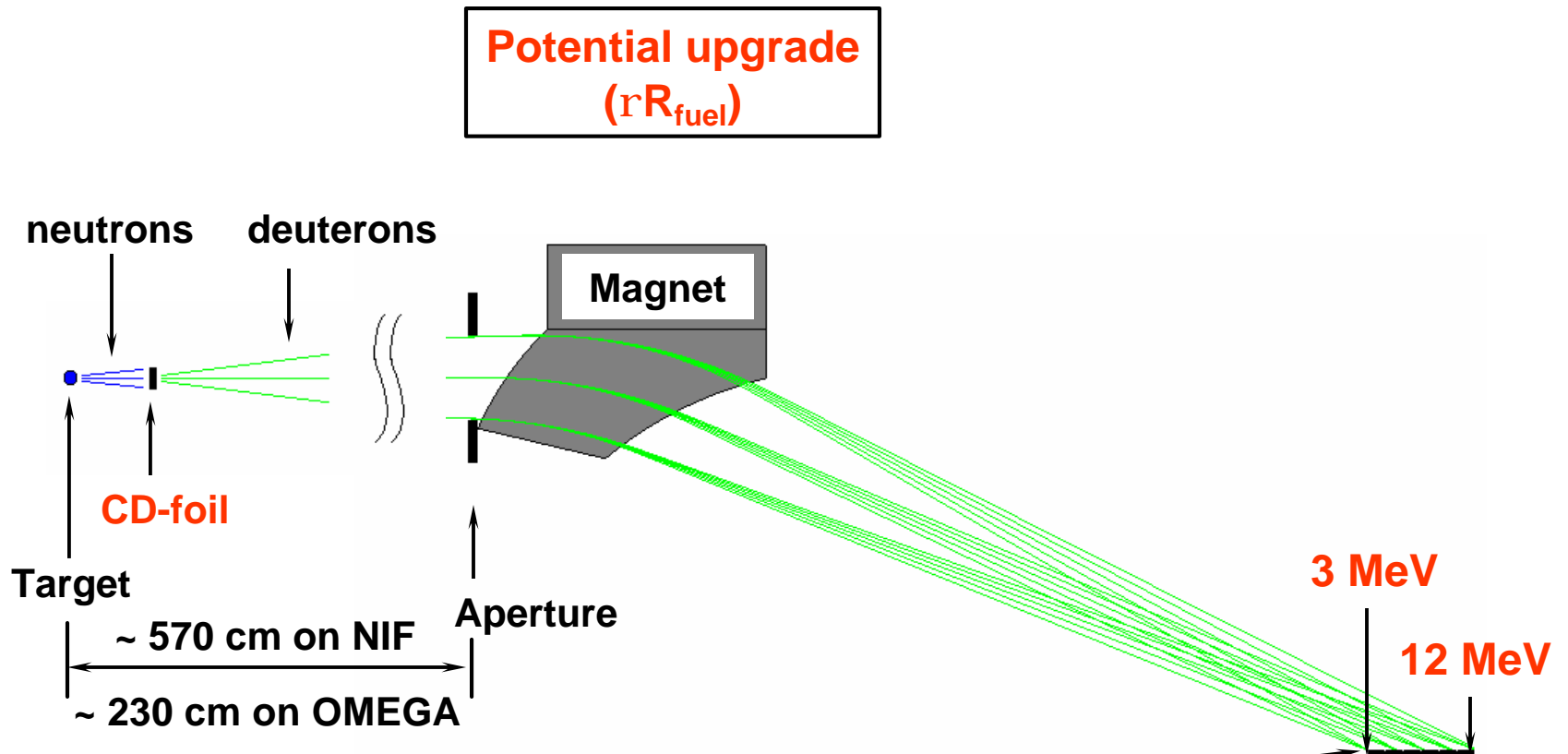
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# Design philosophy

Initial and potentially the final implementation  
( $rR_{\text{fuel}}$  and  $T_i$ )

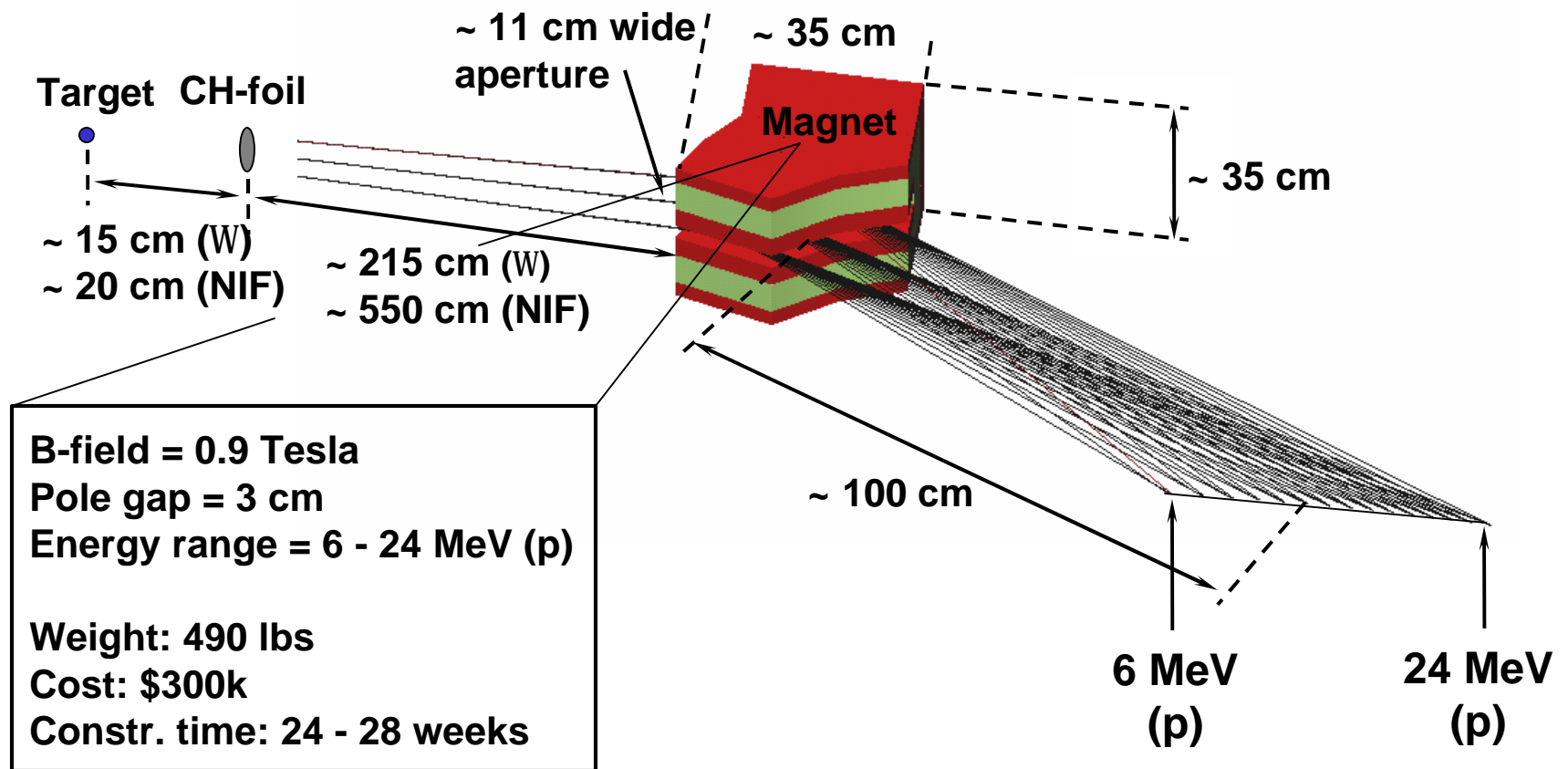


# Design philosophy



1. Coincidence CR-39
2. CVD detectors or Current-mode scintillators

# Design of the MRS at OMEGA and the NIF

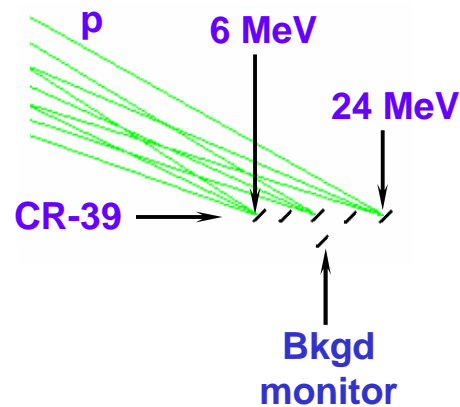


J. A. Frenje et al., Rev. Sci. Instrum. 72 (2001) 854.

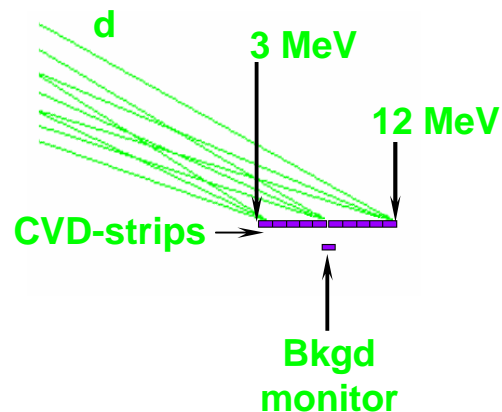
# We will develop coincidence CR-39 and one of two electronic detector systems

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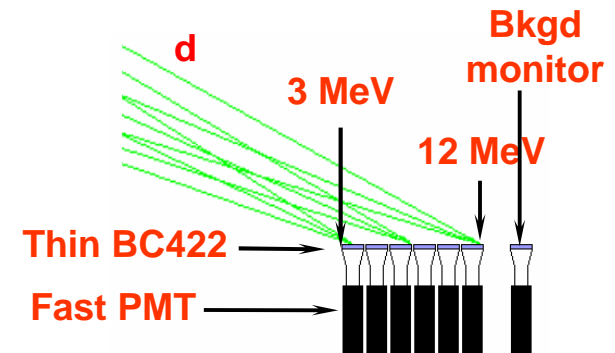
## Coincidence CR-39



## CVD-strip detectors



## Current-mode scintillators



## We will develop coincidence CR-39 and one of two electronic detector systems

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<b>Detector</b>	<b>Advantages</b>	<b>Disadvantages</b>
<b>Coincidence CR-39**</b>	<b>Totally insensitive to EMP, X-rays &amp; g-rays Shielding not required Robust technology</b>	<b>9-12 hour turn around</b>
<b>CVD-strip detector</b>	<b>Large dynamic range Fast Insensitive to g's Radiation hardened</b>	<b>Sensitive to EMP</b>
<b>Current-mode scintillator</b>	<b>Fast Well-known technology</b>	<b>Sensitive to g' Sensitive to EMP</b>

**\*\* At Vulcan, only CR-39, radiochromic film, and film can be reliably used.**



# MRS performance

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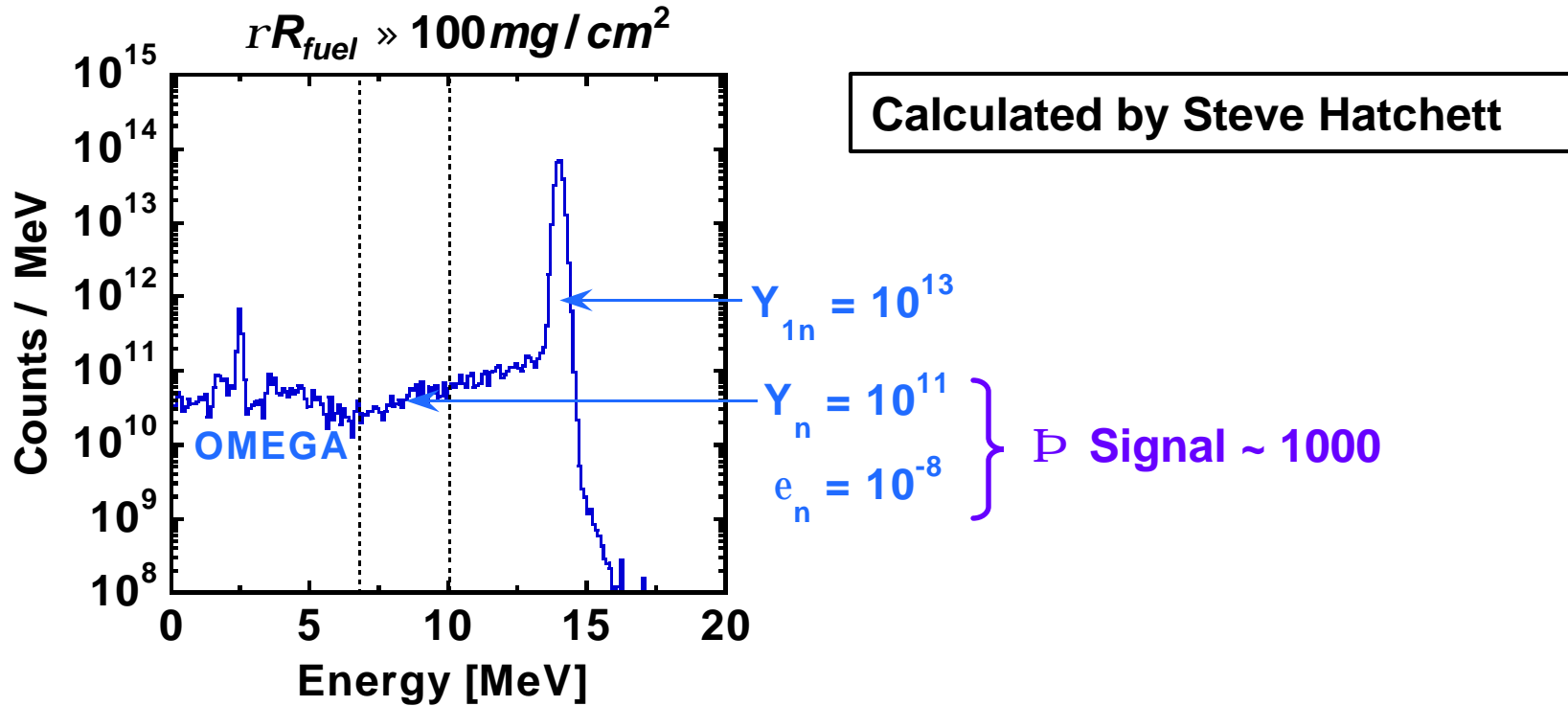


## Performance of MRS at OMEGA and the NIF

Facility	Type of measurement	Foil	$e_n$	$DE_1$ [keV]
OMEGA	$rR_{\text{fuel}} \& T_i$	CH	$5 \times 10^{-10}$	250
“	$rR_{\text{fuel}} \& T_i$	“	$6 \times 10^{-9}$	3000
“	$rR_{\text{fuel}}$	CD	$8 \times 10^{-10}$	250
“	$rR_{\text{fuel}}$	“	$1 \times 10^{-8}$	3000

At the NIF,  $e_n$  is about one order of magnitude smaller for the same  $DE_1$ .

# Predicted signal (S) for $rR_{fuel}$ measurements of a cryo DT target at OMEGA



- How many photons are produced in the thin BC422 scintillator (0.25 mm thick) by these 1000 fully stopped deuterons?

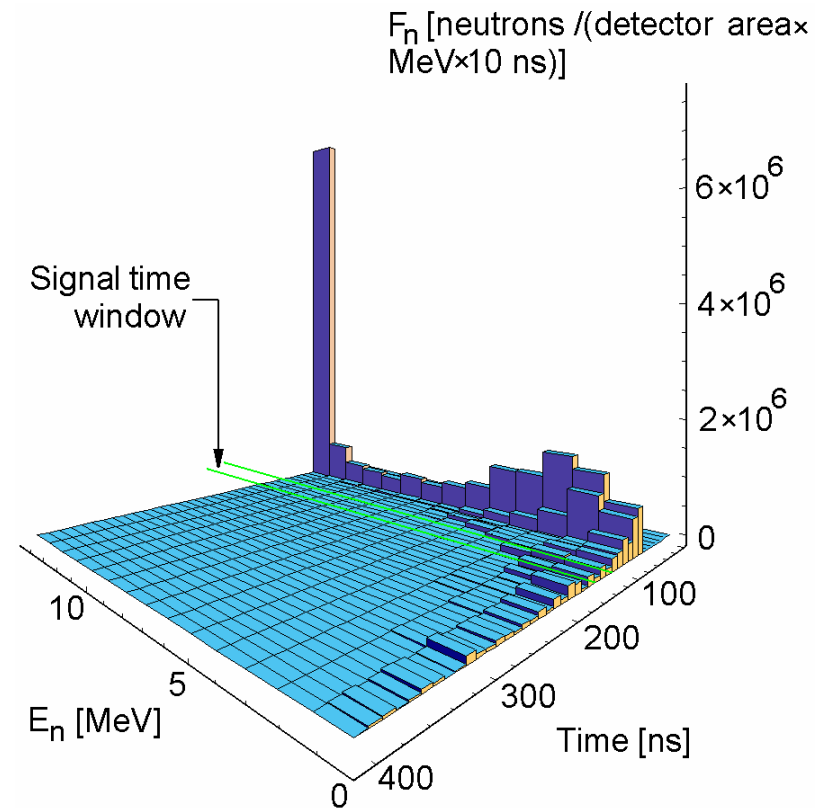
$$S \sim \frac{1000 \times 2 \text{ MeV}_{ee}}{100 \text{ eV/photon}} \sim 2 \times 10^7 \text{ photons}$$

# Predicted Noise (N) for $rR_{fuel}$ measurements of a cryo DT target at OMEGA

## Noise (N)

- Neutron transport codes COG and TART2000 were used to predict neutron flux and spectrum at detector.

- About  $5 \times 10^5$  neutrons ( $E_n = 0 - 4$  MeV) pass the detector in the signal time window (which is about 55 – 81 ns after the primary neutrons hit the detector).



Calculated by Greg Schmid

# Predicted S/N ratio for $rR_{fuel}$ measurements of a cryo DT target on OMEGA

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- About 1200 neutrons interact with the scintillator.
- A benchmarked Monte Carlo code predicted total number of produced photons by modeling scintillator geometry and response to the neutrons.

$$N \sim \frac{1200 \times 0.1 \text{ MeV}_{ee}}{100 \text{ eV/photon}} \sim 1 \times 10^6 \text{ photons}$$

$$\text{P} \quad \boxed{S/N \sim \frac{2 \times 10^7}{1 \times 10^6} \sim 20}$$

$$\frac{S}{N} \mu \frac{rR_{fuel} Y_{1n}}{Y_{1n}} = rR_{fuel} \quad \text{P} \quad \text{At NIF, } S/N \sim 200$$

## Predicted signal-to-noise (S/N) ratio for the different measurements at OMEGA and the NIF

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Implosion	$rR_{fuel}$ [mg/cm <sup>2</sup> ]	Facility	S/N (CR-39)	S/N (BC422)
Warm DT	~ 10	OMEGA	~ 40	~ 2
Cryo DT	~ 100	OMEGA	~ 400	~ 20
Cryo DT fizzle ( $9 \times 10^{14}$ )	~ 1000	NIF	~ 160	~ 200
Cryo D <sub>2</sub>	~ 1000	NIF	~ 1600	~ 200

## The remaining detected background can be separately characterized...

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- by moving the foil out of the spectrometer line of sight.
- by background monitors beside the focal plane detector.

# $rR_{\text{fuel}}$ measurements

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## Accuracy analysis of $rR_{fuel}$ measurements using the MRS at OMEGA

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The number of measured signal events ( $S$ ), which are generated by down-scattered neutrons, is linearly proportional to  $rR_{fuel}$ , and the relative statistical uncertainty in  $S$  can be expressed as

$$\frac{DS}{S} = \sqrt{\frac{rR_{fuel} + 6}{10^{-12} rR_{fuel}^2 Y_{1n}}} \quad (2)**$$

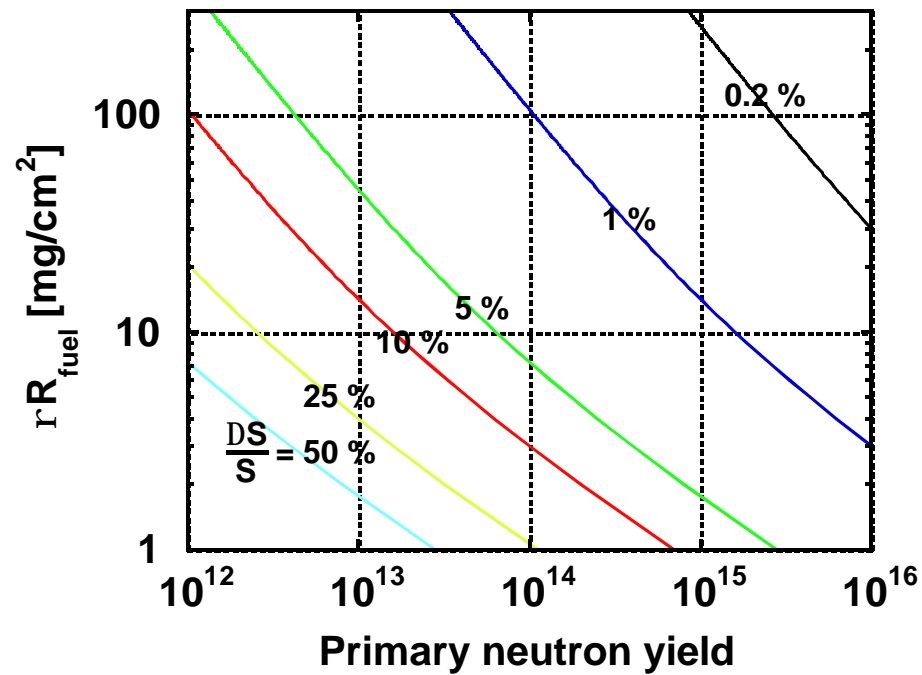
when operating the MRS at  $DE_i=3000$  keV.  $rR_{fuel}$  is given in mg/cm<sup>2</sup>. Eq. (2) can be rewritten as

$$rR_{fuel} = \frac{1}{2 \cdot 10^{-12} Y_{1n} \frac{DS}{S}} + \sqrt{\frac{1}{2 \cdot 10^{-12} Y_{1n} \frac{DS}{S}} + \frac{6}{2 \cdot 10^{-12} Y_{1n} \frac{DS}{S}}} \quad (3)$$

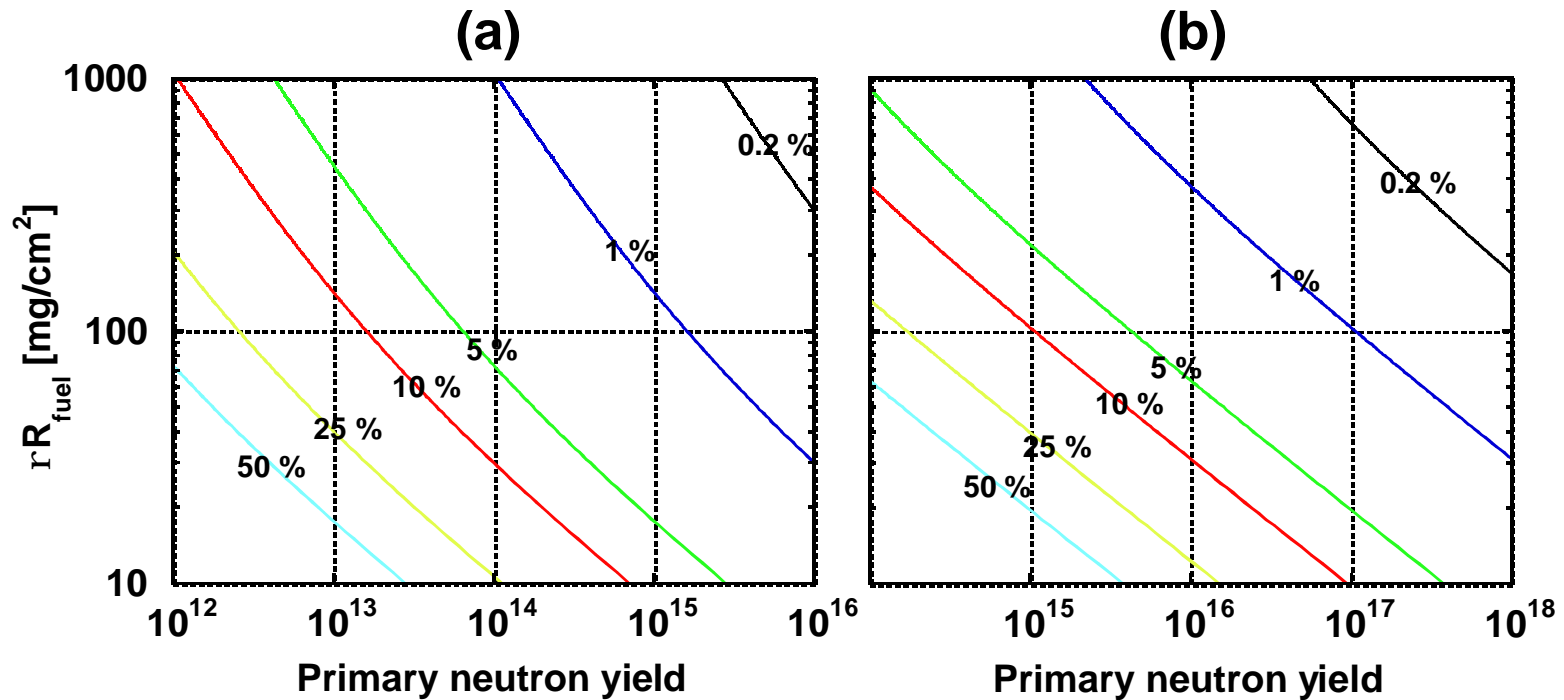
\*\* Eq. (2) assumes that  $S/B$  scales linearly with  $rR_{fuel}$ , which is the case for electronic detection.



# $rR_{\text{fuel}}$ vs Yield at OMEGA for different DS/S when operating the MRS at $DE_1 = 3000$ keV



$rR_{\text{fuel}}$  vs Yield at NIF for different DS/S when operating the MRS at  $DE_1 = 3000$  keV (a), and  $DE_1 = 250$  keV (b)

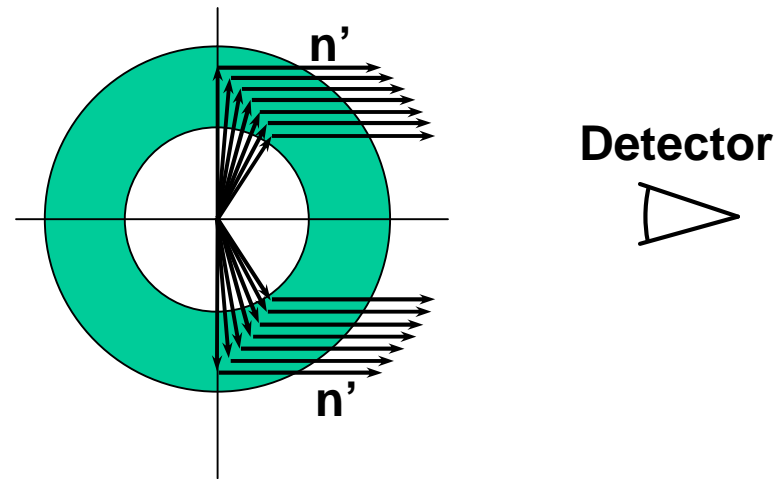
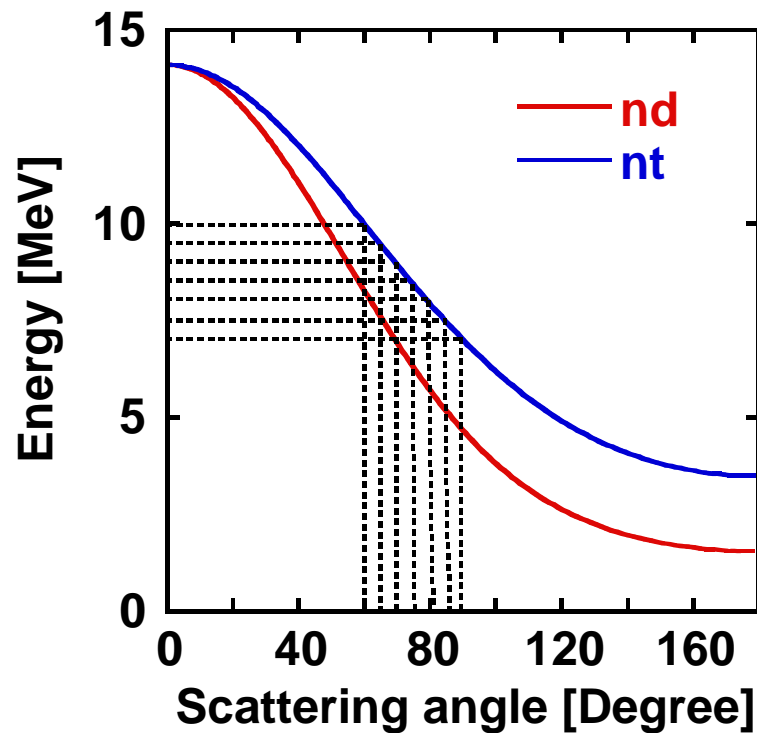


# Haan and Hatchett calculations

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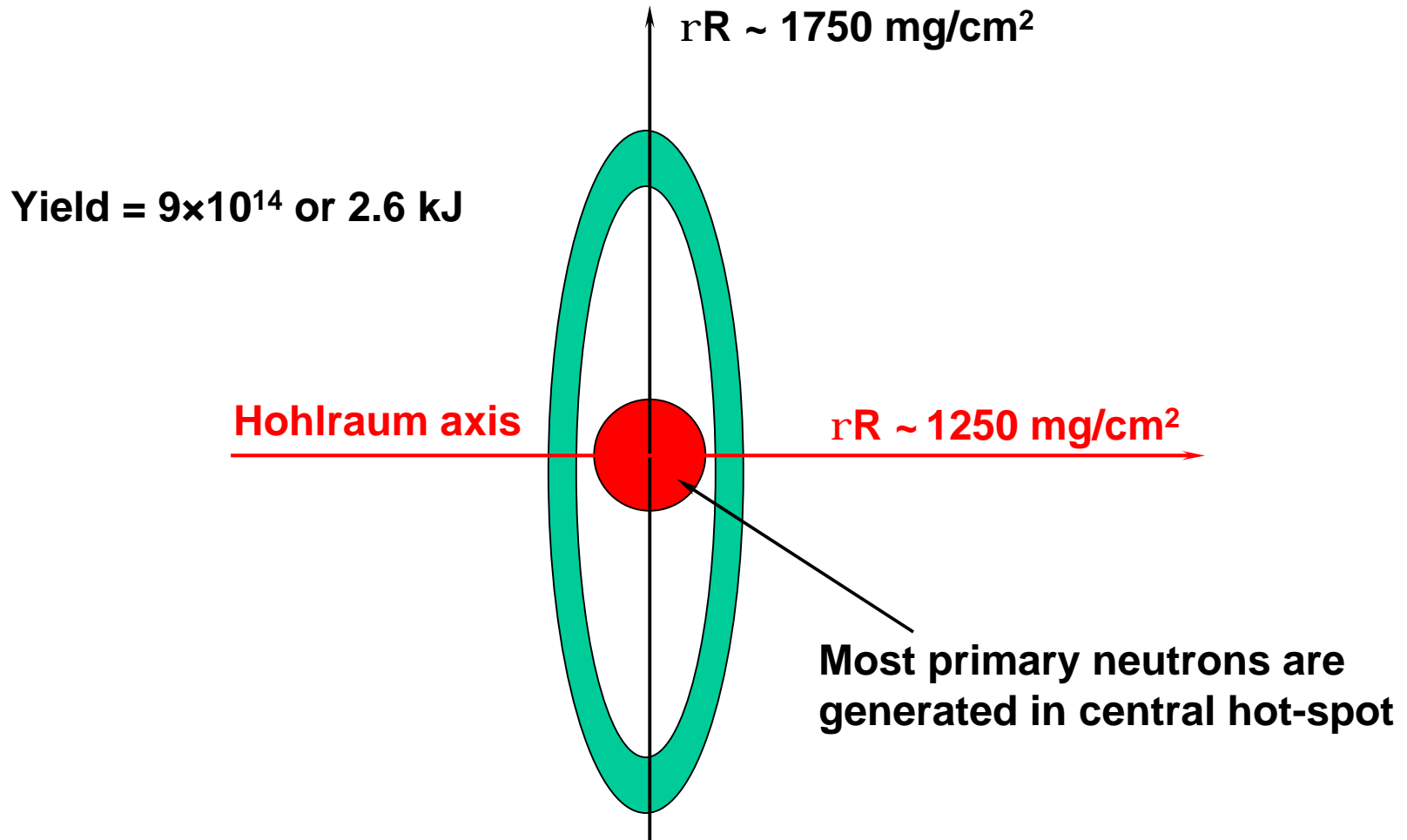
$rR_{fuel}$  asymmetries, at OMEGA and the NIF, could be inferred from yield of down-scattered neutrons in energy range 7-10 MeV

$$DE_1 = 500 \text{ keV} \Leftrightarrow DQ = 5^\circ$$



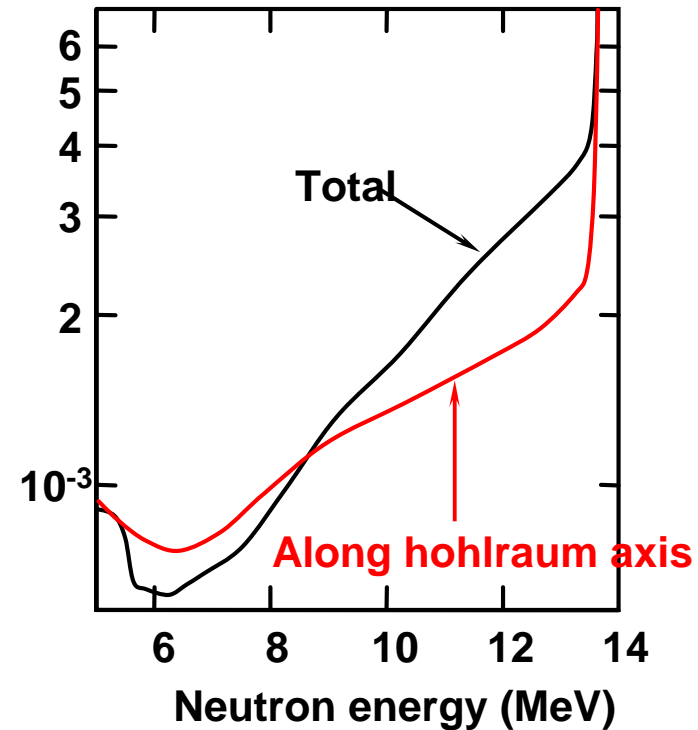
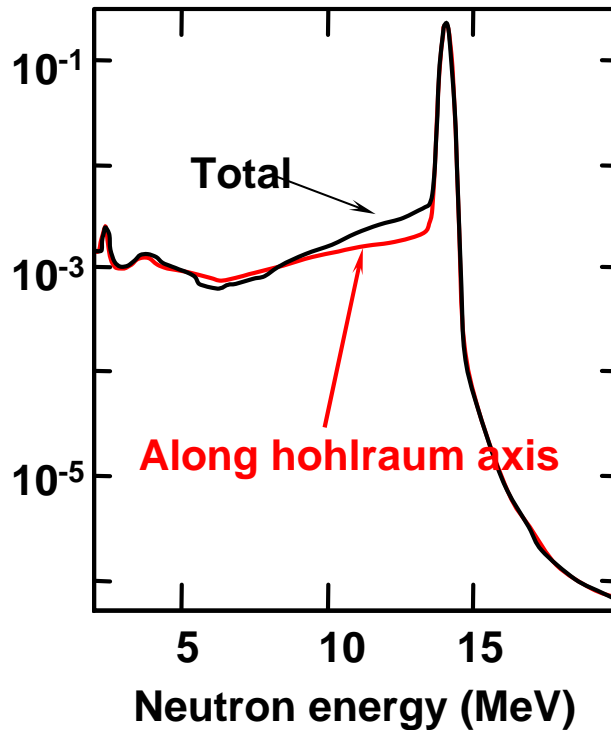
# Using down-scattered neutrons, $rR$ asymmetries of a pancaked $P_2$ Haan fizzle can be measured with MRS

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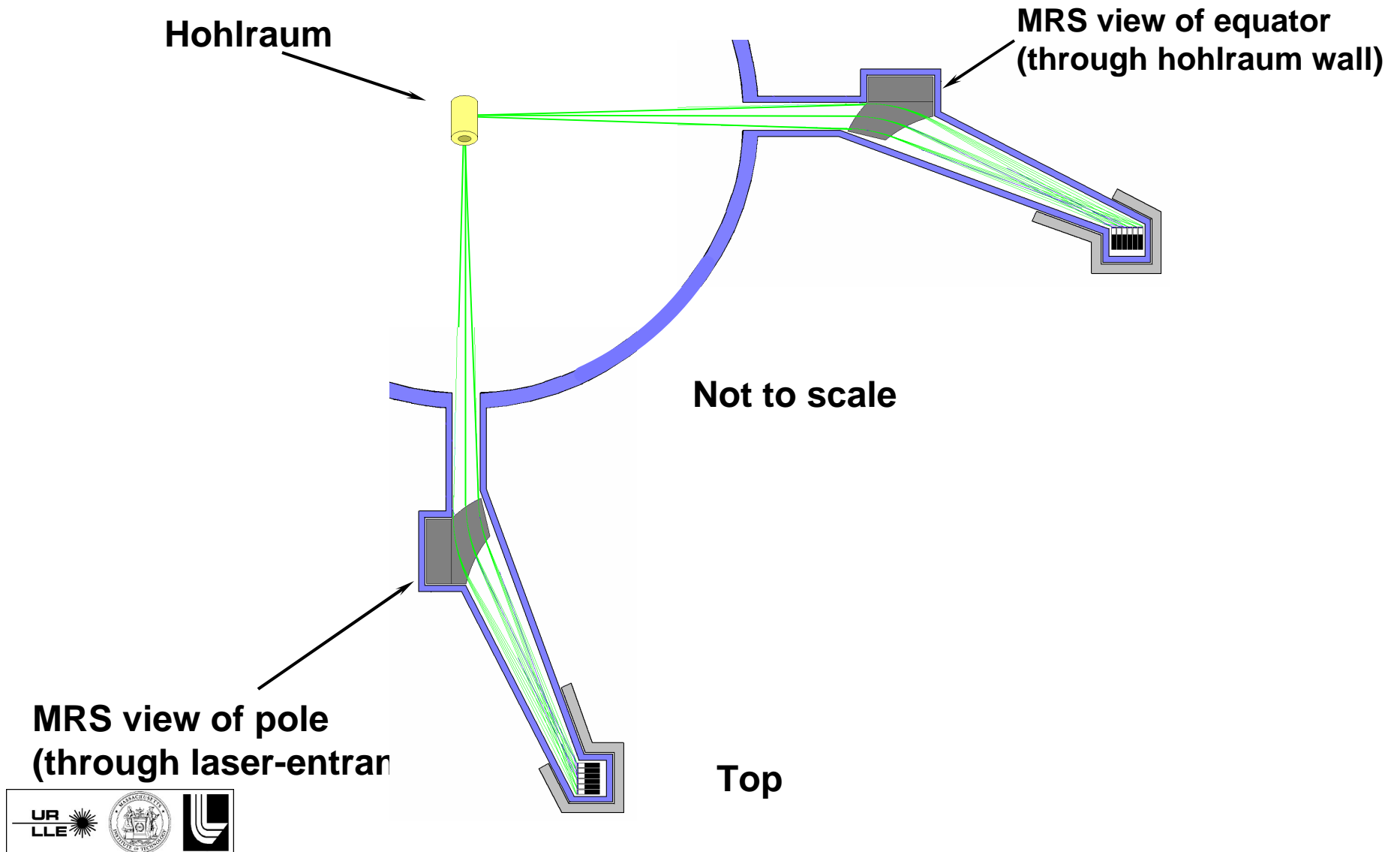
# With the MRS, rR asymmetries can be measured on NIF for this Haan P2 fizzle of $9 \times 10^{14}$

Neutrons/MeV (arbitrary scale, curves normalized to same integral)



$9 \times 10^{14}$  is about a factor 10 larger than is required to measure this rR asymmetry.

# Orthogonal MRS would be desirable at the NIF



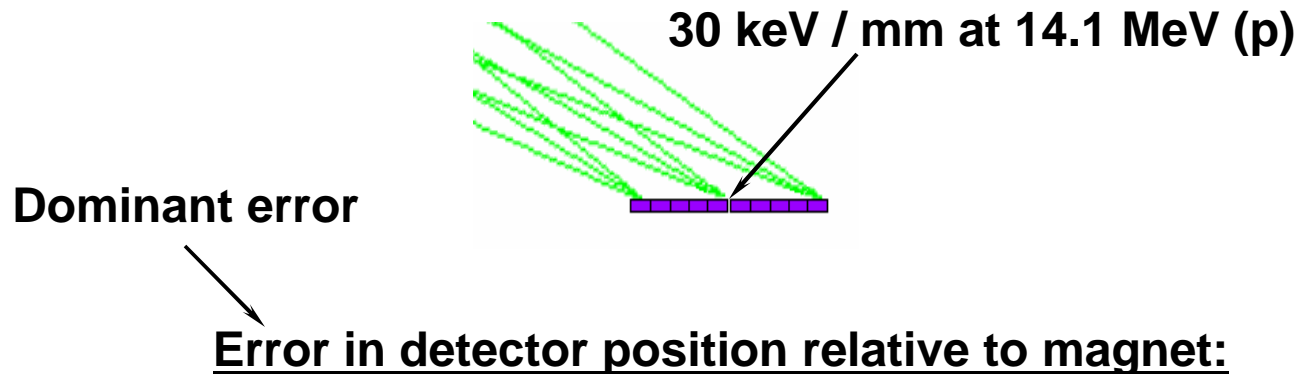
# $T_i$ measurements

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$T_i$  can be accurately measured with the MRS:  
 $DT_i = \pm 30 \text{ eV}$  (perfect statistics)

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$$Dx = \pm 1 \text{ mm}$$



$$DE = \pm 30 \text{ keV}$$



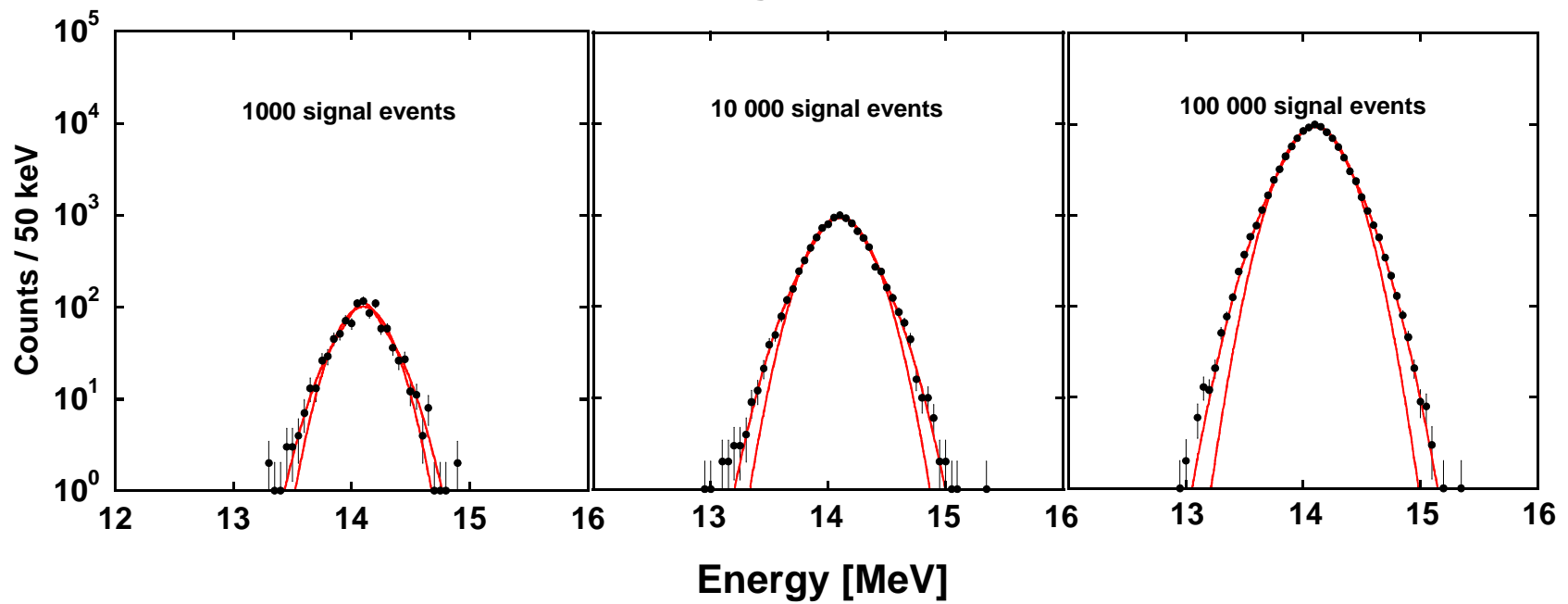
$$DE = 177\sqrt{T_i}$$



$$DT_i = \pm 30 \text{ eV}$$

# Using the CH-foil, the MRS can measure deviations from Maxwellian distributions when operated at $DE_1 = 250$ keV

A hot spot at 10 keV and surrounding cold plasma at 2 keV was assumed.  
(A model was used which resulted in comparable yields from the two regions.)



# $T_i$ measurement is affected by $DE_I$ , $DE_D$ and number of counts in spectrum

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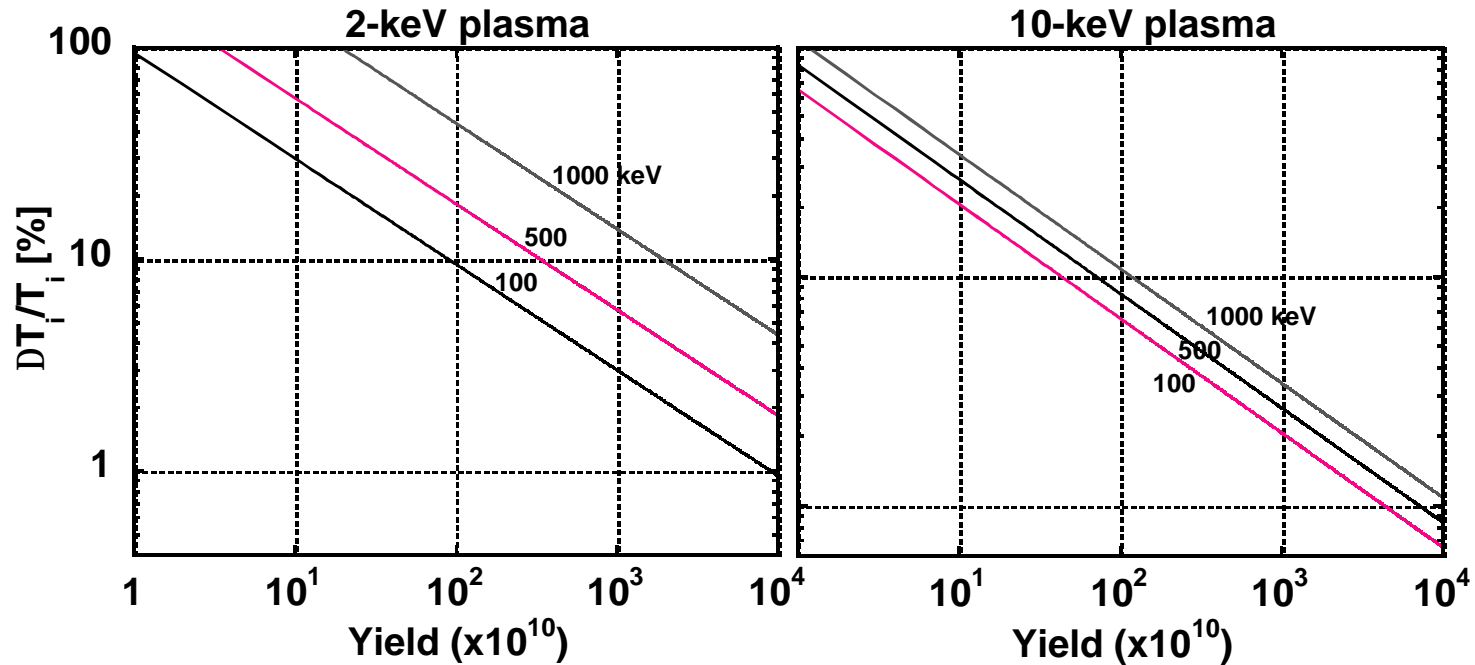
The relative statistical uncertainty in the  $T_i$  measurement can be expressed as

$$\frac{DT_i}{T_i} = \frac{1}{\hat{e}} + \frac{DE_I}{DE_D} \sqrt{\frac{2}{N}} \quad (1) **$$

$DE_I$  is the instrumental response function,  $DE_D$  is the Doppler broadening, and  $N$  is the number of counts in the spectrum.

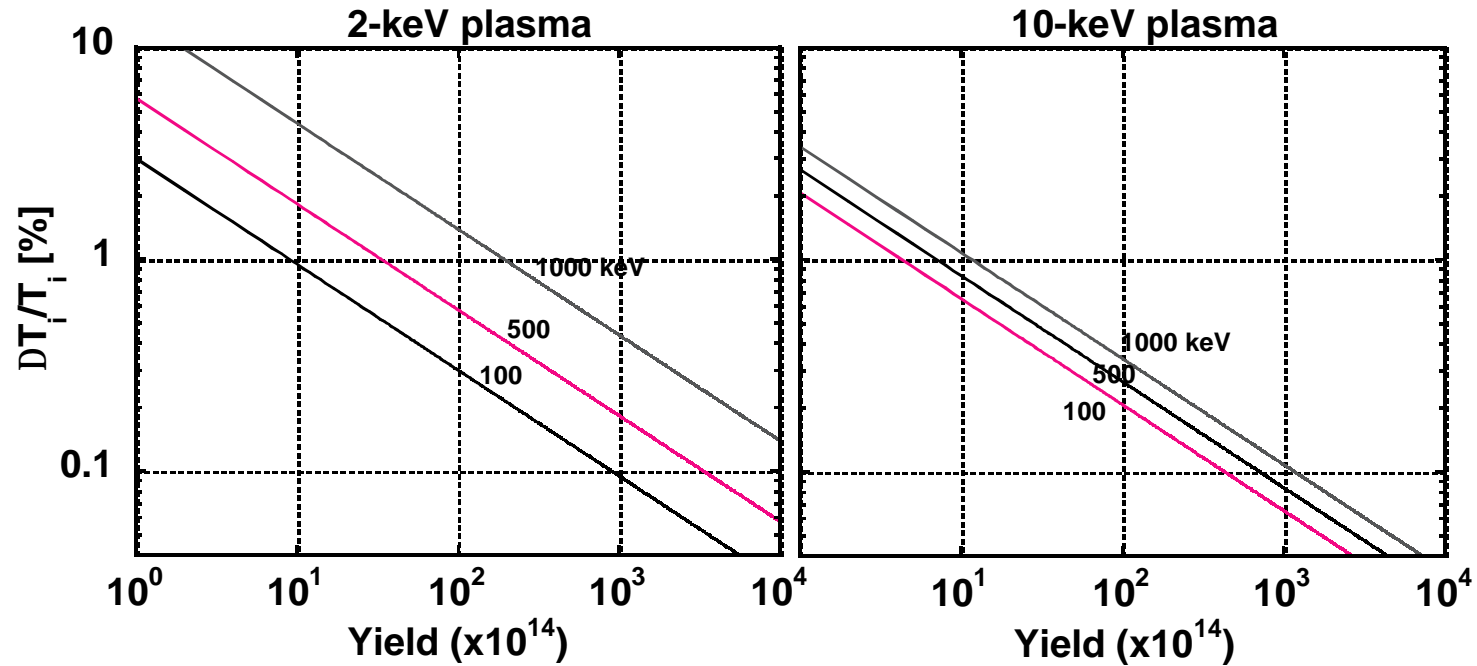
\*\* Eq. (1) assumes that the point response function is characterized very well, ie,  $D(DE_I) = 0$ . The equation also assumes that background is negligibly small.

# DT<sub>i</sub>/T<sub>i</sub> vs Yield at OMEGA for different instrumental point response functions DE<sub>i</sub>



$$\frac{DT_i}{T_i} = 1 + \frac{e}{e} \frac{DE_i}{DE_D} \sqrt{\frac{2}{3.3 \cdot 10^{-10} \text{Yield} \frac{DE_D}{100 \text{keV}}}} = N$$

# DT<sub>i</sub>/T<sub>i</sub> vs Yield at the NIF for different instrumental point response functions DE<sub>i</sub>



$$\frac{DT_i}{T_i} = 1 + \frac{DE_i}{DE_D} \sqrt{\frac{2}{3.3 \cdot 10^{-11} \text{Yield} \frac{DE_D}{100 \text{keV}}}} = N$$