

# Overview of the Current Status of Shock Ignition



**P. W. McKenty**  
**University of Rochester**  
**Laboratory for Laser Energetics**

**Omega Laser Facility**  
**Users' Group Workshop**  
**Rochester, NY**  
**27–29 April 2011**

# Workshop discussions focused on target design and understanding the effects of LPI on target performance

---



## Target design

- Design viable implosion platforms over a variety of facilities
- Develop a wide database evaluating strengths and faults of shock-ignition (SI) designs
- Design experimental platforms for OMEGA and the NIF

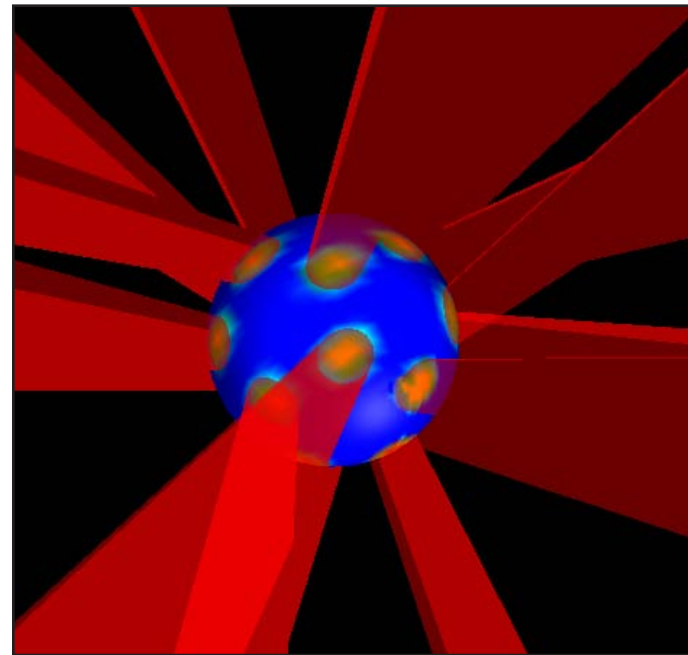
## LPI

- Identify, quantify, and mitigate preheat during the fuel-assembly phase
- Determine the benefits and detriments of spike-pulse preheat
  - enhanced drive
  - fuel-assembly preheat
  - backscatter losses

# Contributors

---

**K. S. Anderson (LLE)**  
**R. Nora (LLE)**  
**C. Stoeckl (LLE)**  
**W. Theobald (LLE)**  
**J. Bates (NRL)**  
**A. Schmitt (NRL)**  
**M. Lafon (CELIA)**  
**X. Ribeyre (CELIA)**  
**G. Schurtz (CELIA)**  
**S. Weber (CELIA)**  
**V. Tykhonchuk (CELIA)**  
**S. Atzeni (U. Rome)**  
**J. Perkins (LLNL)**  
**O. Klimo (CTU)**  
**and others...**



# The puzzle of high gains: how to ignite low-velocity imploding targets



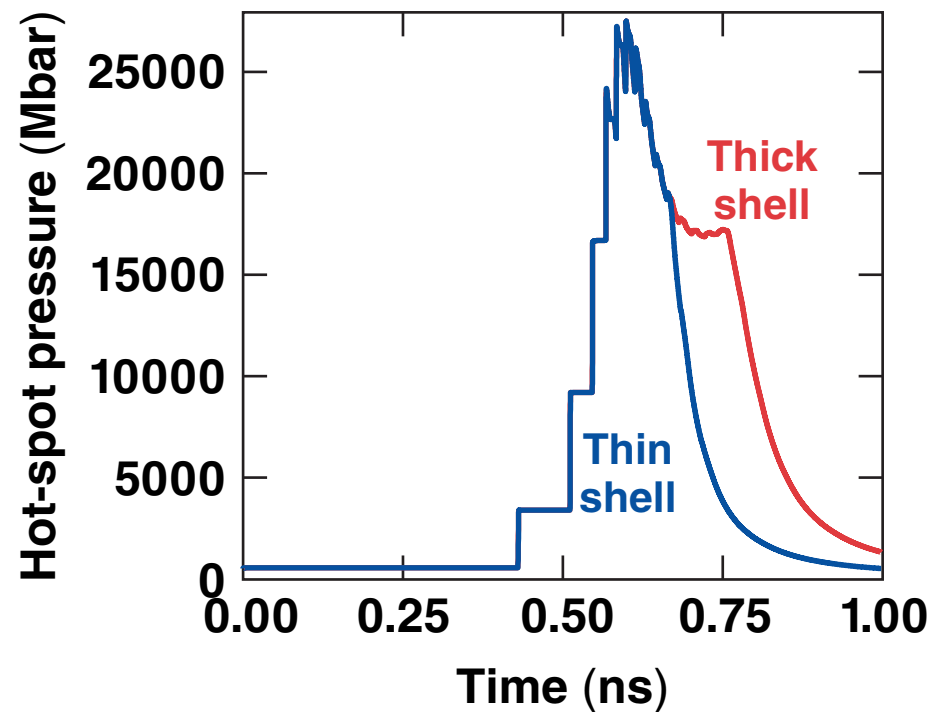
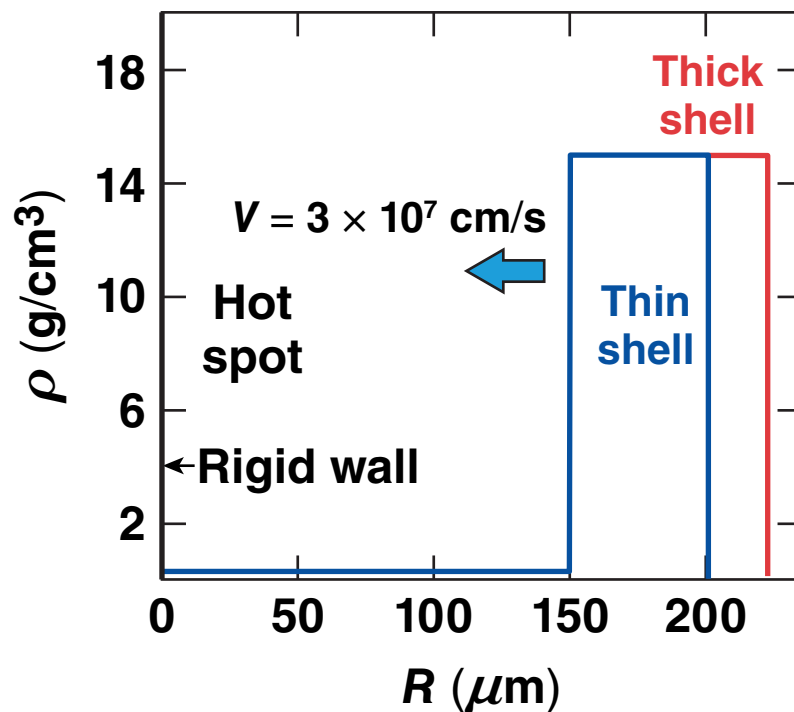
- Thick shells (with large fuel mass) produce high gains if ignited
- Thick shells have good hydro-stability properties (because they are thick)
- For a fixed laser energy, thick shells have low-implosion velocity
- Low-implosion velocity leads to low hot-spot pressure ( $P \sim V_i^{2-3}$ )
- Low-pressure hot spots do not ignite ( $P\tau > 30$  Gbar/ns)
- The energy required for ignition scales as  $E \sim 1/P^{2-2.5}$

**How do we ignite low-velocity implosions?**

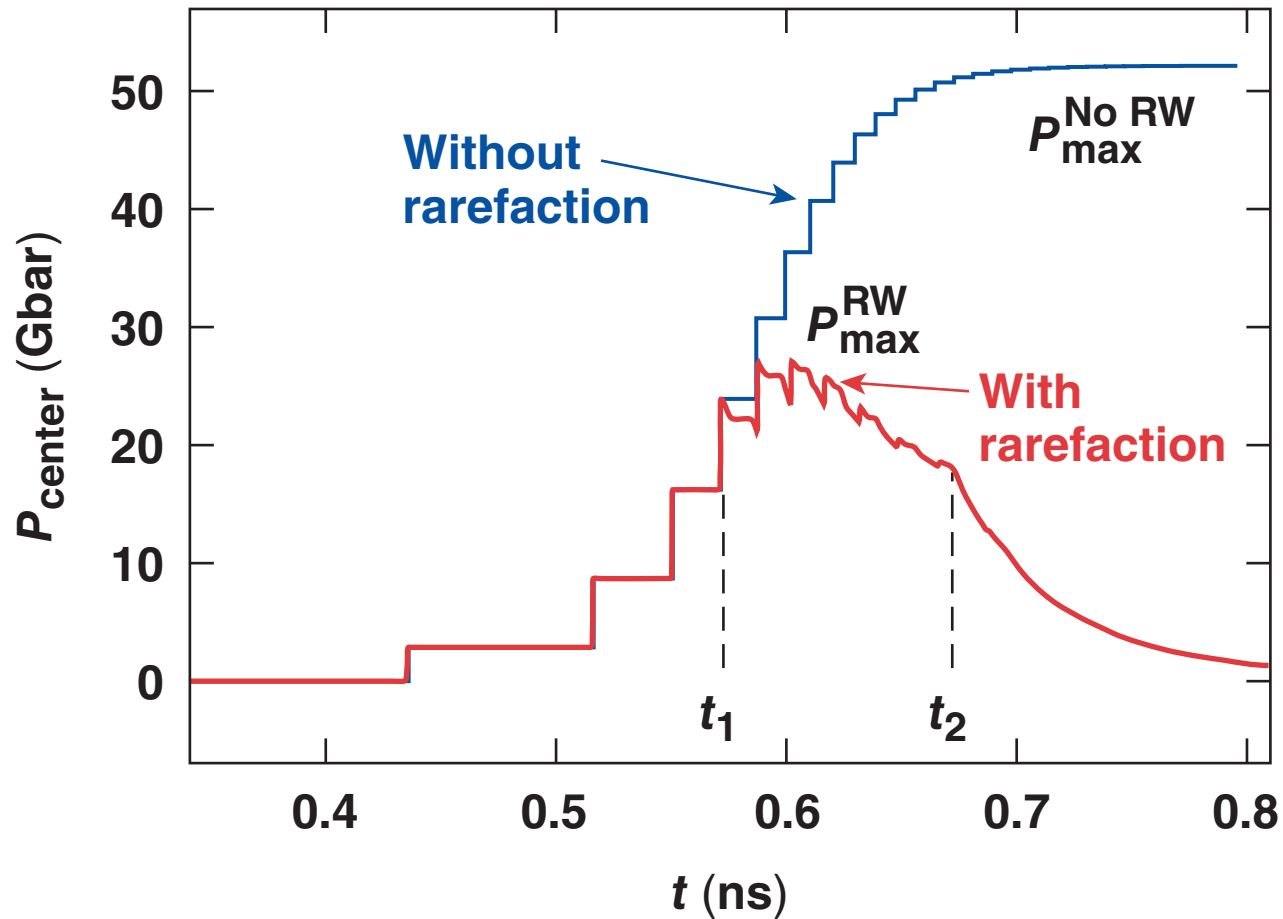
# Raising the kinetic energy by thickening the shell does not increase the hot-spot pressure



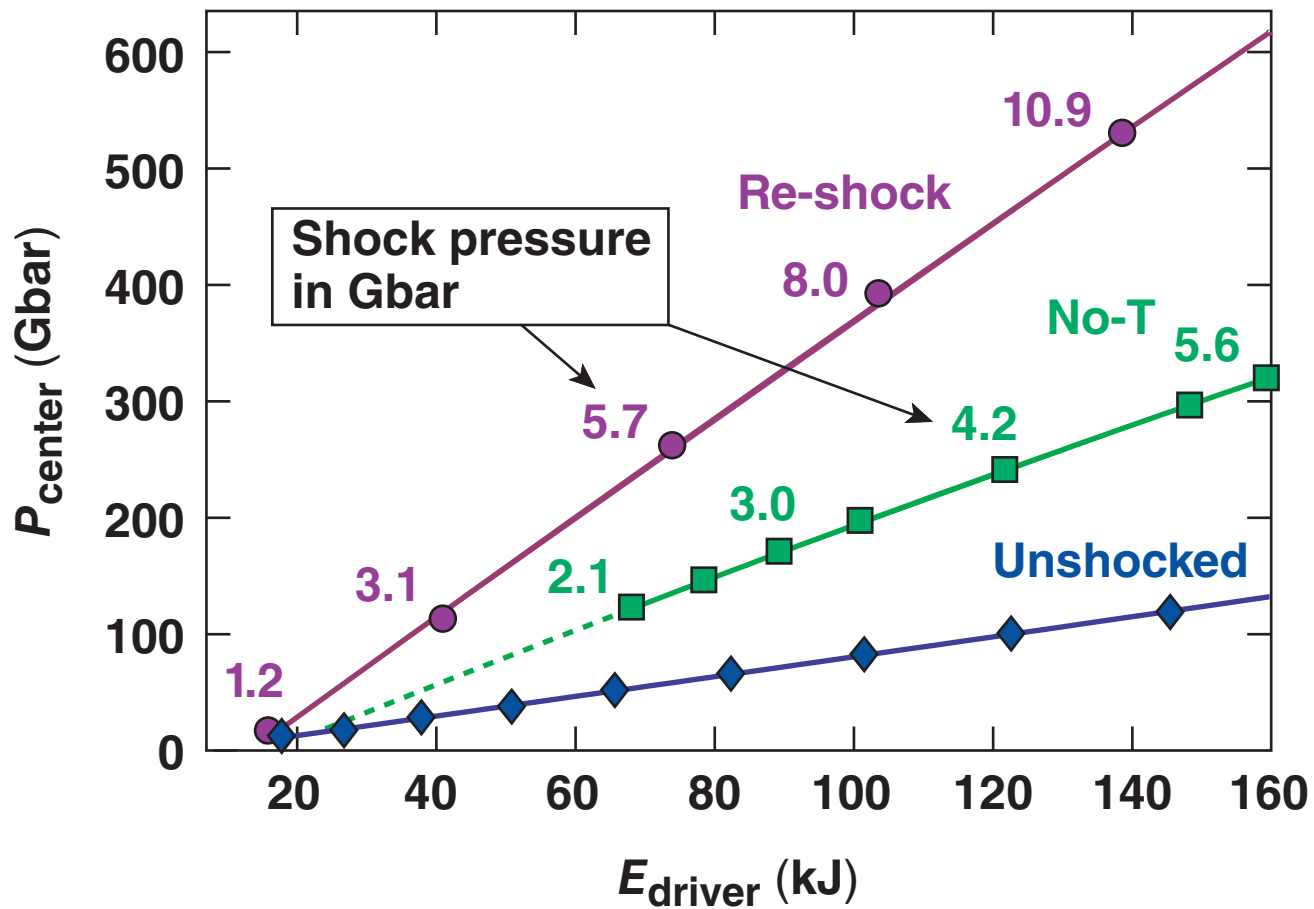
Planar model of a compressible dense slab/shell compressing a low-density gas



# Without rarefaction waves, the peak hot-spot pressure would be twice as high



# The re-shock technique produces the highest hot-spot pressure

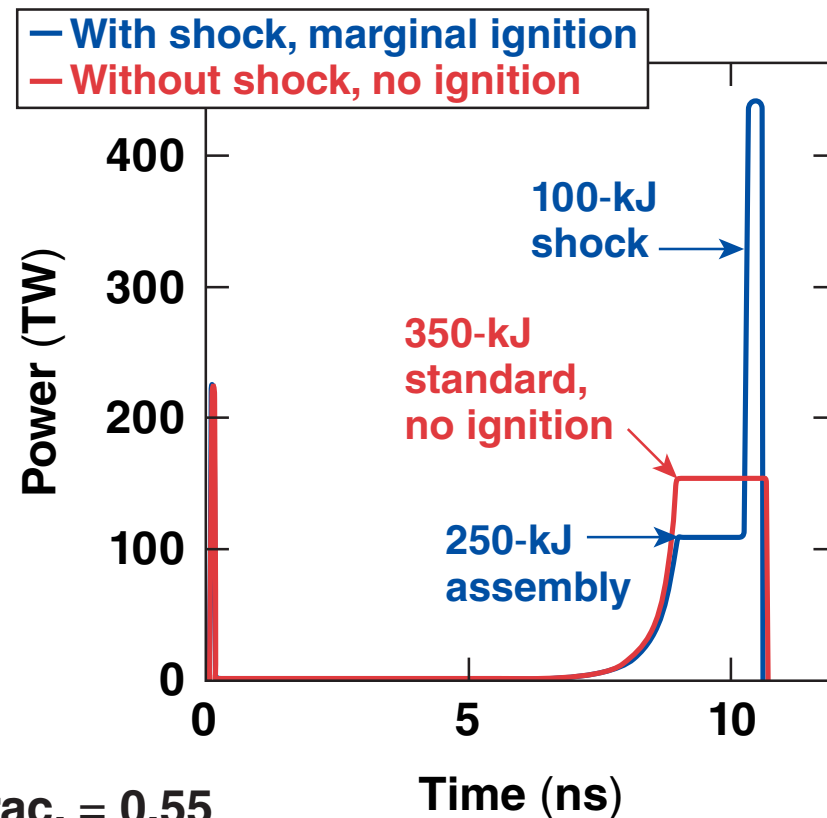
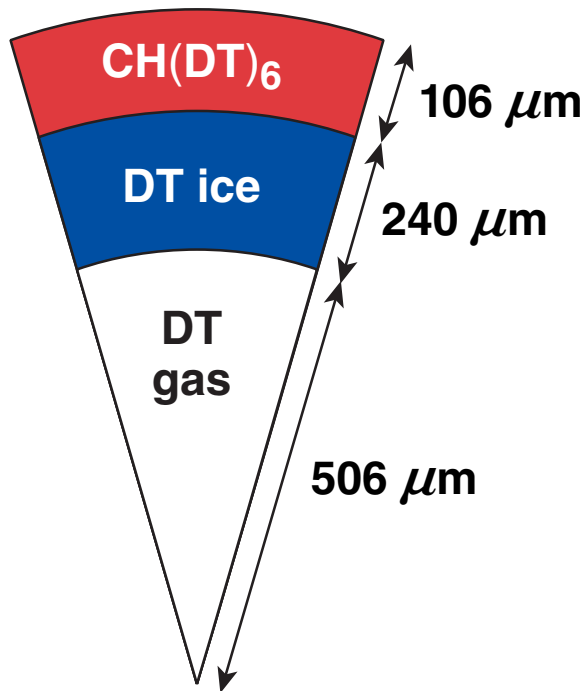


The shock pressure is high because of the planar geometry

# Optimal shock-ignition targets are wetted-foam shells (in the absence of hot-electron preheat)



$E_L = 350\text{-kJ UV light}$ ,  $V_i = 2.4 \times 10^7 \text{ cm/s}$ ,  $\alpha = 1$ ,  $\lambda_L = 0.35 \mu\text{m}$

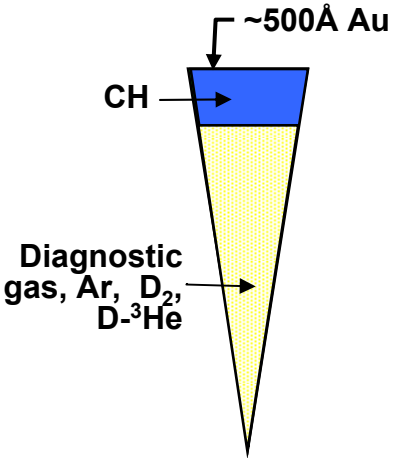
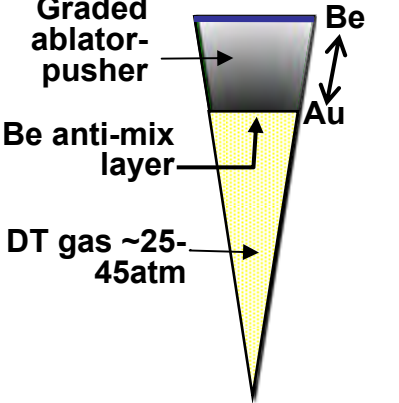
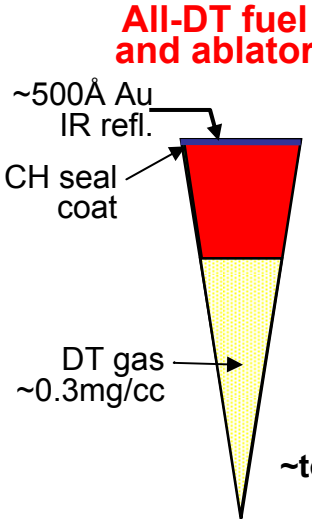
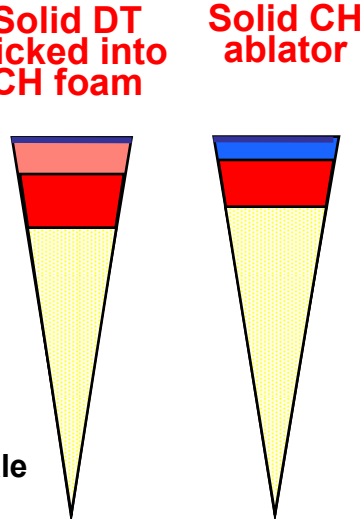


- Standard pulse-shape abs. frac. = 0.55
- Shock-ignition pulse-shape abs. frac. = 0.50



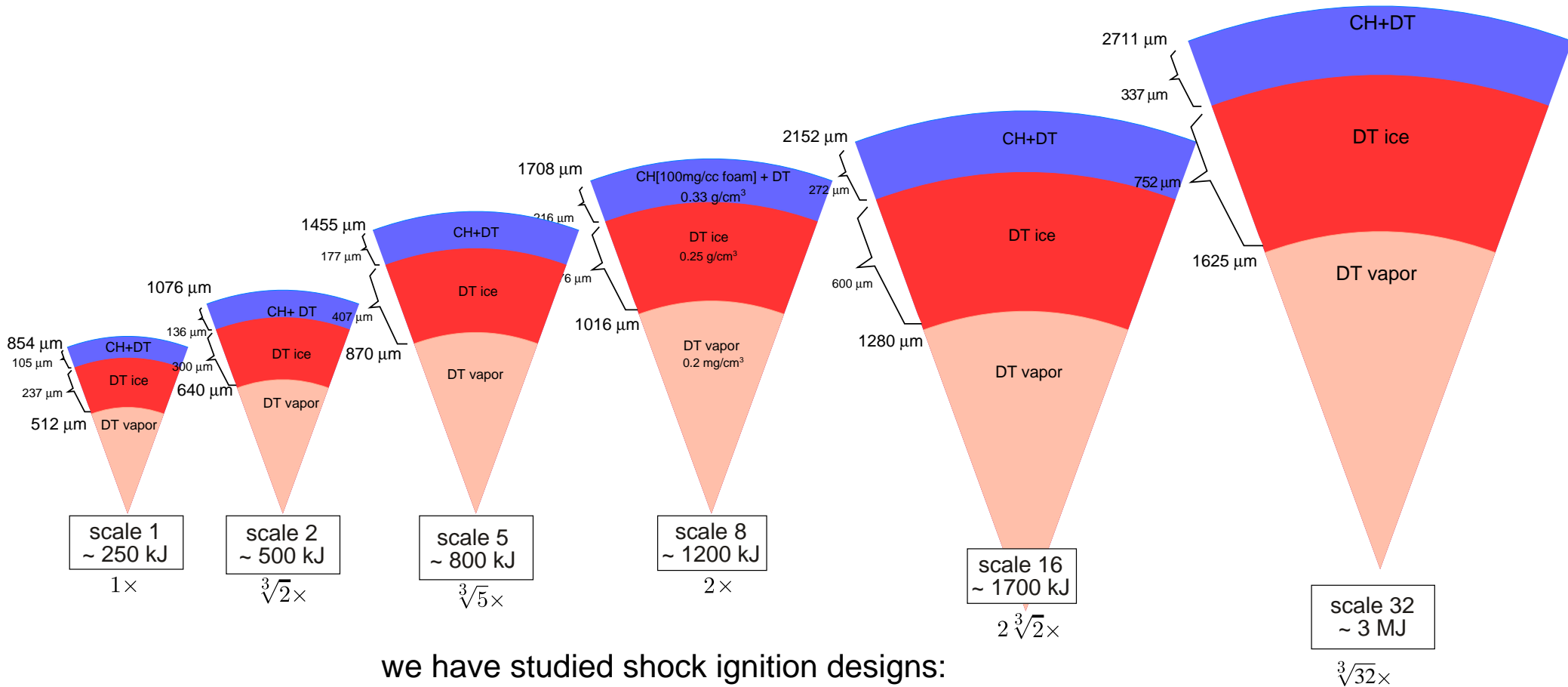


# Candidate NIF shock ignition targets

Non-Cryo Hydro-Equiv. CH	Non-Cryo Pushered Single Shell	High Gain Cryo	
			
<ul style="list-style-type: none"> <li>• Immediate term (~1-3yr) tests of polar drive symmetry, shock coupling, late-time LPI with day-1 hardware</li> <li>• Diagnostic yields only at ~0.5MJ drive</li> </ul>	<ul style="list-style-type: none"> <li>• Near term (~3yr) tests of room-temp volumetric ignition at ~4keV</li> <li>• Gain/yield ~1/1MJ @ ~1.5MJ drive</li> <li>• Req'd NIF hardware?</li> </ul>	<ul style="list-style-type: none"> <li>• Medium term (~4+yr) tests of high gain shock ignition @ &lt;1MJ</li> <li>• Gain/yield ~60/30MJ @ 0.5MJ drive</li> <li>• Req'd NIF hardware?</li> </ul>	<ul style="list-style-type: none"> <li>• Longer term (≥6yr) tests of high yield shock ignition</li> <li>• Gain/yield ≥100/100MJ @ ≥1MJ drive</li> </ul>

# Overview: shock ignition targets designed for high gain with KrF

NRL



we have studied shock ignition designs:

- low-aspect (AR=2.5) foam/DT targets
- driven by 248 nm KrF light
- laser spot size is zoomed twice
- target mass varied by a scale factor of 32  
(scale 1 = ~250 kJ - scale 32 = ~3 MJ targets)
- target adiabat is kept moderately low ( $\alpha\sim 2$ )

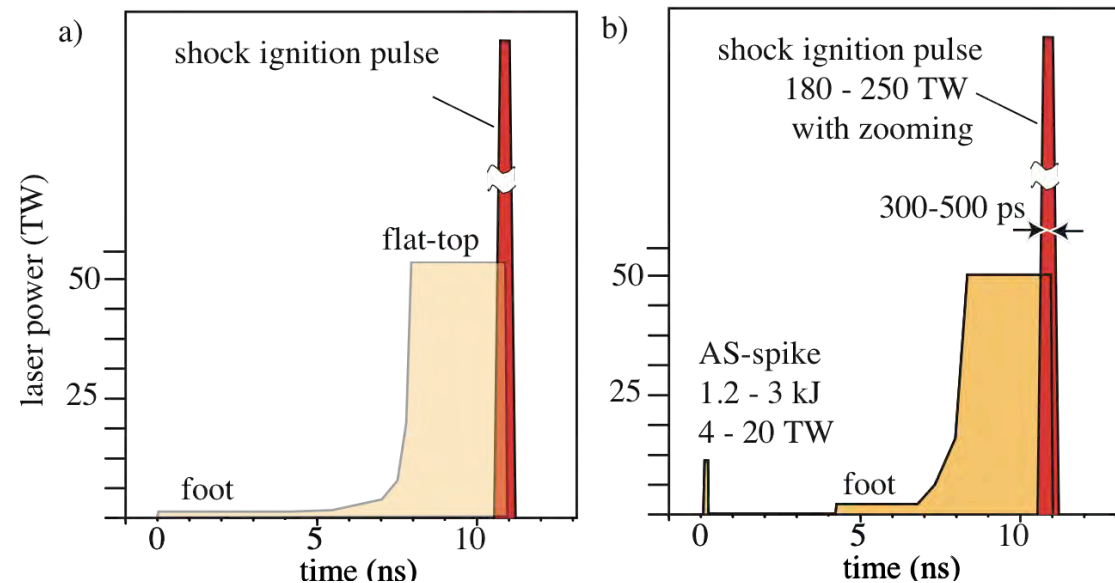
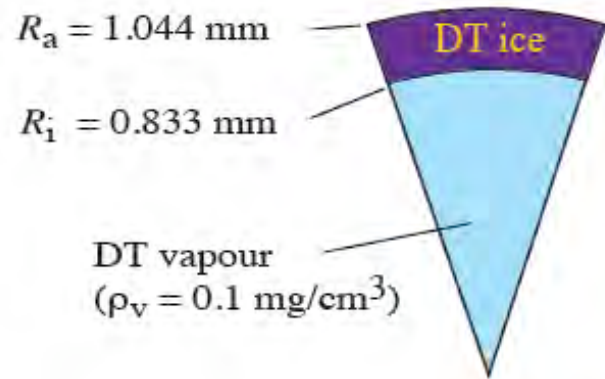


# HiPER baseline target -- Shock-ignition



Target: HiPER baseline target

Laser wavelength =  $0.35 \mu\text{m}$   
Compression energy: 180 kJ  
Focal spot: 0.64 mm (compression)  
0.4 mm (SI)



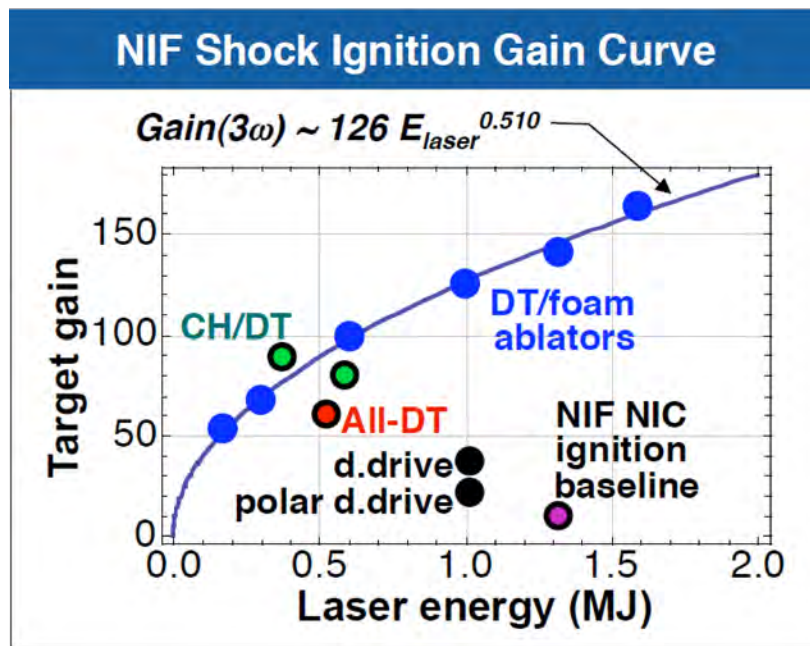
Target: S. Atzeni, A. Schiavi and C. Bellei, PoP, **15**, 14052702 (2007)

Pulses: X. Ribeyre *et al*, PPCF **51**, 015013 (2009);

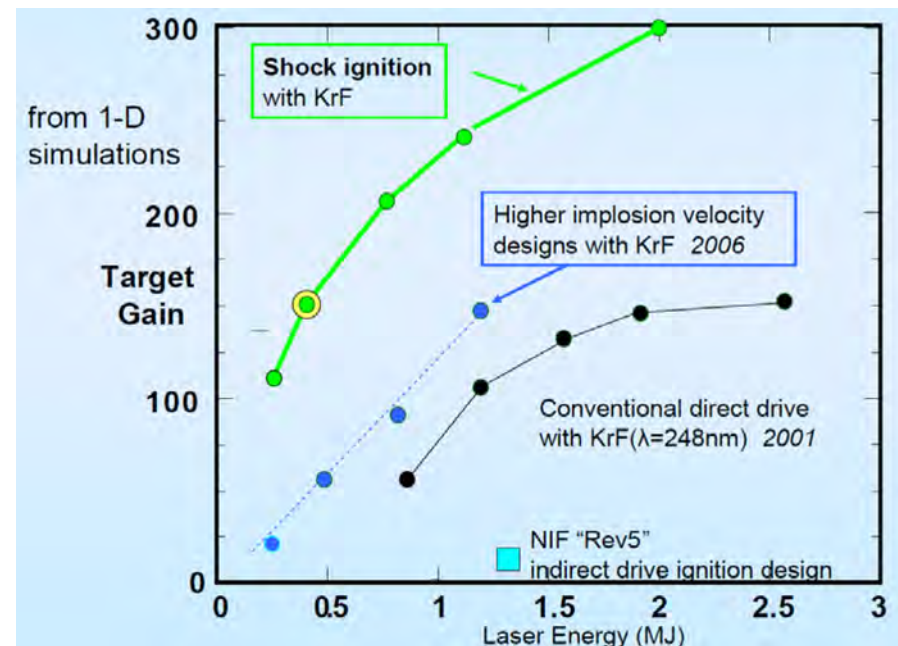
S. Atzeni, A. Schaivi, A. Marocchino, PPCF (2011)



# Gain curves for shock ignition look impressive but must assess the sensitivity to preheat (during the main pulse) and (for CH targets) to laser imprinting



L. J. Perkins (LLNL)



A. Schmitt (NRL)



# Shock ignition: pros & issues



## PROS

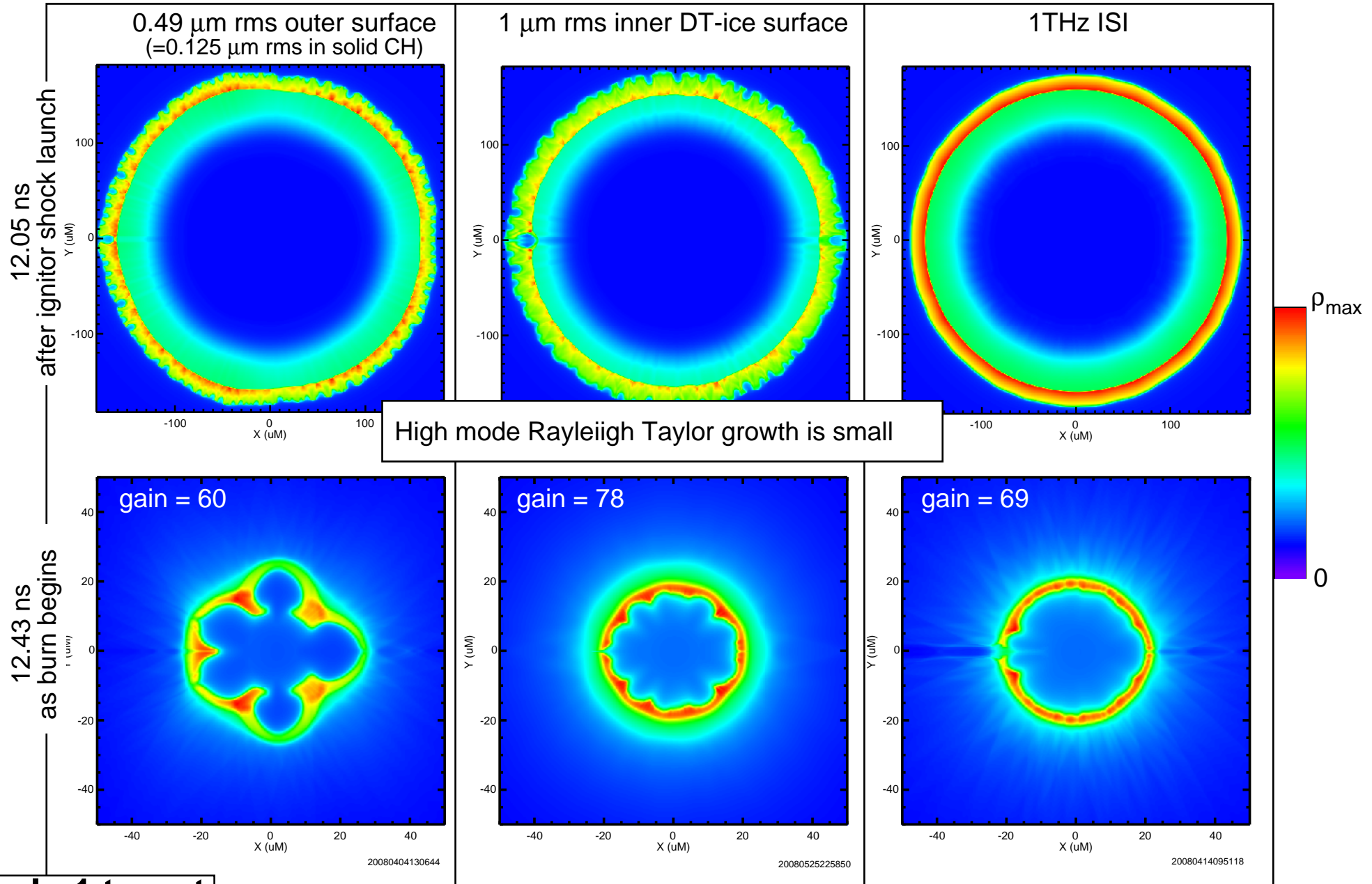
- Implosion velocity smaller than for central ignition
  - ⇒ Lower intensity, smaller RTI growth ⇒ more room for direct-drive
  - ⇒ Potentially higher gain
- Ignition configuration: Non isobaric ⇒ higher gain (than central ignition)
- Spherical targets

## ISSUES, DESERVING EXPERIMENTS (@ NIF, Omega?)

- Laser-plasma interaction at  $10^{16}$  W/cm<sup>2</sup>: backscattering? Hot electrons?
- Energy transport at above intensity
- Shock propagation through perturbed materials

## MEANWHILE: WHAT ABOUT ROBUSTNESS?

# Three different sources have been simulated: outer and inner surface perturbations and laser imprint.

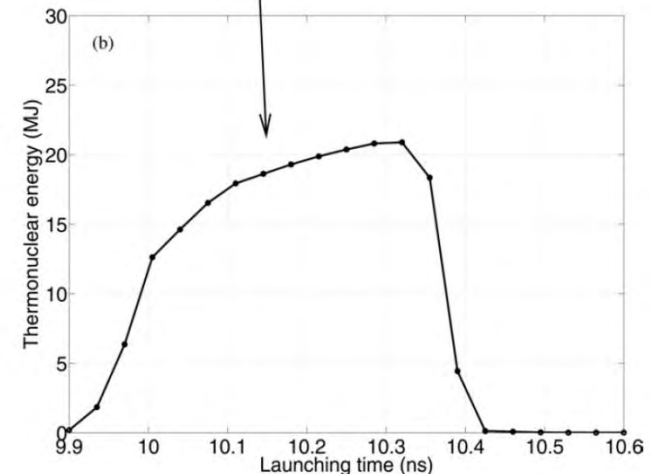
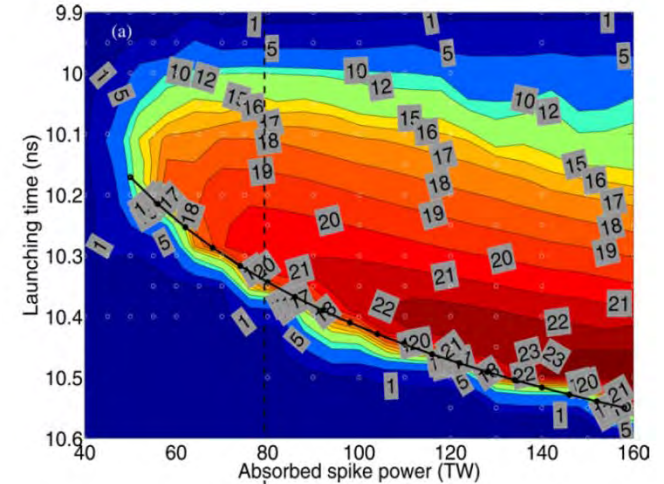
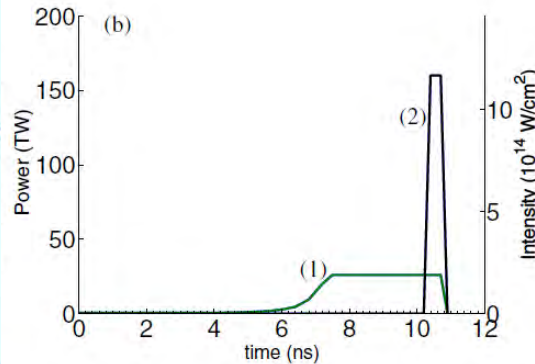
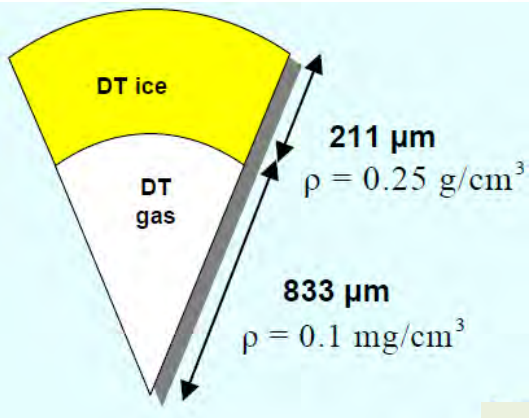
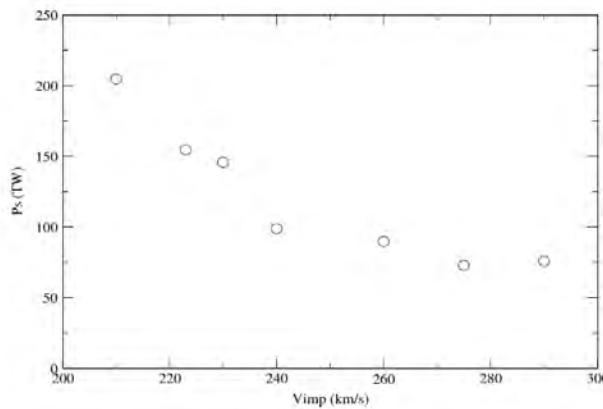


scale 1 target

# The spike power and launching time are optimized for HiPER shock ignition targets

## HiPER shock ignition target

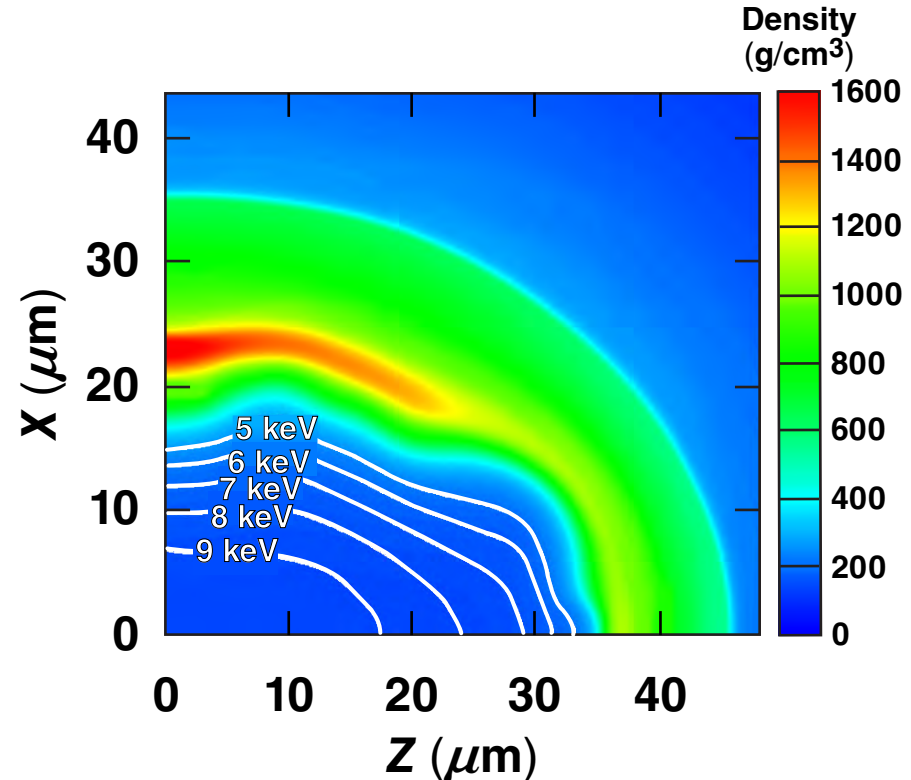
Initial aspect ratio	$\approx 5$
In-flight aspect ratio	$\approx 35$
In-flight mass (mg)	$\approx 0.28$
Implosion velocity ( $\text{km s}^{-1}$ )	$\approx 290$
Adiabat parameter	$\approx 1.0$
Peak density ( $\text{g cm}^{-3}$ )	$\approx 625$
Peak areal density ( $\text{g cm}^{-2}$ )	$\approx 1.50$



# Symmetric 2-D *DRACO* simulations performed with similar targets indicate robustness to ice roughness $>3.5\text{-}\mu\text{m rms}$



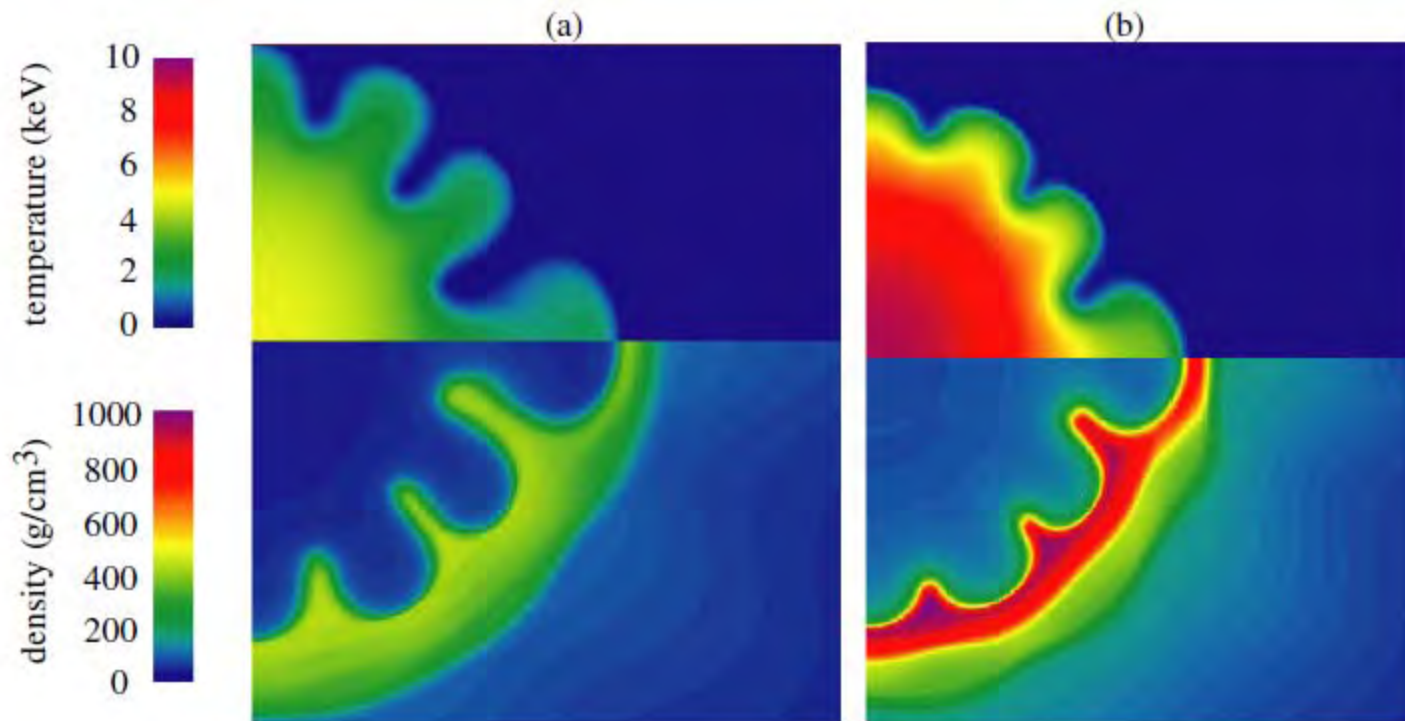
- Symmetric laser irradiation
- *DRACO* simulations with  $3.5\text{-}\mu\text{m-rms}$  roughness in modes  $\ell = 2$  to 50
- Target ignites with full gain
- Upper limit on robustness to ice modes not yet explored
- Other nonuniformity studies to follow (imprint, target offset, polar drive, etc.)





# Ignitor-return shock collision seems to reduce the deceleration RTI growth before ignition

---



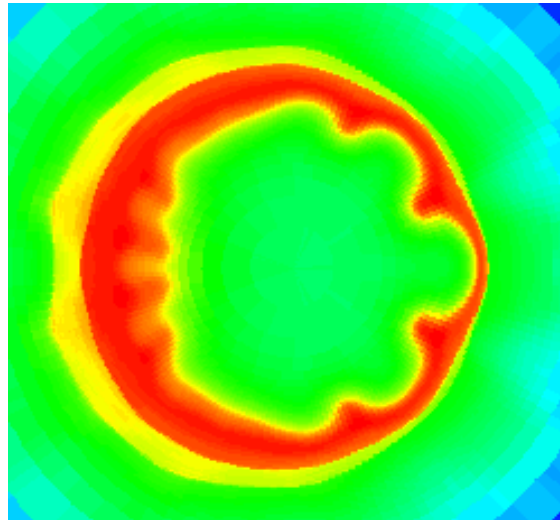
Atzeni, Davies, Hallo, Honrubia, Maire, Olazabal, Feugeas, Ribeyre, Schiavi, Schurtz, Breil, Nicolai, Nucl. Fusion 49, 055008 (2009)



# Shock-ignition: sensitive to mispositioning

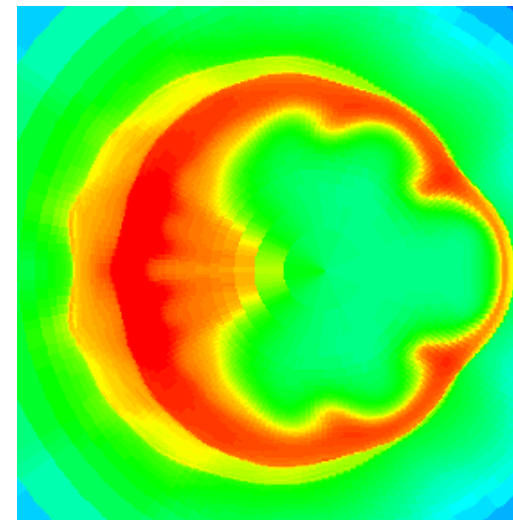


Density maps when central  $T_{\text{ion}} = 10 \text{ keV}$   
( $80 * 80 \mu\text{m}$ )



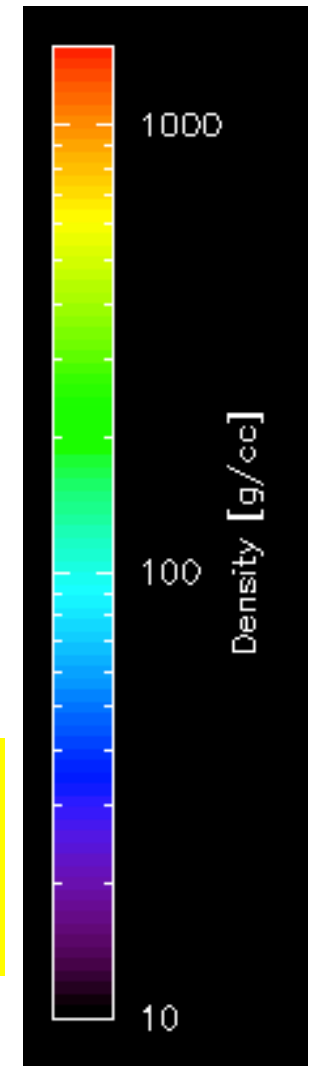
10  $\mu\text{m}$  displacement

**Gain = 95% of 1D gain**



20  $\mu\text{m}$  displacement

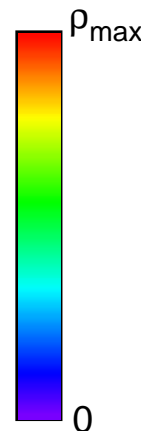
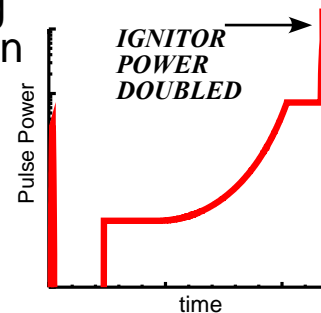
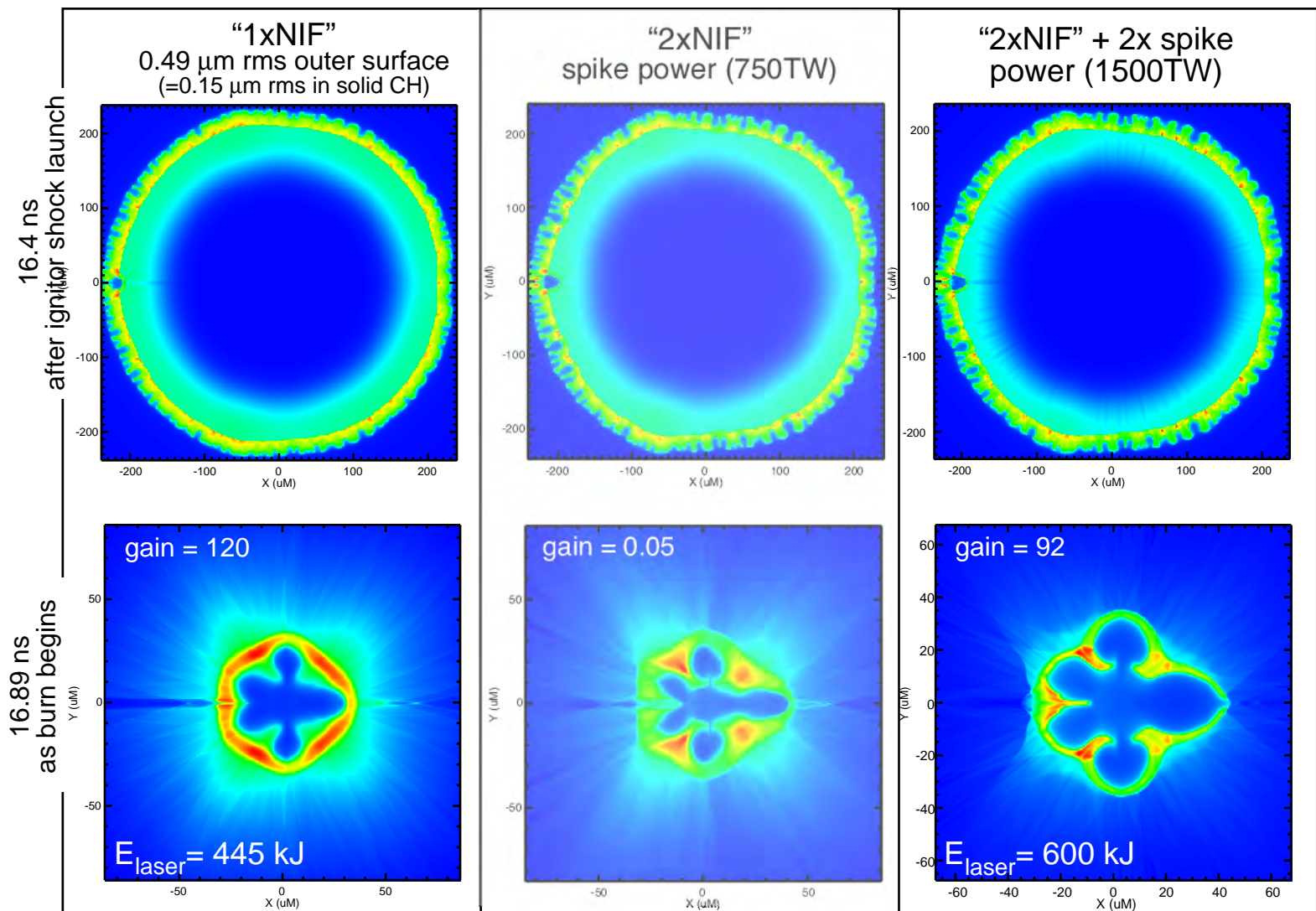
**Gain = 1% of 1D gain**



# ...But increasing the ignitor power restores significant gain



fixed:  
doubling the surface roughness **and** doubling spike power recovers gain



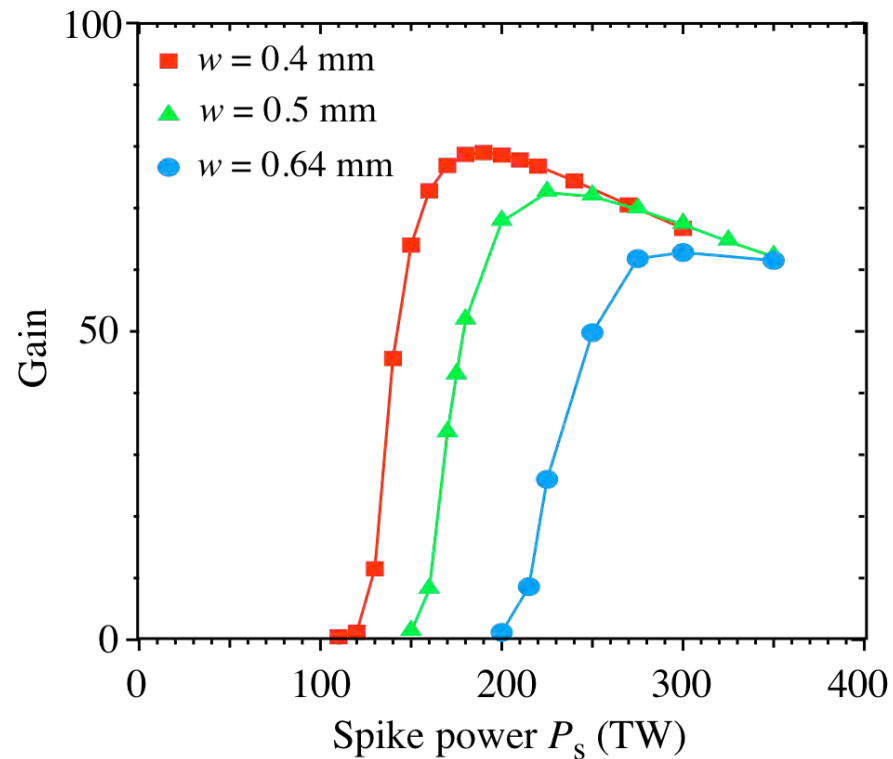
scale 2 target



# Zooming required to reduce spike power



HiPER target



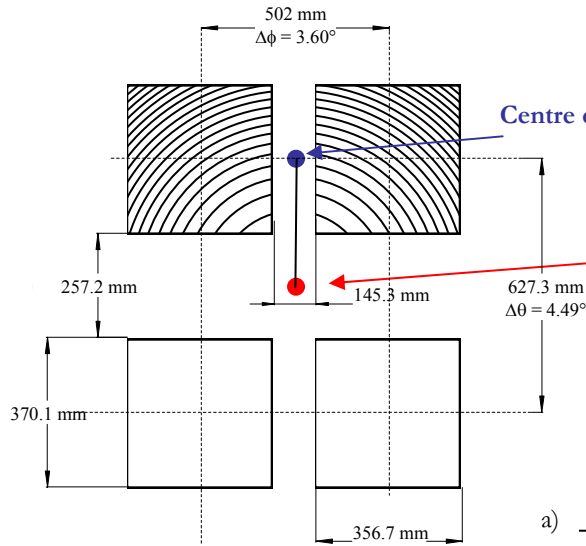
Gaussian beams, width  $w_s$

$w_s$	min. spike power
400 $\mu\text{m}$	150 TW
500 $\mu\text{m}$	200 TW
640 $\mu\text{m}$	270 TW



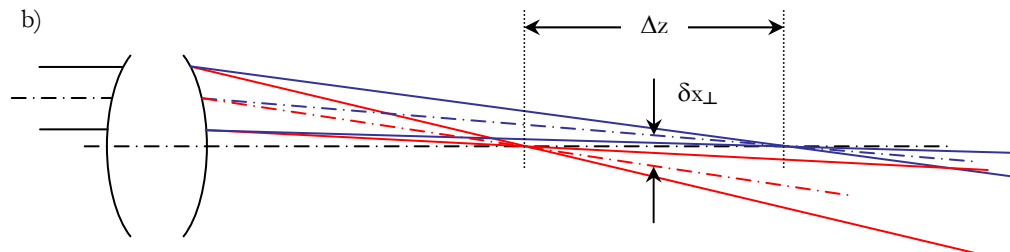
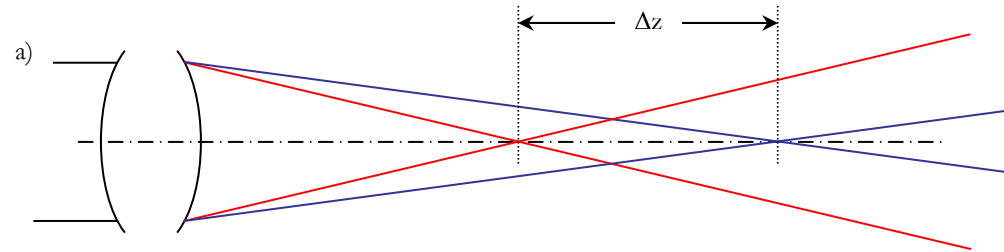
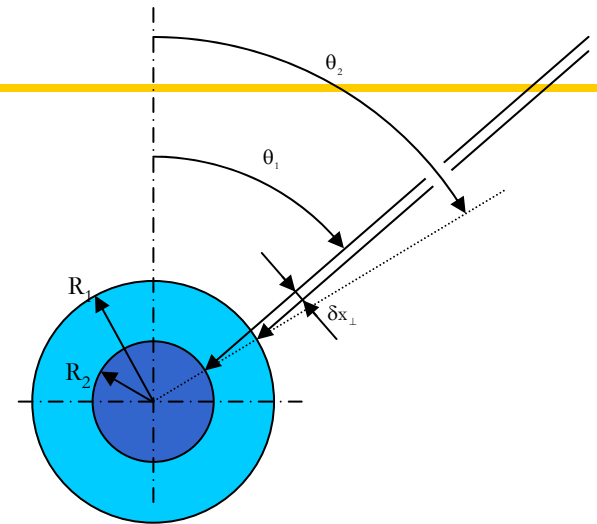


# Dynamic repointing seems achievable on LMJ



Centre des deux faisceaux

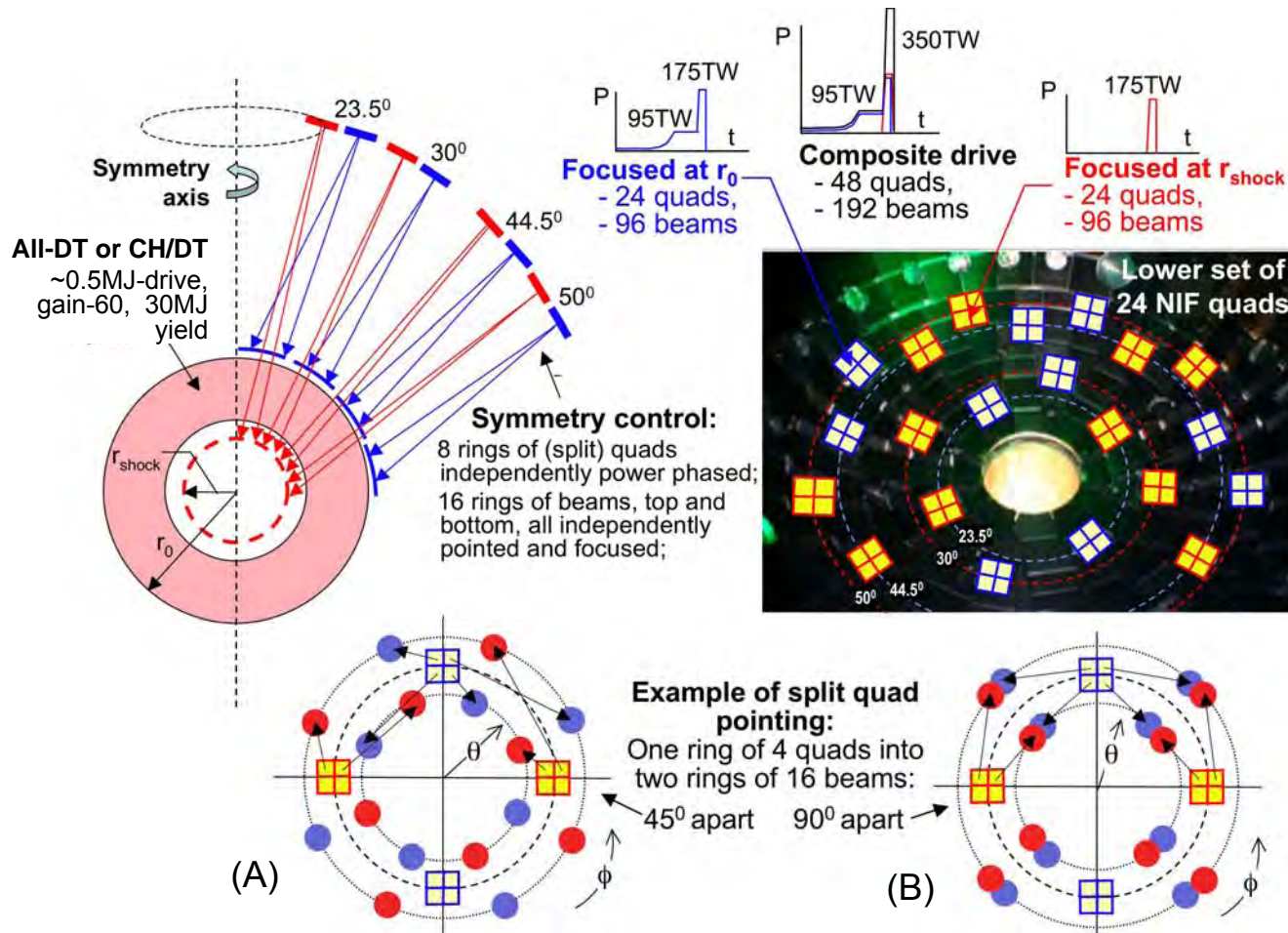
Axe du Quadruplet, Projection de la Tache Focale en Mouvement



# A paramount issue: Optimization of NIF polar drive symmetry and shock coupling efficiency at high convergence ratio



- 96-beams (**main+shock**) at  $r_0$  at  $t = 0$ ; 96-beams (**shock**) zoomed at  $r_{\text{shock}}$  at  $t = t_{\text{shock}}$
- Optimize pointing, focal spots and power phasing on each of 2x4/8 sets of quad/beam rings



**Necessary for beam uniformity?**

↓

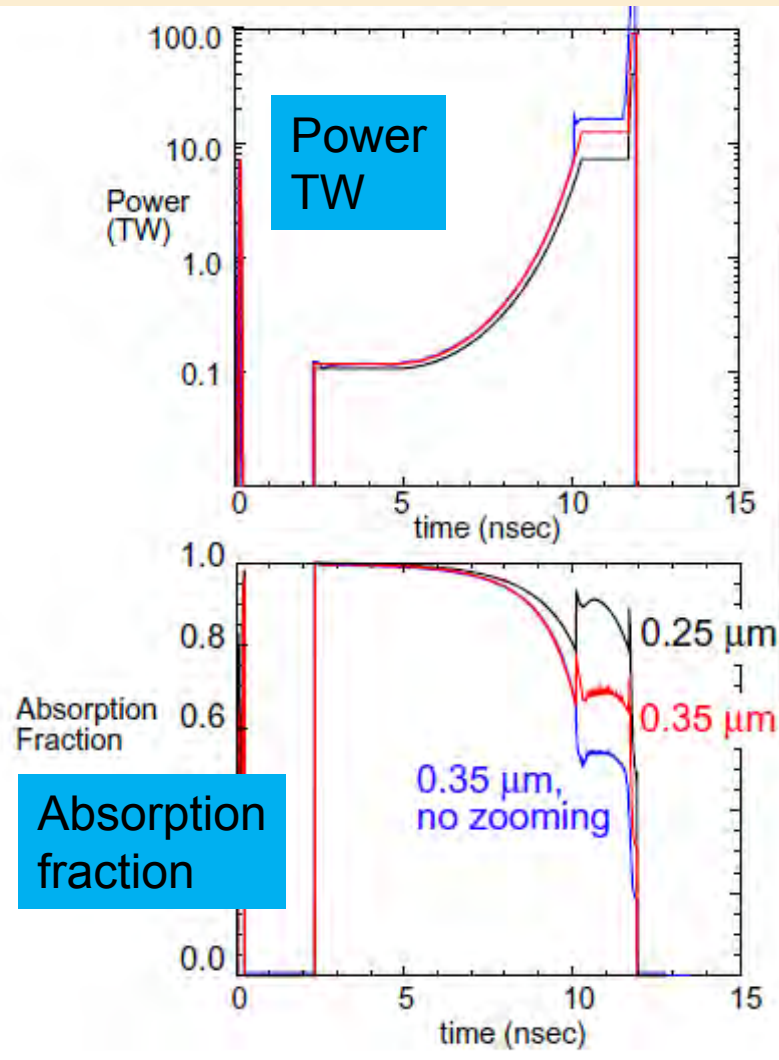
**Example of split quad pointing for optimum beam uniformity**

4 rings of quads split into 2x4 rings of beams

(C)

# Shock ignition benefits from shorter $\lambda$ and zooming

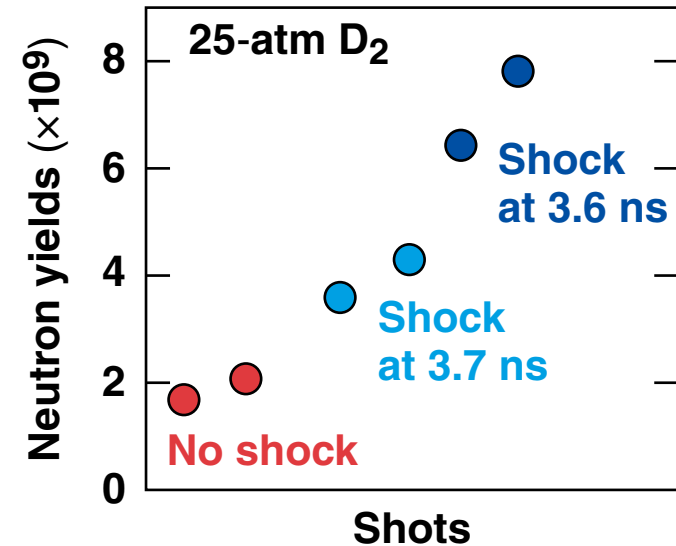
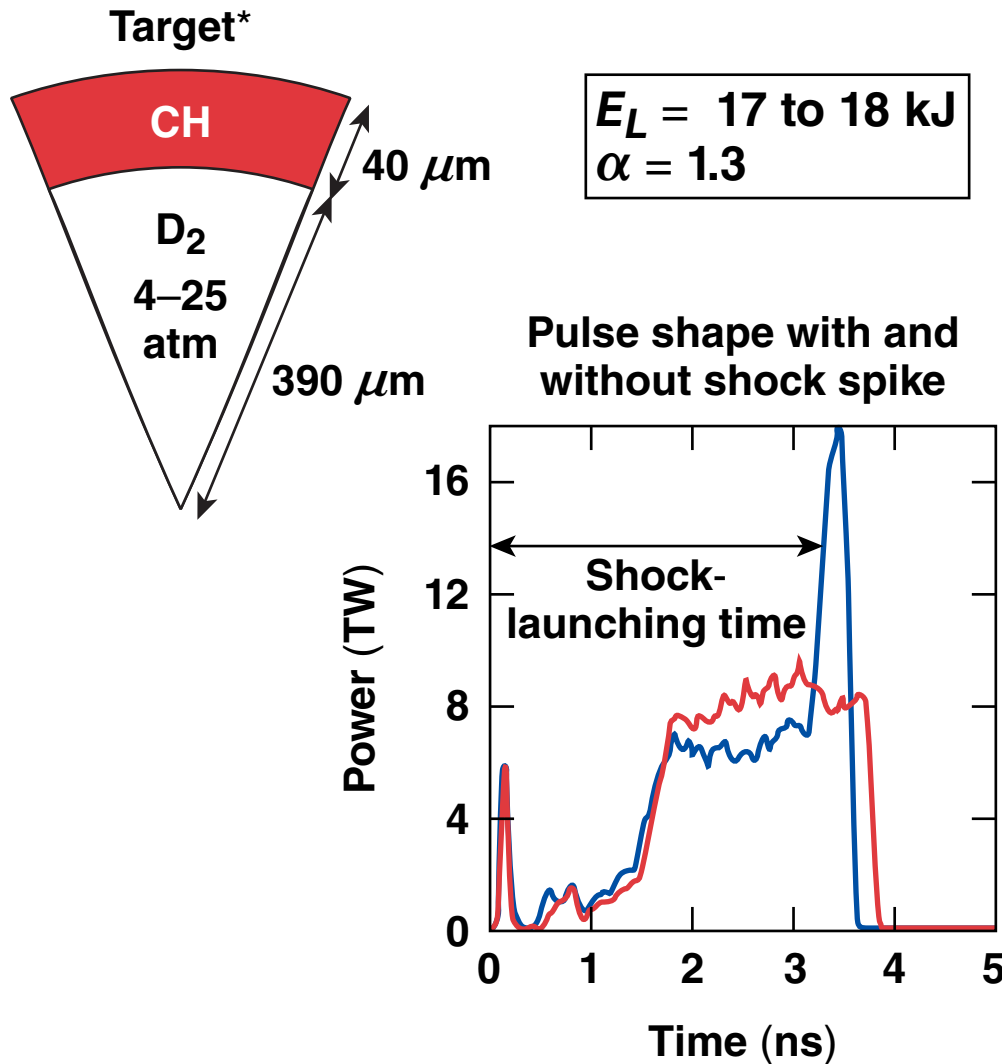
1-D Hydrocode simulations  
Fixed low aspect ratio pellet



	<b>KrF</b> $\lambda=248$ nm with Zoom	<b>Nd:glass</b> $\lambda=351$ nm with Zoom	<b>Nd:glass</b> $\lambda=351$ nm no Zoom
<b>Laser Energy</b>	<b>230 kJ</b>	<b>430 kJ</b>	<b>645 kJ</b>
Yield	22 MJ	24 MJ	23 MJ
<b>Gain</b>	<b>97</b>	<b>56</b>	<b>35</b>
Peak compression intensity (W/cm <sup>2</sup> )	$1.55 \times 10^{15}$	$2.2 \times 10^{15}$	
Peak igniter intensity (W/cm <sup>2</sup> )	$1.6 \times 10^{16}$	$3.1 \times 10^{16}$	

- Significantly higher gain with 248 nm & zoom
- Lower risk from laser plasma instability

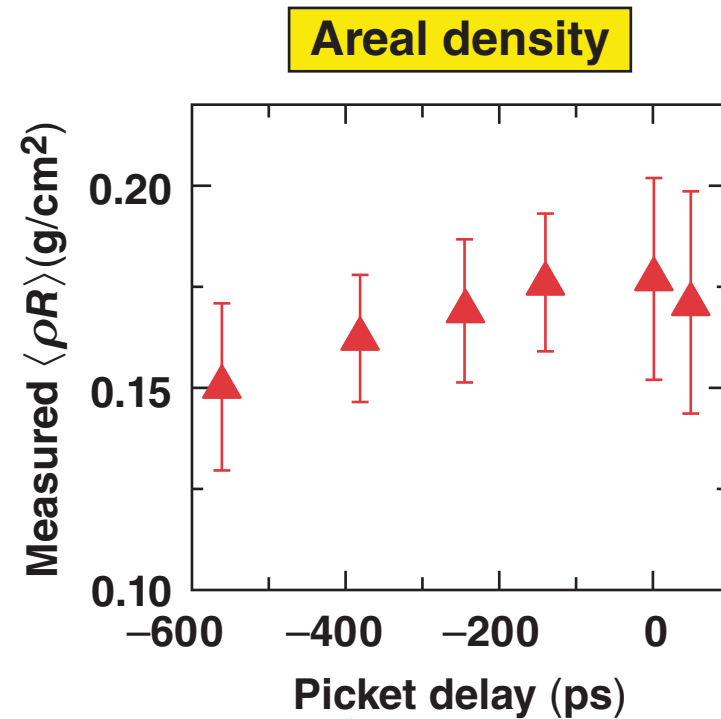
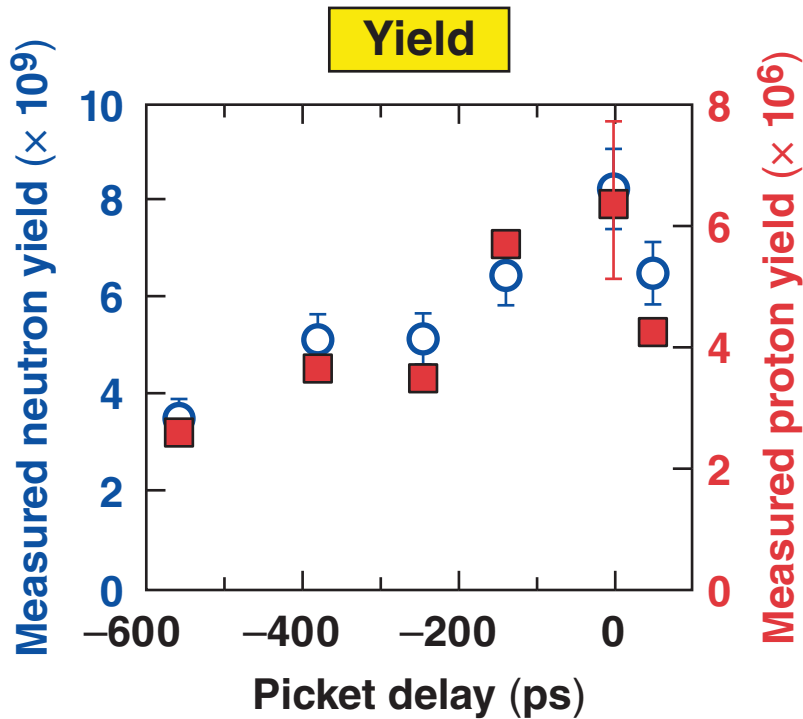
# CH shells have been imploded on OMEGA to test the performance of shock-ignition pulse shapes



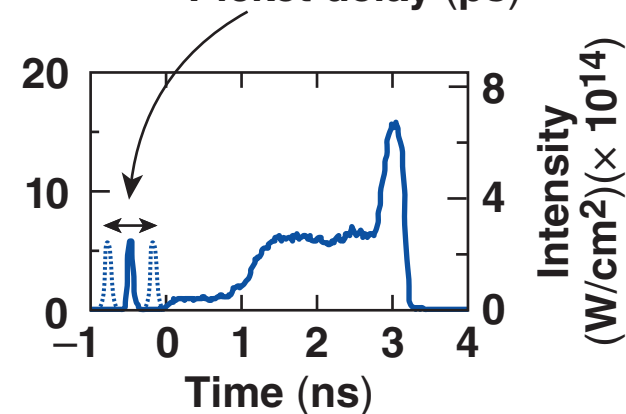
**The neutron yield increases considerably when a shock is launched at the end of the pulse.**



# The implosion was optimized with respect to the timing of the picket pulse with fixed spike timing

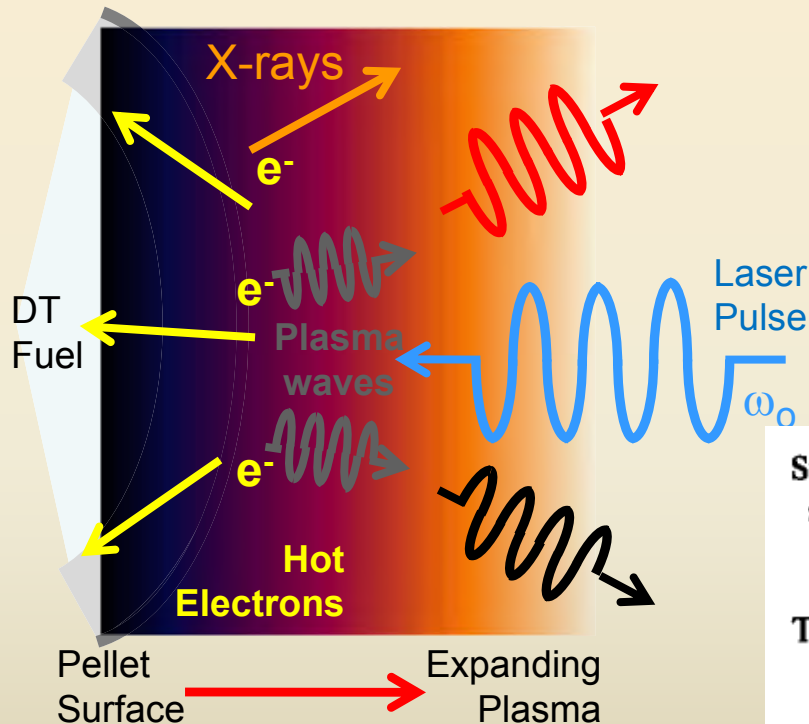


25-atm D<sub>2</sub>,  $E_L \sim 17$  kJ,  
spike at 2.8 ns



# Laser Plasma Instability limits the maximum intensity

- Can produce high energy electrons that preheat DT fuel
- Can scatter laser beam, reducing drive efficiency



**Shorter  $\lambda$  suppresses LPI**

$$(V_{\text{osc}}/v_{\text{the}})^2 \sim I\lambda^2$$

$N_c/4$  instability thresholds  
(single planar beam)

Stimulated Raman  
scatter ( $n \approx 1/4 n_{\text{cr}}$ )

$$I_t \approx \frac{5 \times 10^{16}}{L_n^{4/3}(\mu\text{m}) \lambda_0^{2/3}(\mu\text{m})} \frac{\text{W}}{\text{cm}^2}$$

Two plasmon decay

$$I_t \approx \frac{5 \times 10^{15}}{L_n(\mu\text{m}) \lambda_0(\mu\text{m})} \theta_{\text{keV}} \frac{\text{W}}{\text{cm}^2}$$

# LPI during the compression pulse?

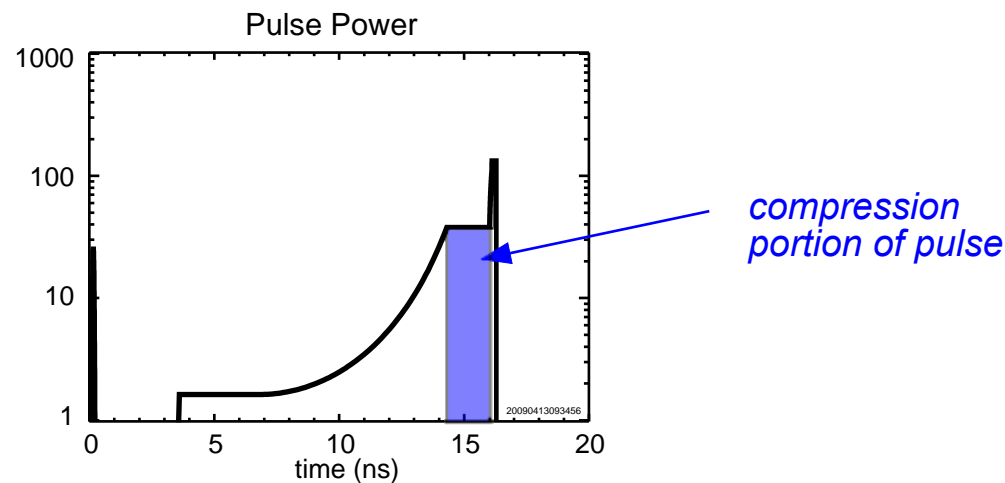
Fast electrons can preheat the fuel and prevent compression.

Instabilities at the quarter critical surface often have the lowest intensity threshold. E.g., the two plasmon ( $2\omega_{pe}$ ) decay threshold is\*:

$$I_{15} \sim 80 \frac{T_{\text{kev}}}{\lambda_{\mu\text{m}} L_{\text{d},\mu\text{m}}}$$

This simple formula has (so far) been **unreasonably effective** in predicting the intensity threshold of the occurrence of instability at  $n_c/4$  in a variety of experiments.

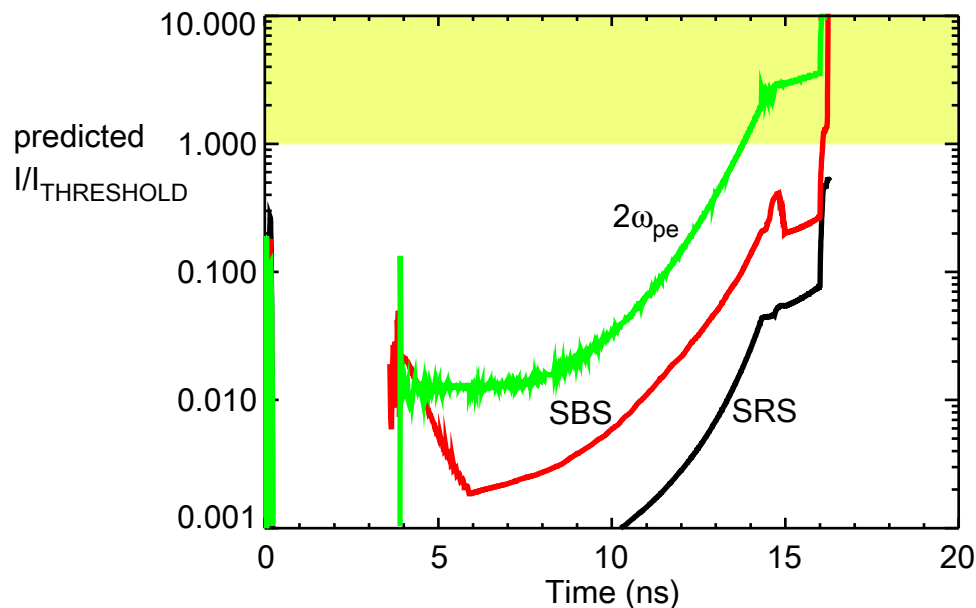
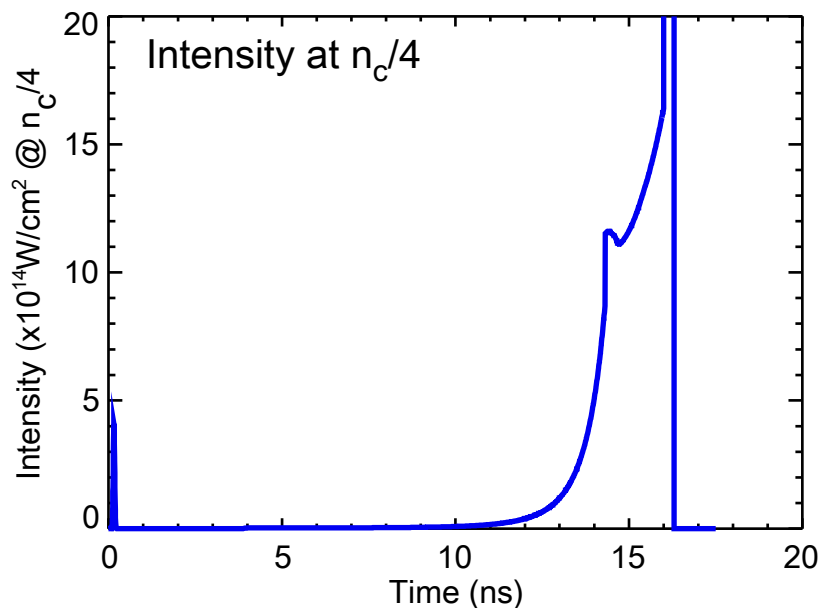
The impact of LPI will depend upon the number and energy of hot electrons generated, which is still quite unknown.



A. Simon, R. Short, E.A. Williams, and T. DeWandre, *Phys. Fluids* **26**, 3107 (1983);  
B. Afeyan and E.A. Williams, *Phys. Plasmas* **4**, 3788, 3803, 3827, & 3845 (1997).

# The baseline shock ignition target is above the predicted $2\omega_{pe}$ threshold during compression

baseline ~ 500 kJ shock ignition target

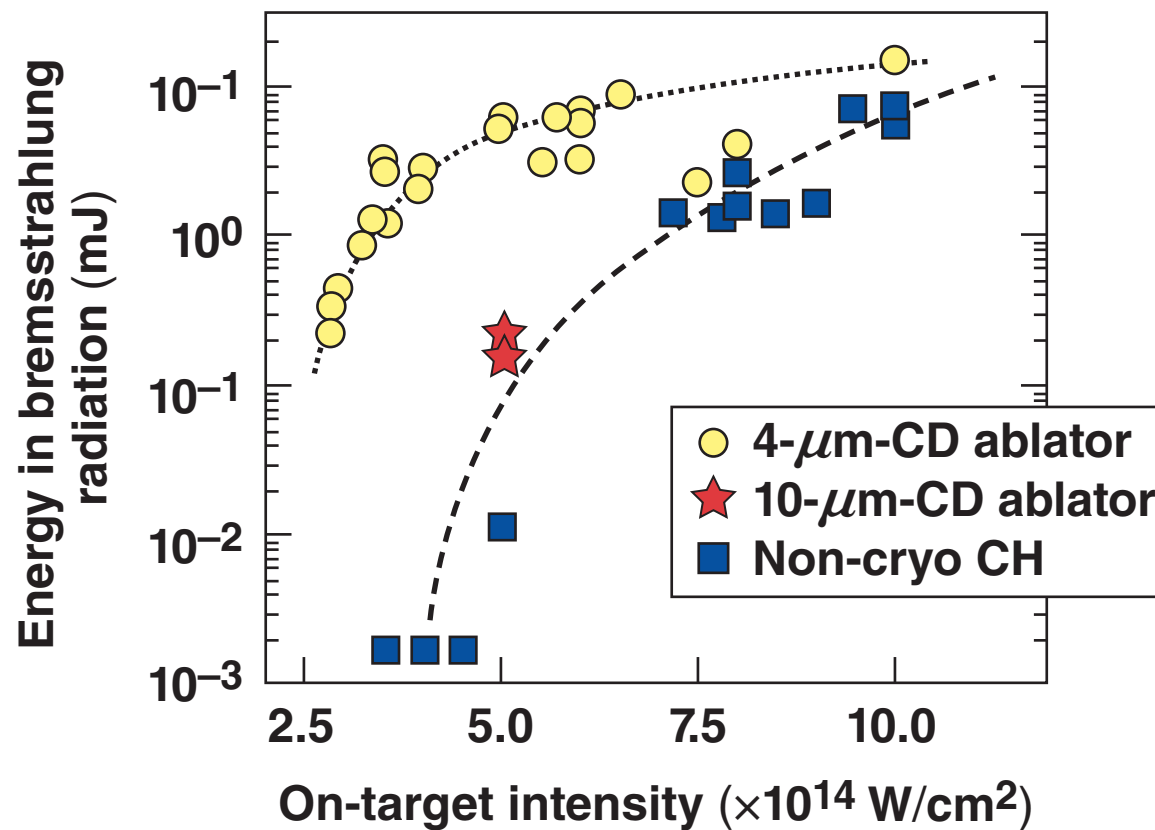


predicted  $I/I_{2\omega_{pe}\text{-threshold}}$

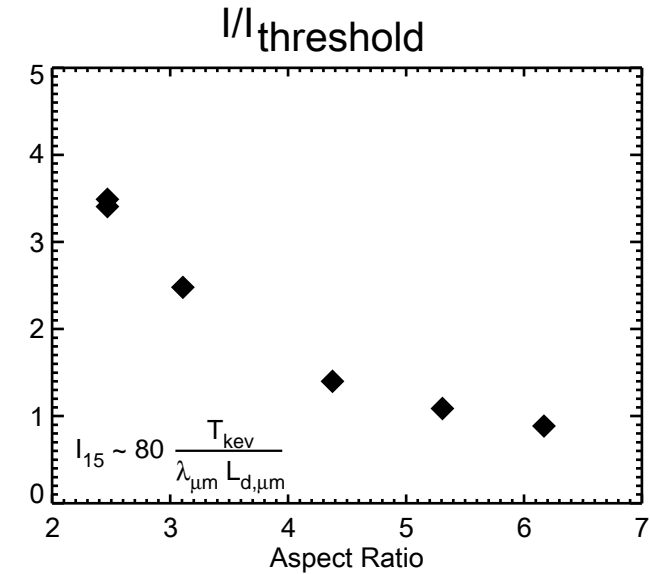
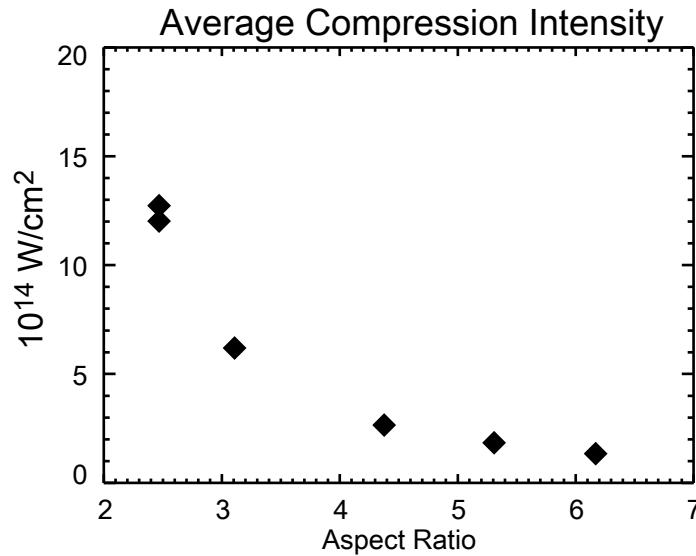
$$I_{15} \sim 80 \frac{T_{\text{keV}}}{\lambda_{\mu\text{m}} L_{d,\mu\text{m}}}$$

based on plane EM wave linear plasma ramp analysis

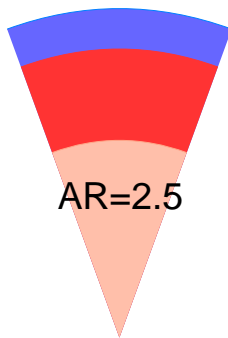
# OMEGA experiments show high hot-electron signals for hydrogenic ablators



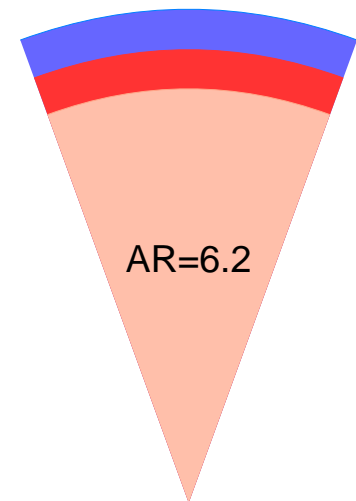
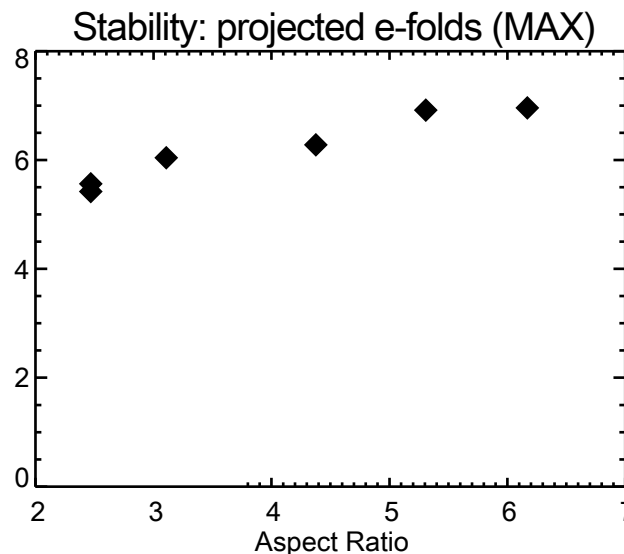
# Increasing the initial Aspect Ratio (AR) allows one to use lower drive intensities and decrease LPI risk



$$AR = \frac{R_{\text{outer}} - R_{\text{inner}}}{R_{\text{outer}}}$$

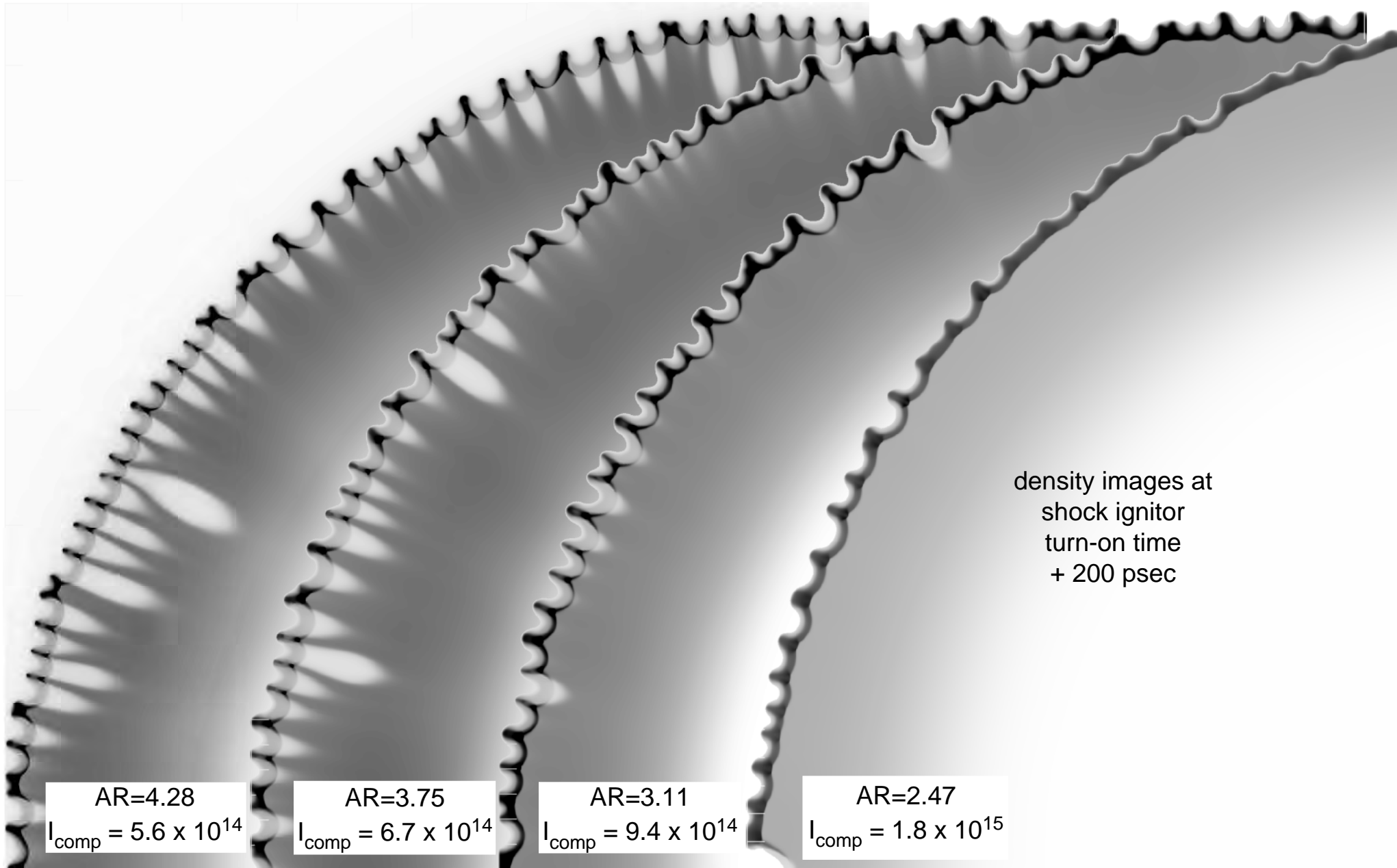


... but stability is worse



# Effects of lower intensity: 2D simulations of higher aspect ratio (AR) targets show greater growth of RT

NRL



density images at  
shock ignitor  
turn-on time  
+ 200 psec

( $I_{\text{comp}}$  = maximum intensity during compression pulse)

# A New Approach to LPI Control



- Instead of just phase control (in space-time) through masks and electro-optic modulators, or the all purpose PS solution, it is worth exploring the intentional variation of the amplitude and duration of short bursts of laser light ==> **STUD pulses**: Spike Train of Uneven Duration or Delay.
- Use **variable width spikes** to last 4-8 growth times of the most unstable mode to be avoided, and then shut off the pump long enough to disallow self-organization of plasma into coherent large amplitude waves which can then do real damage, and then repeat.
- Divide and conquer the laser's propensity to whip the entire plasma up into a coherent pump driven LPI haven. **Start and stop the interaction processes to avoid cumulative damage**. Three main reasons you win with STUD pulses: Don't allow growth in entire hot spot, avoid hitting the same driven wave by the same or similar hot spot over and over again, damp the wave between recurrence of hot spots to the same location as previously driven waves.



# Summary

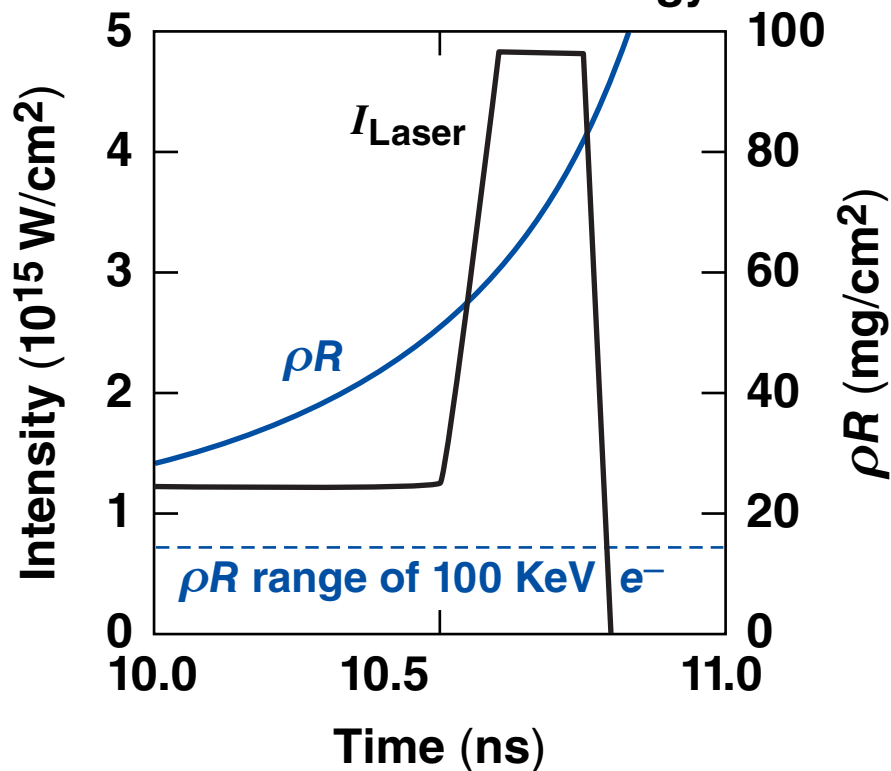


- We have a good understanding of the linear stage of TPD
- Most hot  $e^-$  are produced only in the nonlinear stage of TPD
- Forward hot  $e^-$  ( $>50$ -keV) flux from plane-wave, 2-D PIC is  $>10\times$  that of experiment measurements
  - how to account for 3-D effects like speckles?
  - LPI and hydro are difficult to decouple

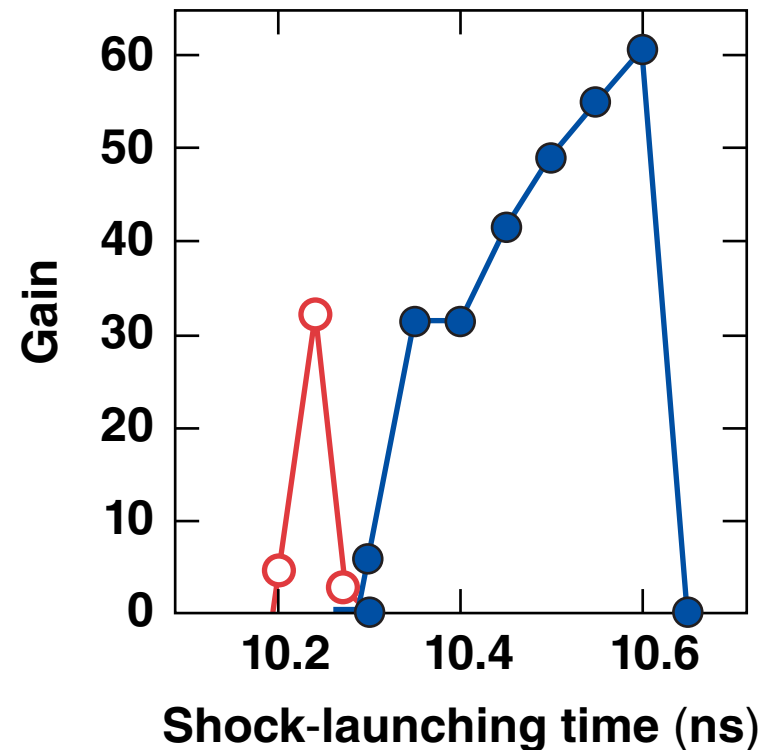
# Hot electrons of moderate energies produced during the shock spike can be beneficial to shock ignition



Shock-ignition target with 350-kJ total energy



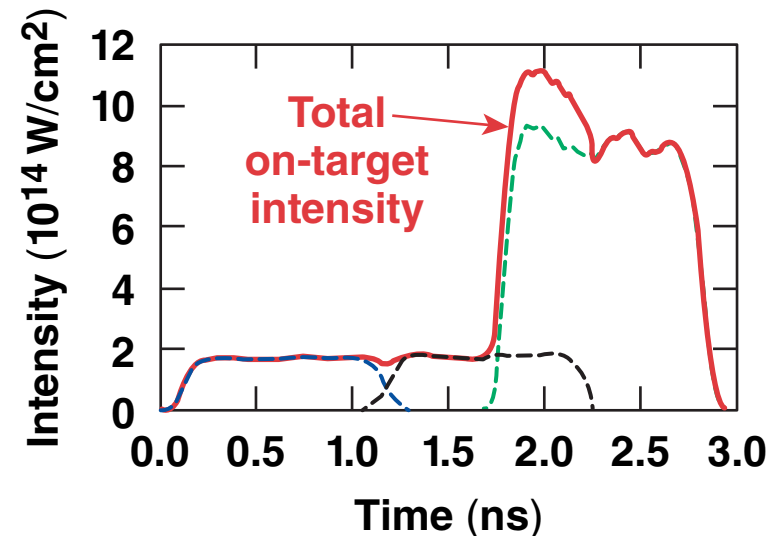
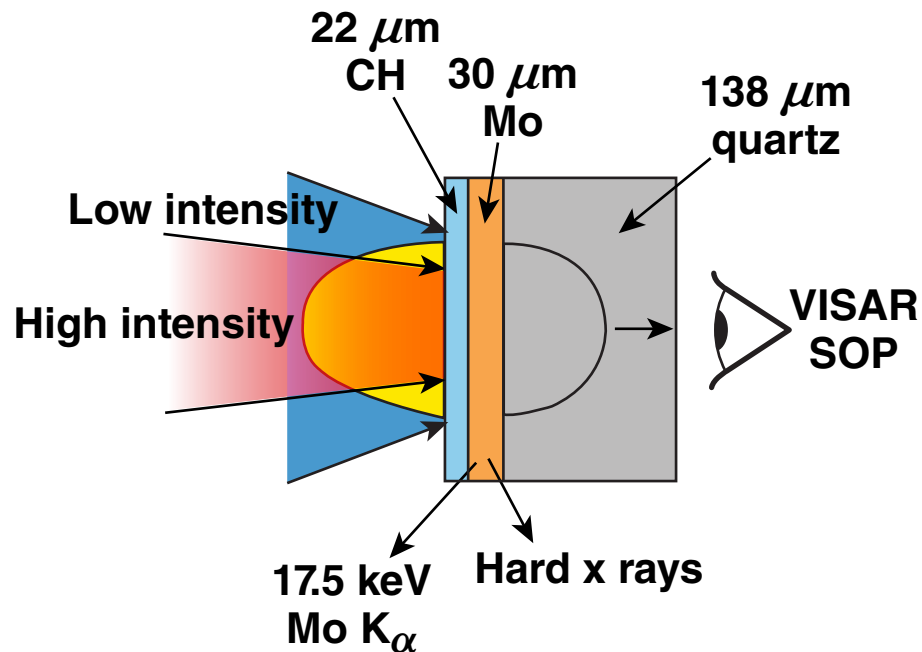
— Without hot  $e^-$  — With hot  $e^-$



Hot  $e^-$  with Maxwellian  $T_{\text{hot}} = 150 \text{ keV}$ ,  $E_{\text{hot}} = 17\%$  of spike energy, treated using a multigroup diffusion model\*

\*J. Detetrez and E. B. Goldman, LLE, Univ. of Rochester, Rochester, NY, LLE Report No. 36 (1976). Also see K. S. Anderson (this conference).

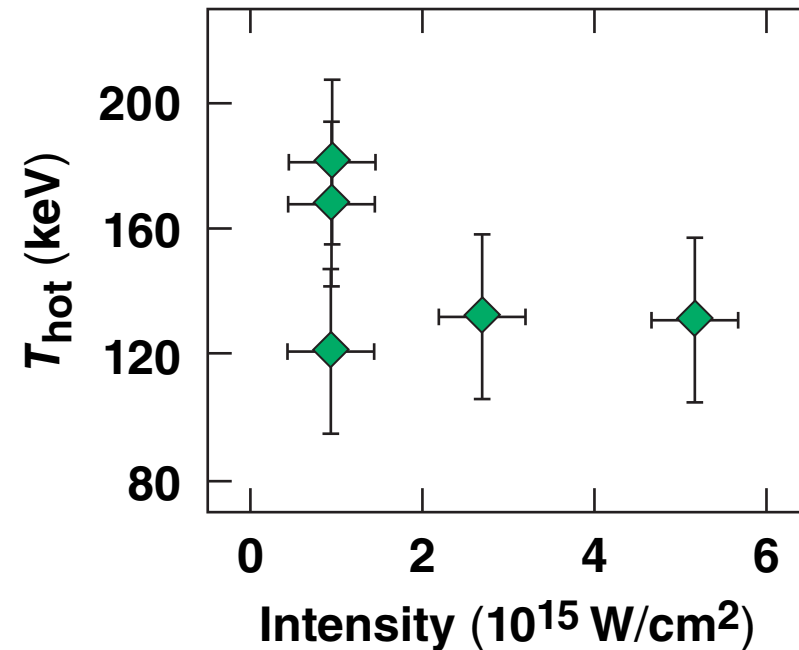
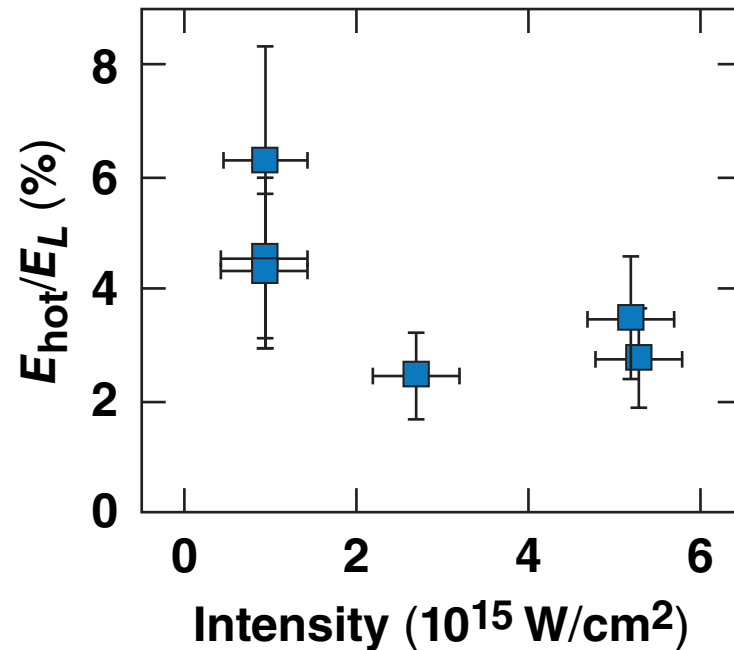
# A laser-plasma interaction experiment was performed in planar geometry with overlapping beams



Pre-plasma pulse:  $\sim 2 \times 10^{14}$  W/cm $^2$   
900- $\mu\text{m}$  spot diameter

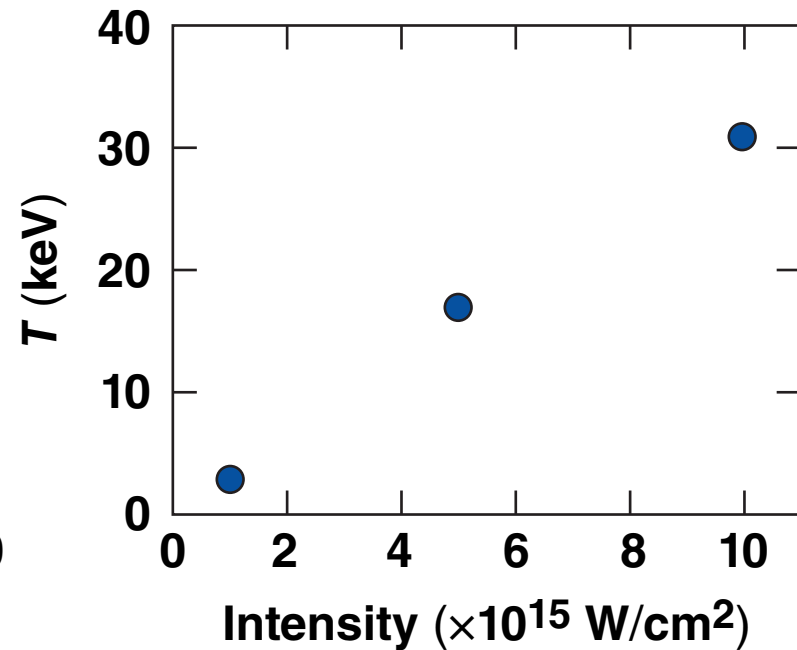
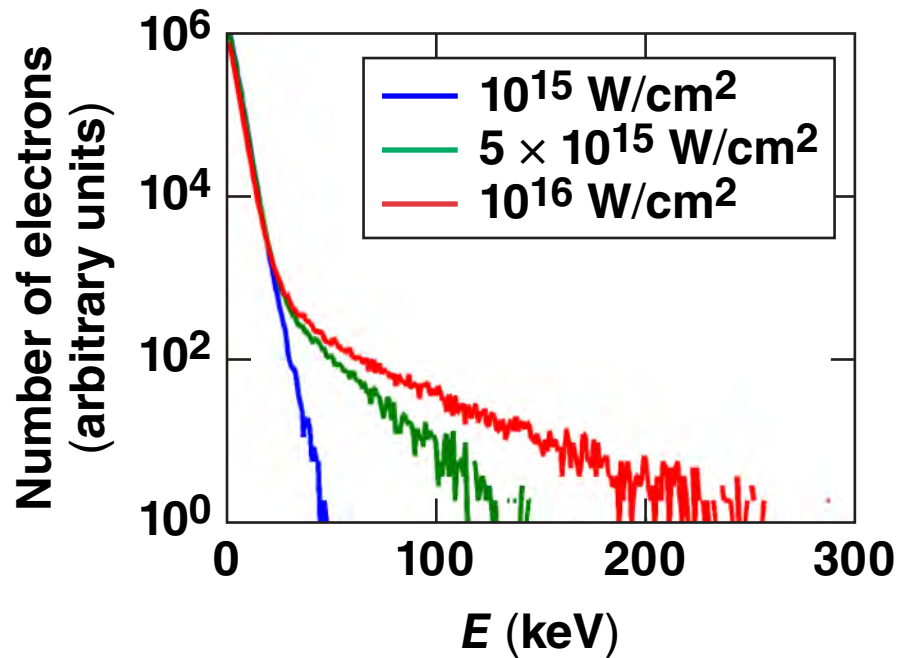
Shock pulse:  $\sim 1$  to  $5 \times 10^{15}$  W/cm $^2$   
250- to 600- $\mu\text{m}$  spot diameter

# Up to 6% of the high-intensity laser energy is converted into hot electrons

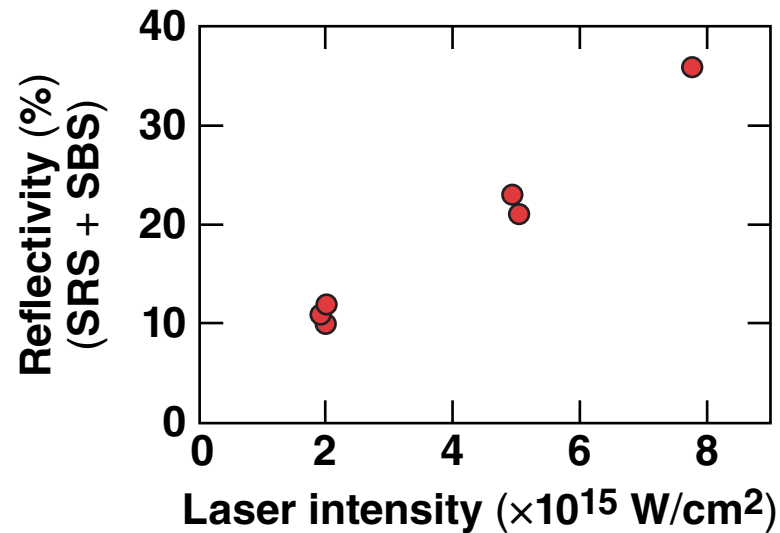


- The measured hot-electron temperature is 3× higher than in spherical geometry
- >150-keV electrons can be detrimental to target performance

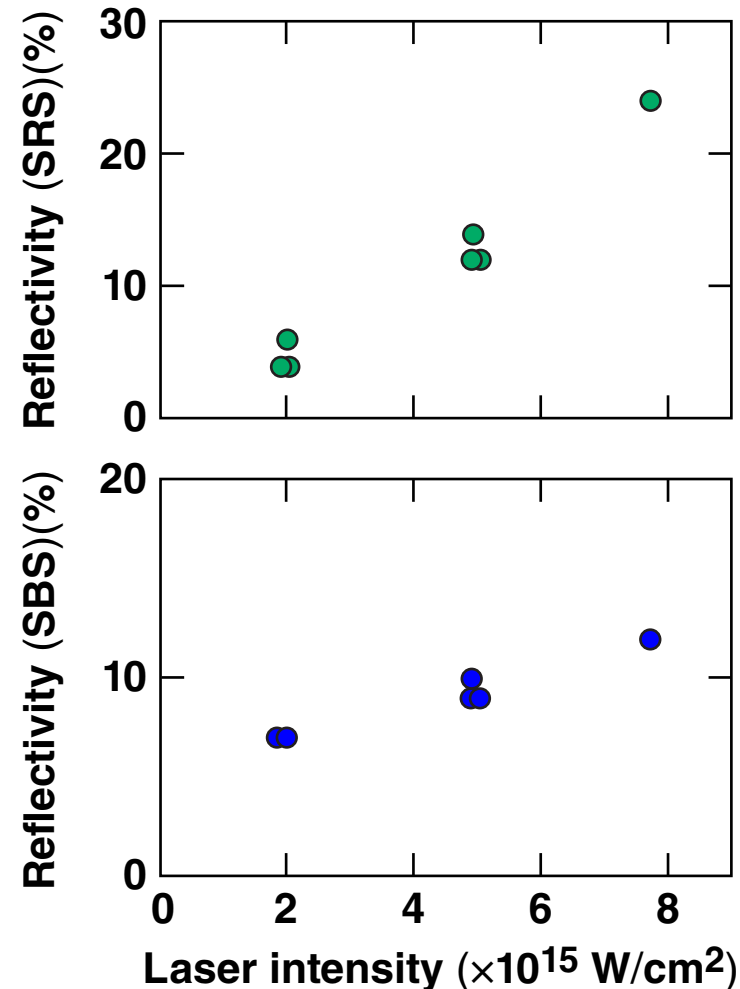
# 1-D PIC simulations at SI-spike relevant intensities show low-temperature hot electrons with an energetic tail



# Up to 35% of the shock-beam laser energy is lost due to backscatter; $T_{\text{hot}} \sim 45$ keV



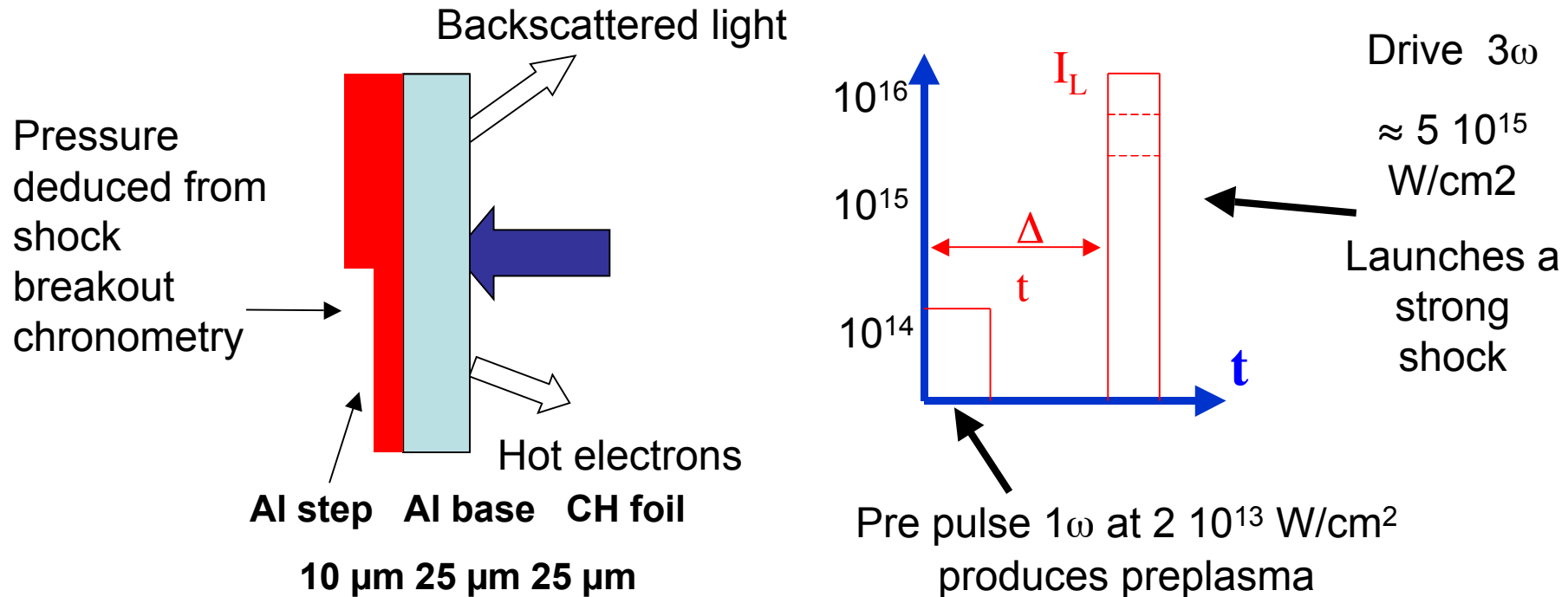
- No measurable signal of the 3/2 harmonic
- SRS dominates back reflection at highest intensity
- SBS reflection is relatively stable at  $\sim 10\%$



C. Stoeckl *et al.*, Bull. Am. Phys. Soc. **54**, 265 (2009).

W. Theobald *et al.*, Plasma Phys. Control. Fusion **51**, 124052 (2009).

# Sketch of expt. set-up



**Prepulse -  $E = 30$  J,  $\lambda = 1.3$  μm,  $\Phi = 1$  mm,  $\tau = 300$  ps  $\Rightarrow I = 1.2 \cdot 10^{13}$  W/cm<sup>2</sup>**

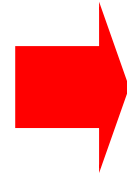
**Temperature**  $T_e (eV) = 10^{-6} \left( I (W/cm^2) \lambda^2 (\mu m) \right)^{2/3} \approx 750 eV$

**Main Pulse -  $E = 250$  J,  $\lambda = 438$  nm,  $\Phi = 100$  μm,  $\tau = 300$  ps  $\Rightarrow I = 10^{16}$  W/cm<sup>2</sup>**

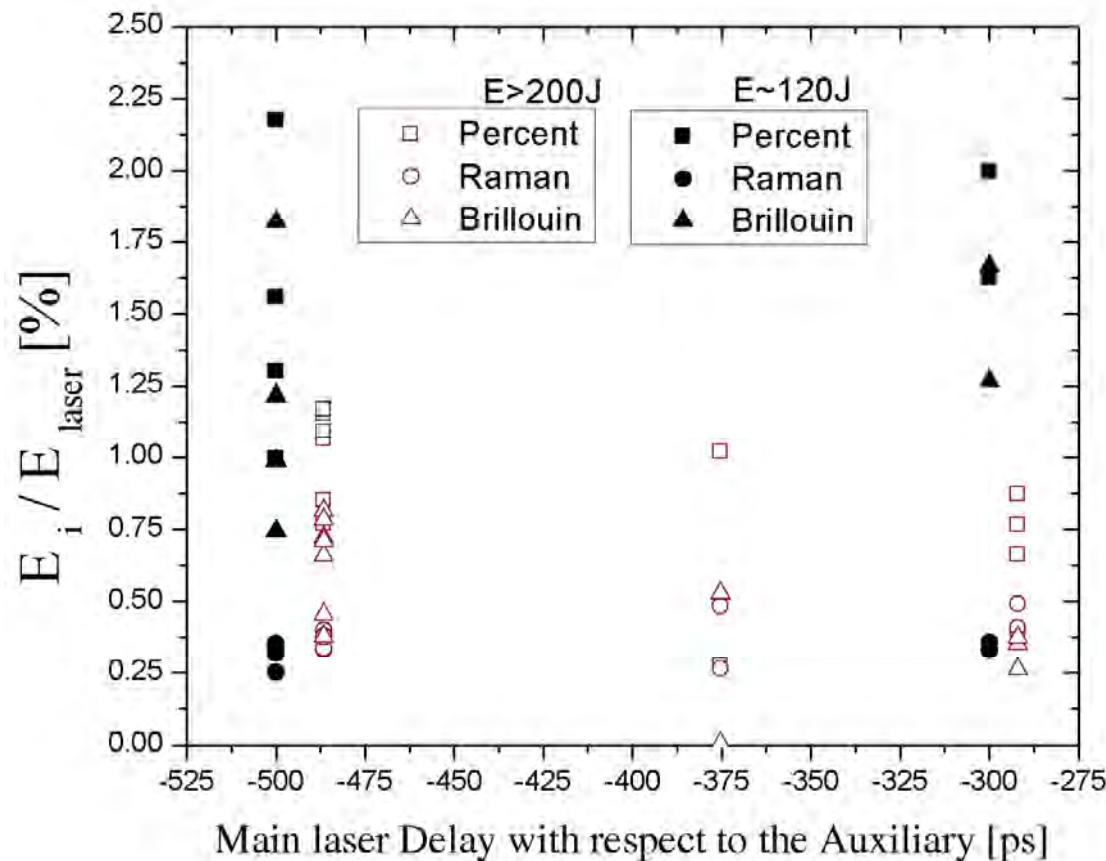
**Pressure**  $P (MBar) = 8.6 \left( \frac{I (W/cm^2)}{10^{14} \lambda (\mu m)} \right)^{2/3} \left( \frac{A}{2Z} \right)^{1/3} = 320 MBar$

# Back scattering: calorimetry

Results at the Omega facility (Usa, 2009) give 33% back reflection at  $I \approx 8 \cdot 10^{15} \text{ W/cm}^2$



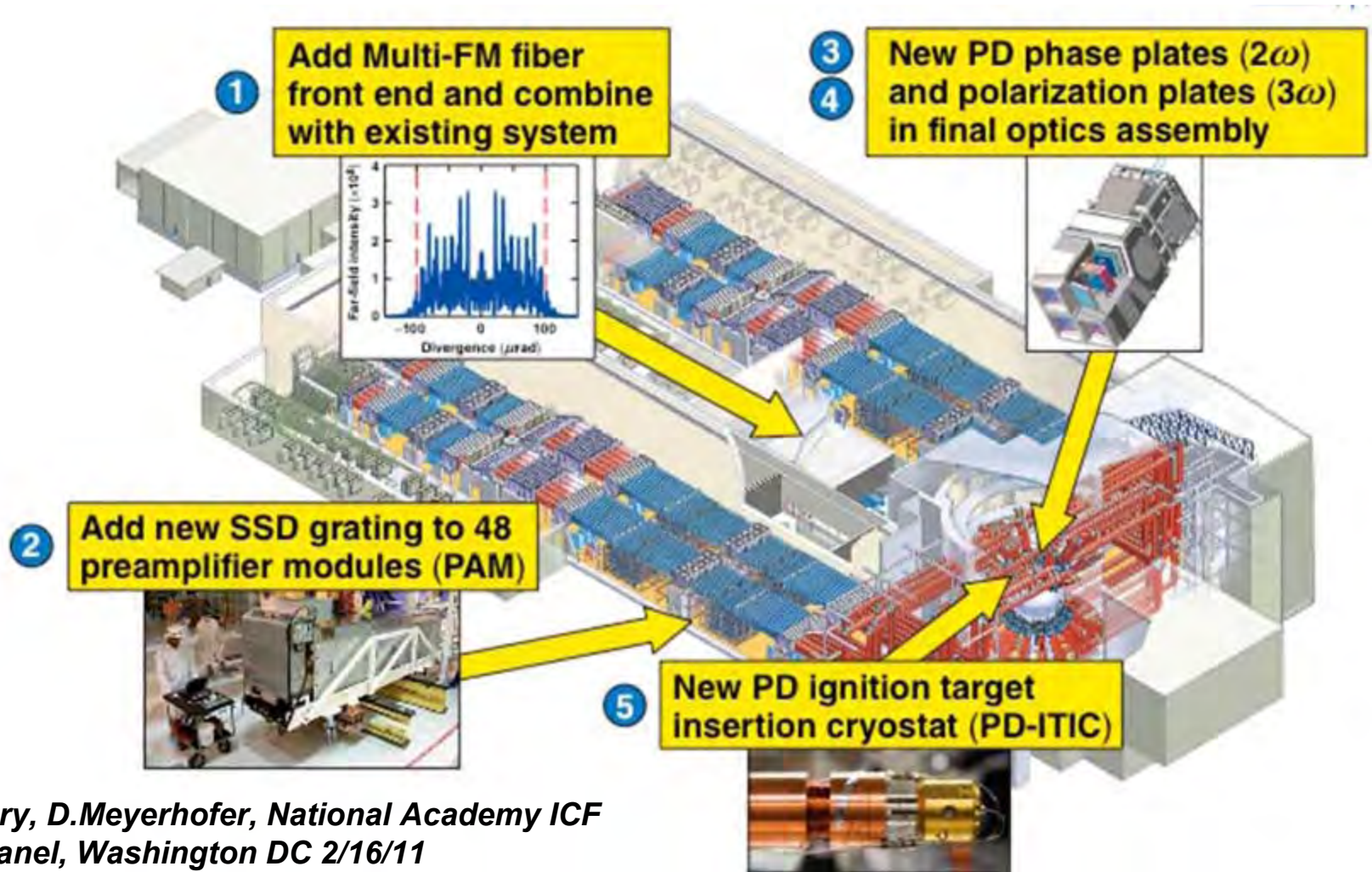
**A surprisingly small fraction of light is backscattered in our experimental conditions ( $I \approx 10^{16} \text{ W/cm}^2, \lambda = 0.44 \mu\text{m}$ )**



WORK IN PROGRESS...

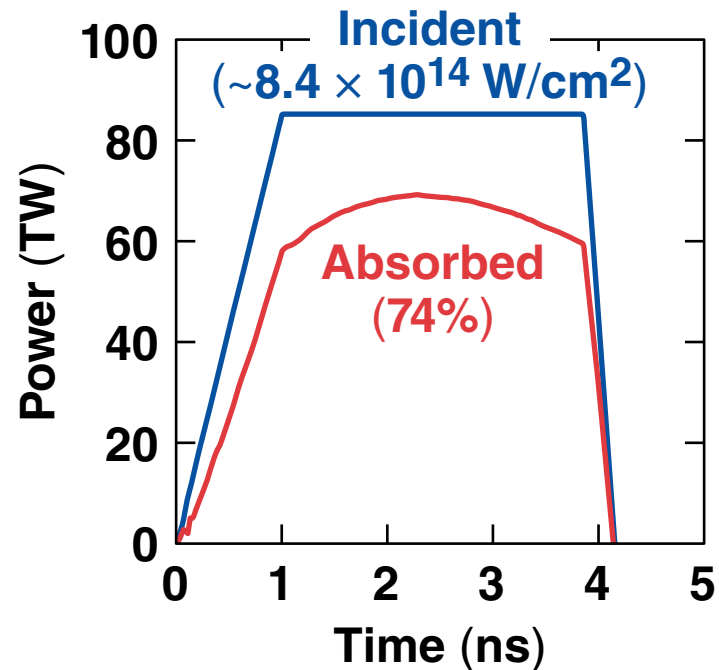
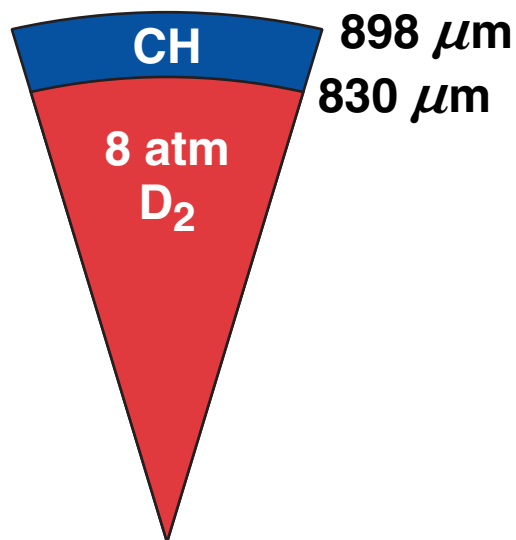


# Full implementation of NIF polar drive will require five hardware upgrades for a (cryo) ignition demonstration



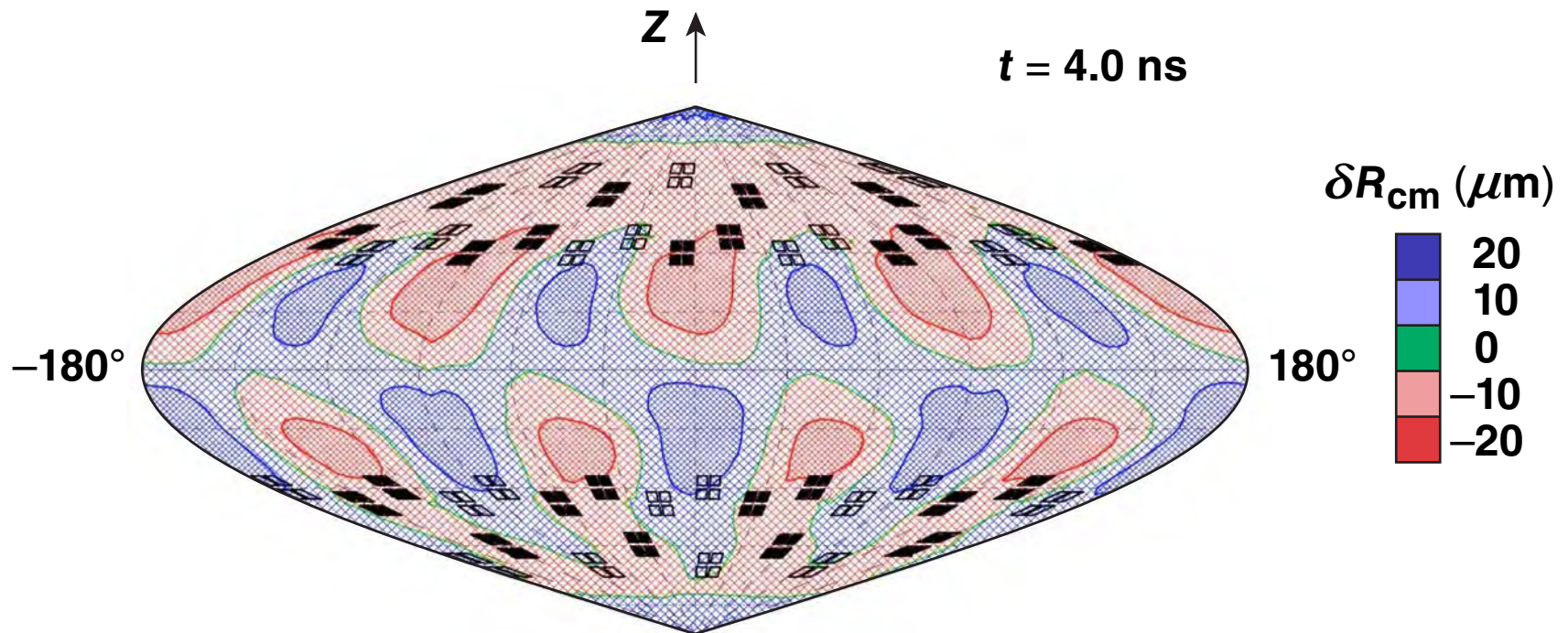
R.McCrory, D.Meyerhofer, National Academy ICF Target Panel, Washington DC 2/16/11

# A surrogate CH target is proposed to test the 24-quad compression phase



- Objectives of the initial experiment
  - diagnose the implosion uniformity
  - measure the speed of the imploding shell
  - diagnose any hot electrons from the two-plasmon instability

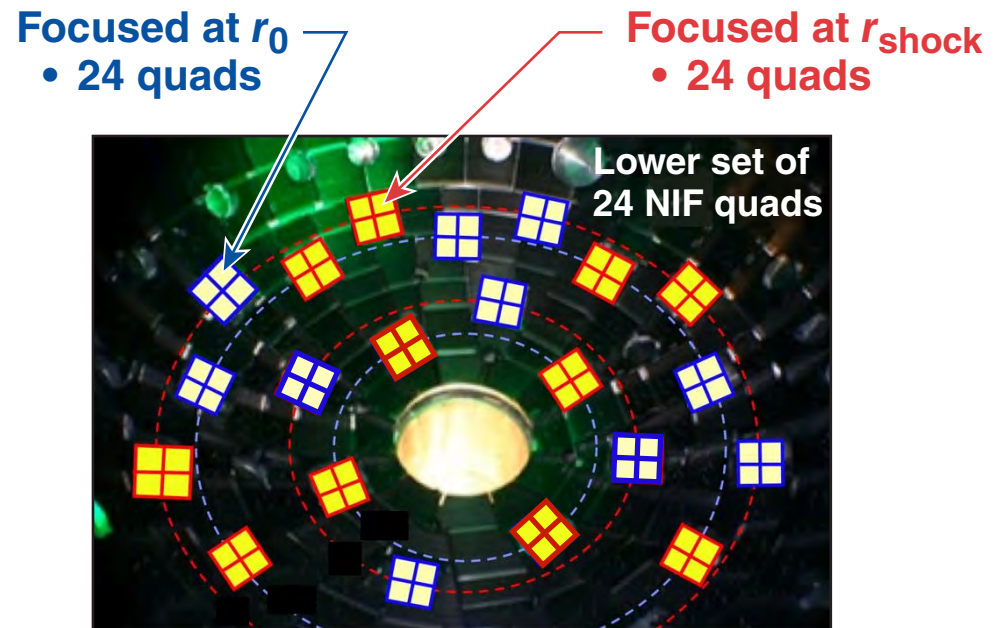
The center of mass radius is uniform to  $8.1 \mu\text{m}$  (rms) when averaged over the sphere



# Beam-pointing schemes are being explored for polar-drive shock ignition on the NIF



- Focusing separate shock beams at a smaller radius late in time allows for better coupling of energy to the target
- A scheme with split quads would allow for best irradiation uniformity on target, but requires time-consuming “rewiring” of NIF seed pulses
- Another scheme employing full quads—half for the main drive and half for the shock pulse—was recently proposed\* by Steve Craxton



# Primary Action Items focused on Target Design and understanding the effects of LPI on target performance

---



### Target Design

- Design a proof-of-principal, low-risk, low-gain SI experiment
- Determine if a planar I15, 300-MB shock experiment is possible
- Determine how we can get more energy into the spike pulse
- Design initial experiments for the NIF

### LPI and the *THING* ( $2\omega_p$ threshold)

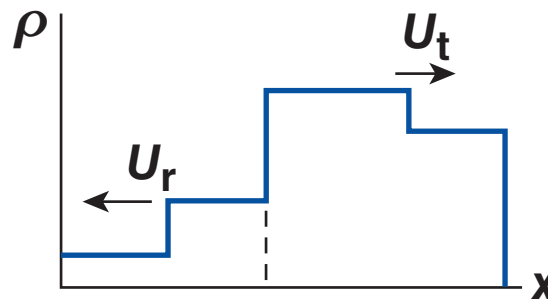
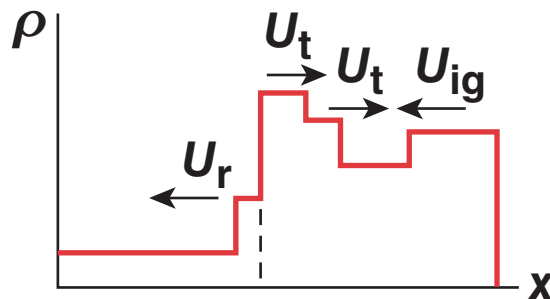
- Determine experimental platform to identify and mitigate preheat during the fuel-assembly phase
- Determine experimental platform to identify if single beam versus overlapped beams mitigate spike-pulse preheat
- Review STUD pulse experimental results from Trident

# Direct Drive w or w/o Shock Ignition Also Requires LPI Control

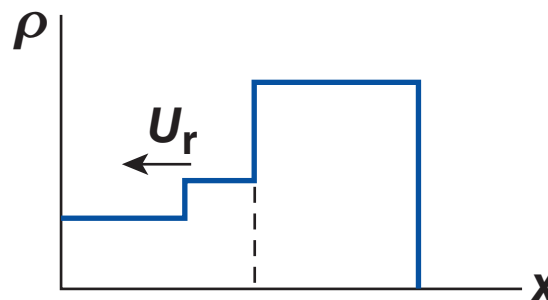
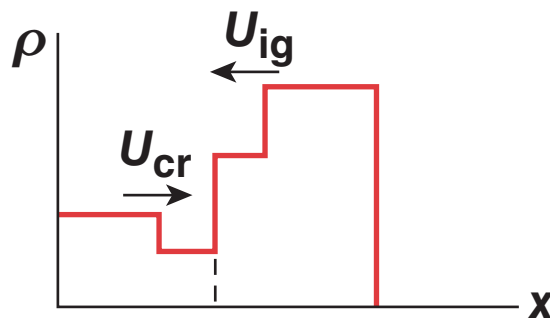


- If we do not keep the growth of parametric instabilities under strict control during the main pulse, then the hot electron preheat will make the final shock have dubious prospects.
- Worry about SRS and  $2\omega_p$  as the two most likely hot electron generating instabilities via their plasma waves daughter waves.
- Worry about the physics of multiple of massively overlapping beams, hot spots overlapping, triggering each other's instabilities, nonlocal influences in space, mediated by hot electrons, secondary instabilities, SRS/SBS anti-correlation, ...
- This is not your grandfather's LPI scenario.
- For shock ignition, need to convert the right distribution of hot e's into a sharp heat front that becomes that last shock, quickly assembled. Designing this is a wonderful challenge of our knowledge of LPI physics.
- What wavelength to use for the last shock, what pulse shape, what intensity regime, all remain open and exciting questions.

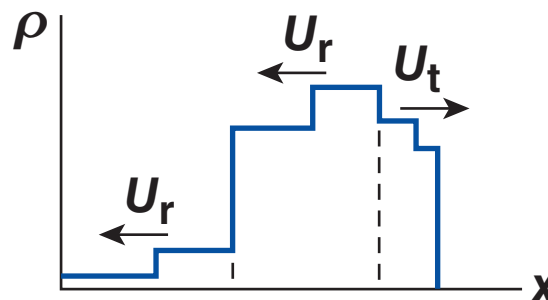
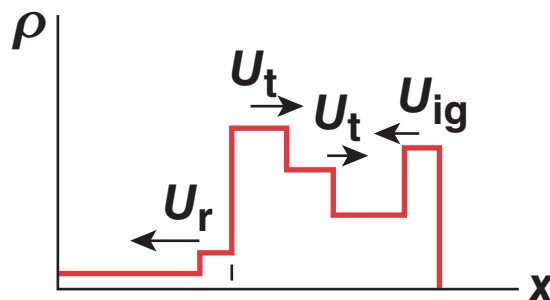
# Late shocks can suppress rarefaction waves— there are three ways shocks can be launched



**No-rarefaction technique**  
(requires many highly synchronized “weak” shocks)

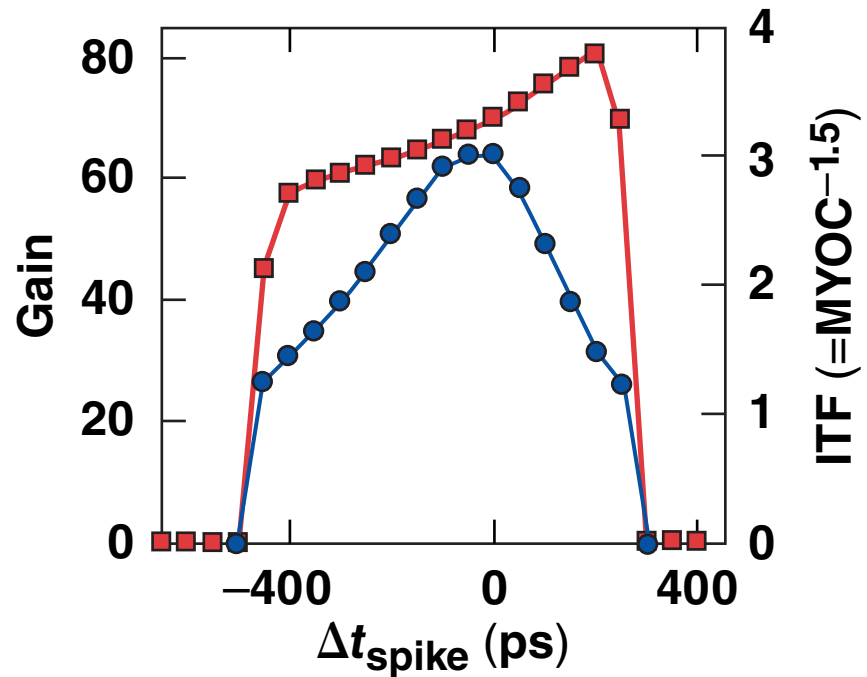
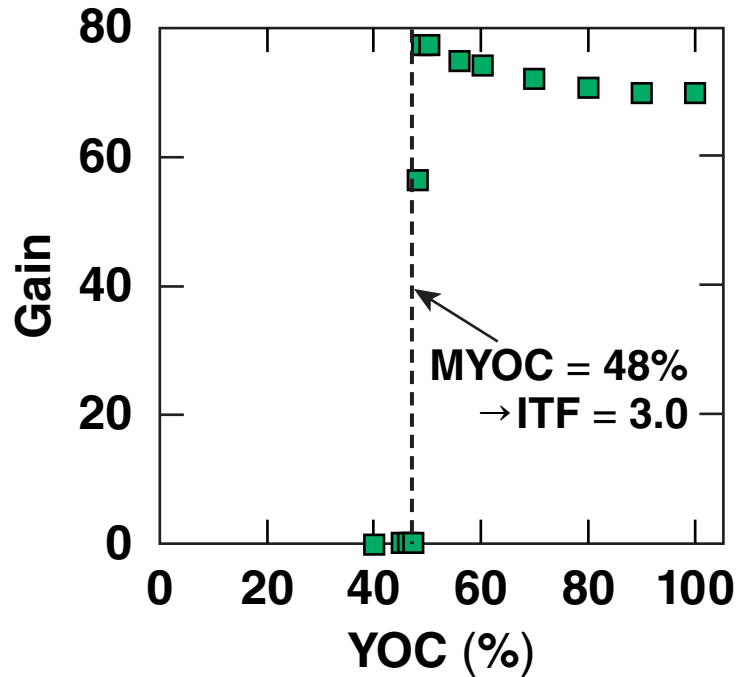


**No-transmission technique**  
(requires one moderate shock)



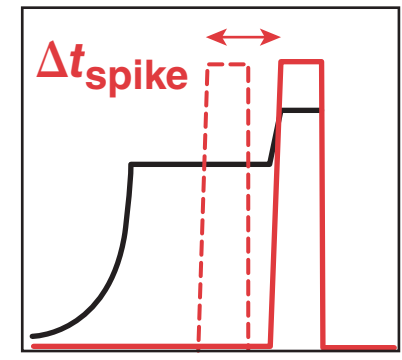
**Re-shock technique**  
(requires one strong shock)

# Plastic-ablator shock-ignition targets are robust to shock timing and reduced clean volumes



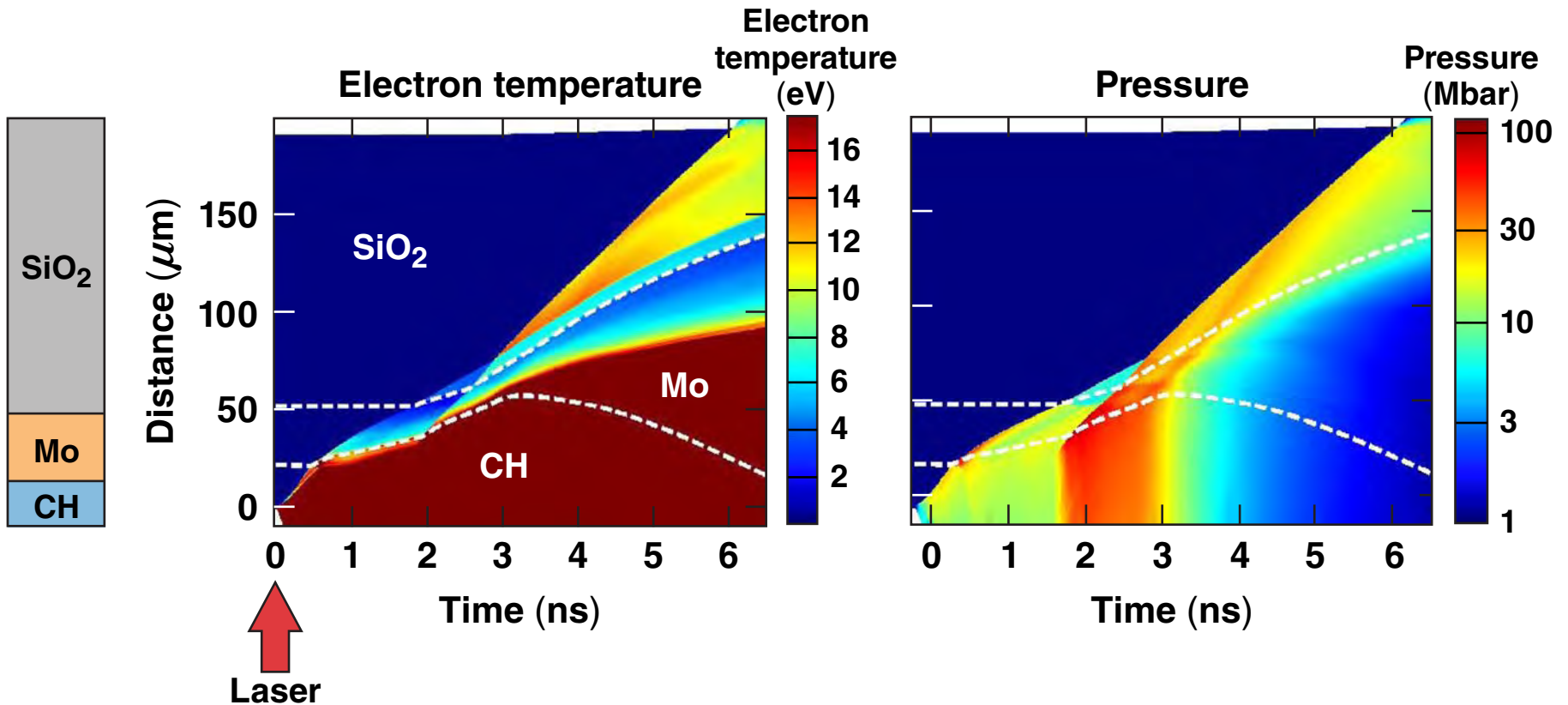
**ITF for indirect-drive point design\* is ~5.3 (MYOC = 33%) at 1 MJ.**

\*J. Lindl, presented to the JASON Review Committee Study #JSR-09-330, San Diego, CA, 14-16 January 2009.



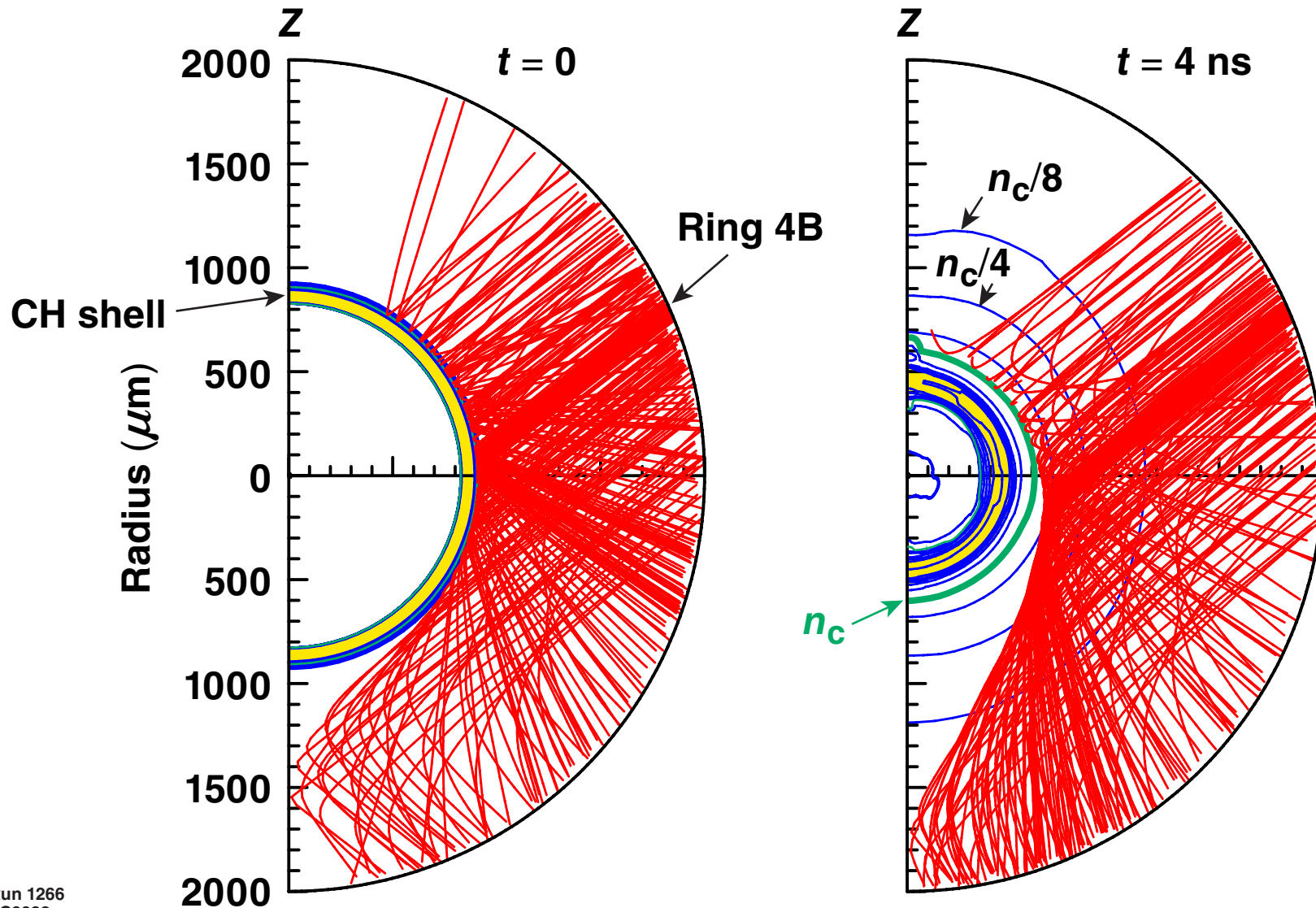


# 1-D hydrodynamic simulations predict an initial plasma pressure of $\sim 100$ Mbar for $\sim 1 \times 10^{15}$ W/cm<sup>2</sup>



- The spike absorption is varied to match the shock-breakout time
- 2-D *DRACO* simulations are currently being performed

# The CH shell implodes uniformly throughout the 4-ns laser pulse





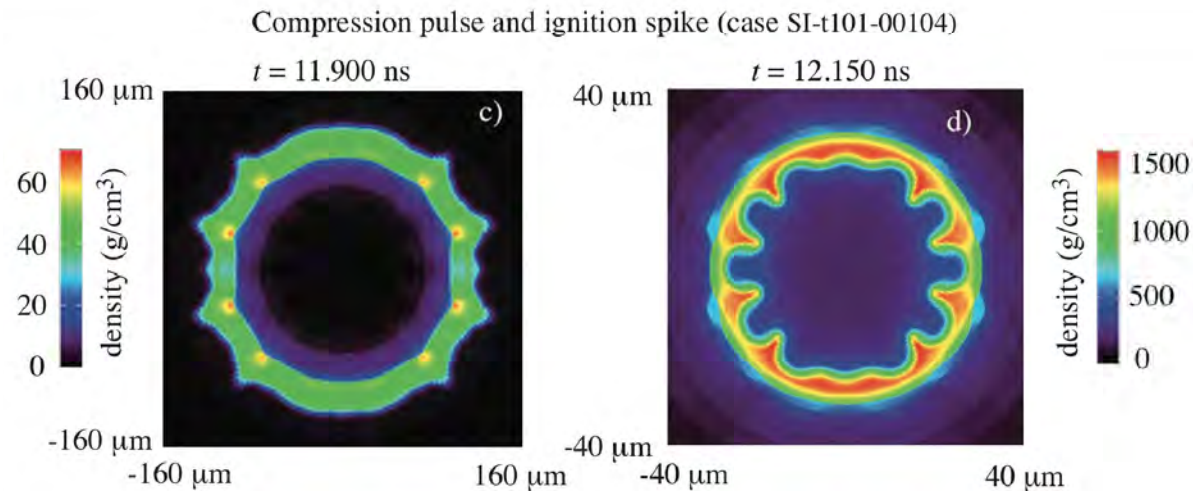
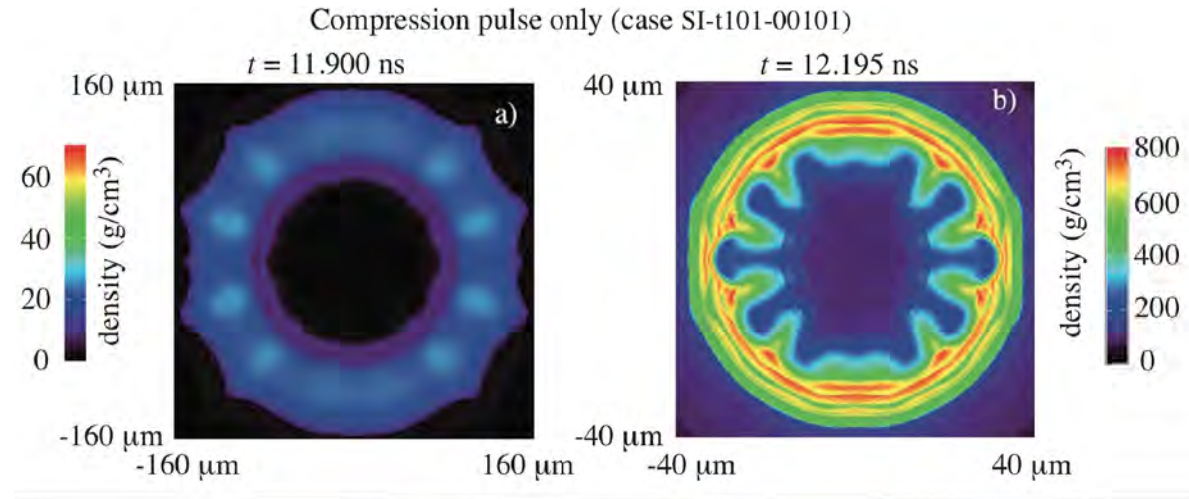
# Shock-ignition: reduced hot spot-RTI growth



No SI spike

with the  
CELIA  
radiation  
spectrum

Shock ignition



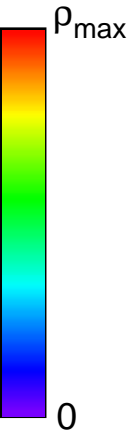
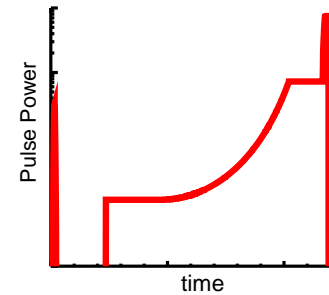
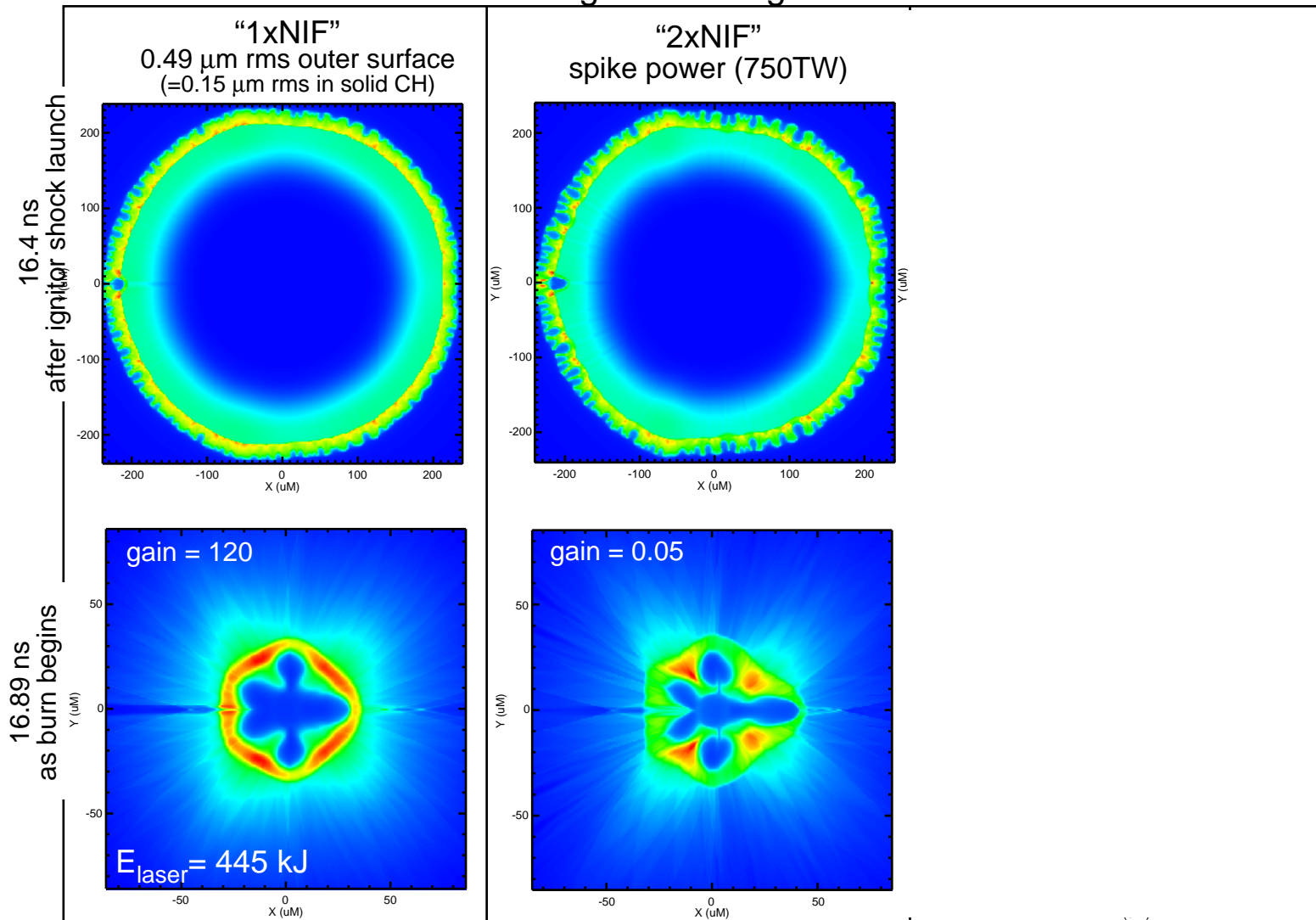
perturbation growth halts  
@ shock collision



# Doubling the outer surface perturbations causes gain failure

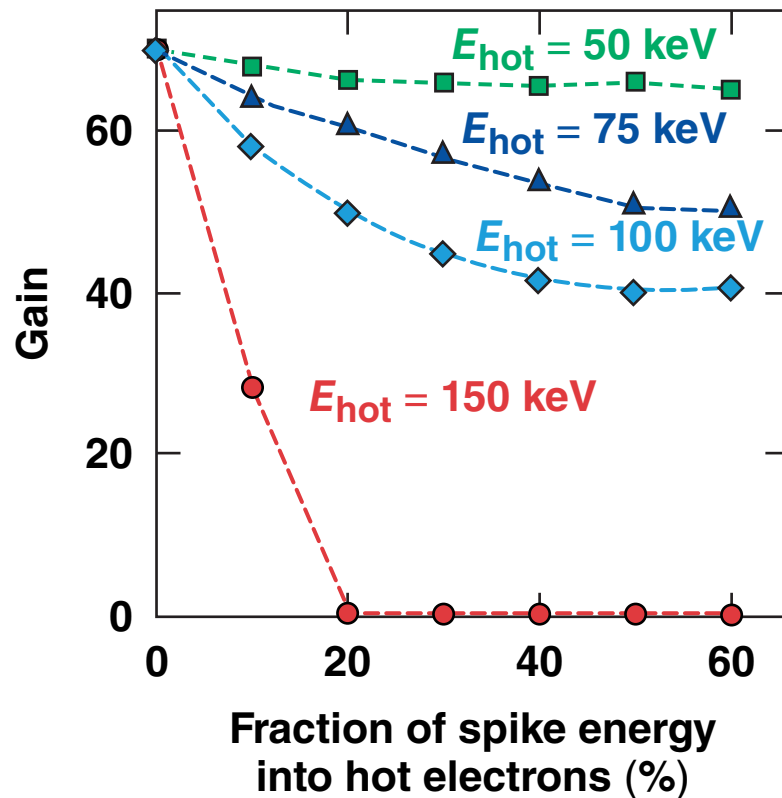


**broken:**  
doubling the surface roughness prevents ignition and gain



**scale 2 target**

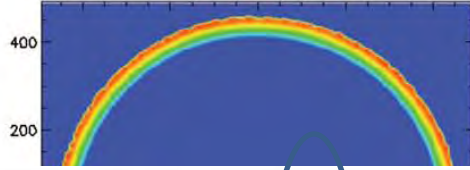
# The plastic-ablator SI design is robust to hot electrons up to 100 keV at 60% of laser energy during the spike pulse



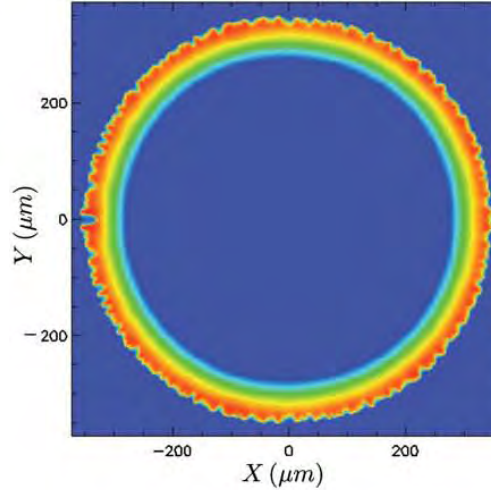
- Straight line hot-electron-transport model by A. A. Solodov
- Future work will investigate hot-electron transport during the main pulse

# Comprehensive 2D simulations of SI KrF targets, with zooming are carried out by the NRL group

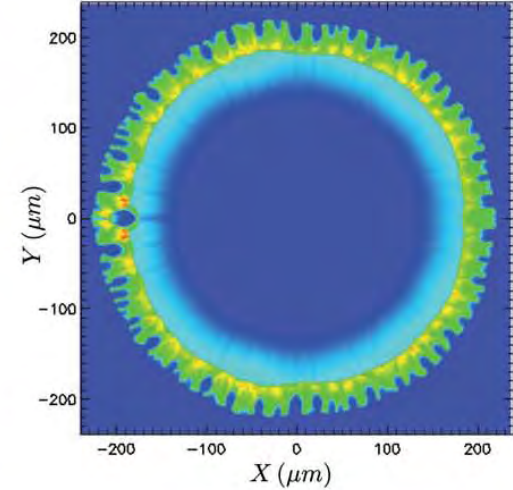
$t = 15.30$  ns



$t = 15.90$  ns

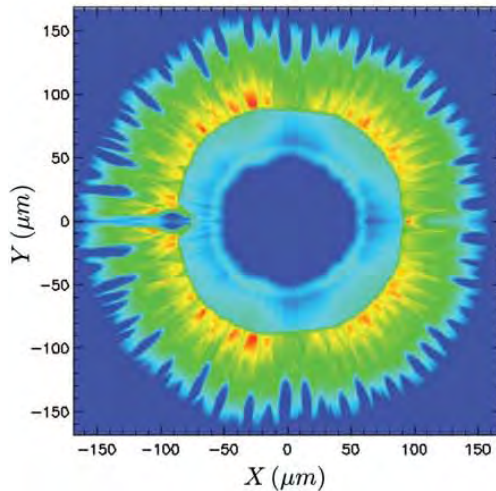


$t = 16.45$  ns

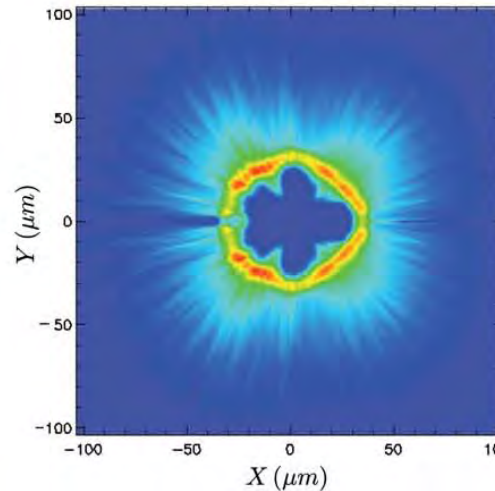


Parameter	Scale-1	Scale-2	Scale-5
Pellet mass (mg)	0.58	1.17	2.89
$R_1$ ( $\mu\text{m}$ )	512	640	871
$R_2$ ( $\mu\text{m}$ )	237	300	407
$R_3$ ( $\mu\text{m}$ )	108	136	177
Initial aspect ratio	2.48	2.47	2.49
Convergence ratio	64	65	63
Peak velocity (km/s)	286	260	220
Laser energy (kJ)	243	398	727
Highest gain	101	143	210

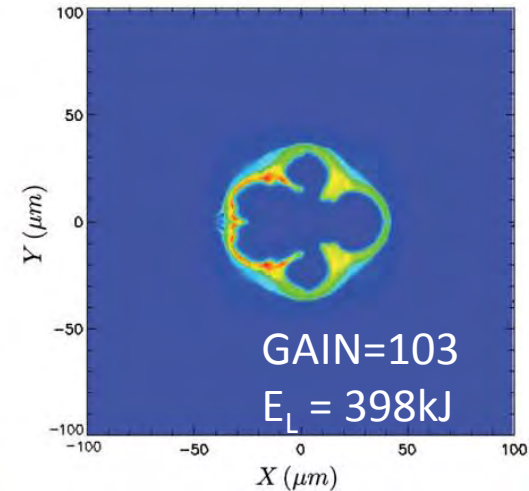
$t = 16.70$  ns



$t = 16.85$  ns



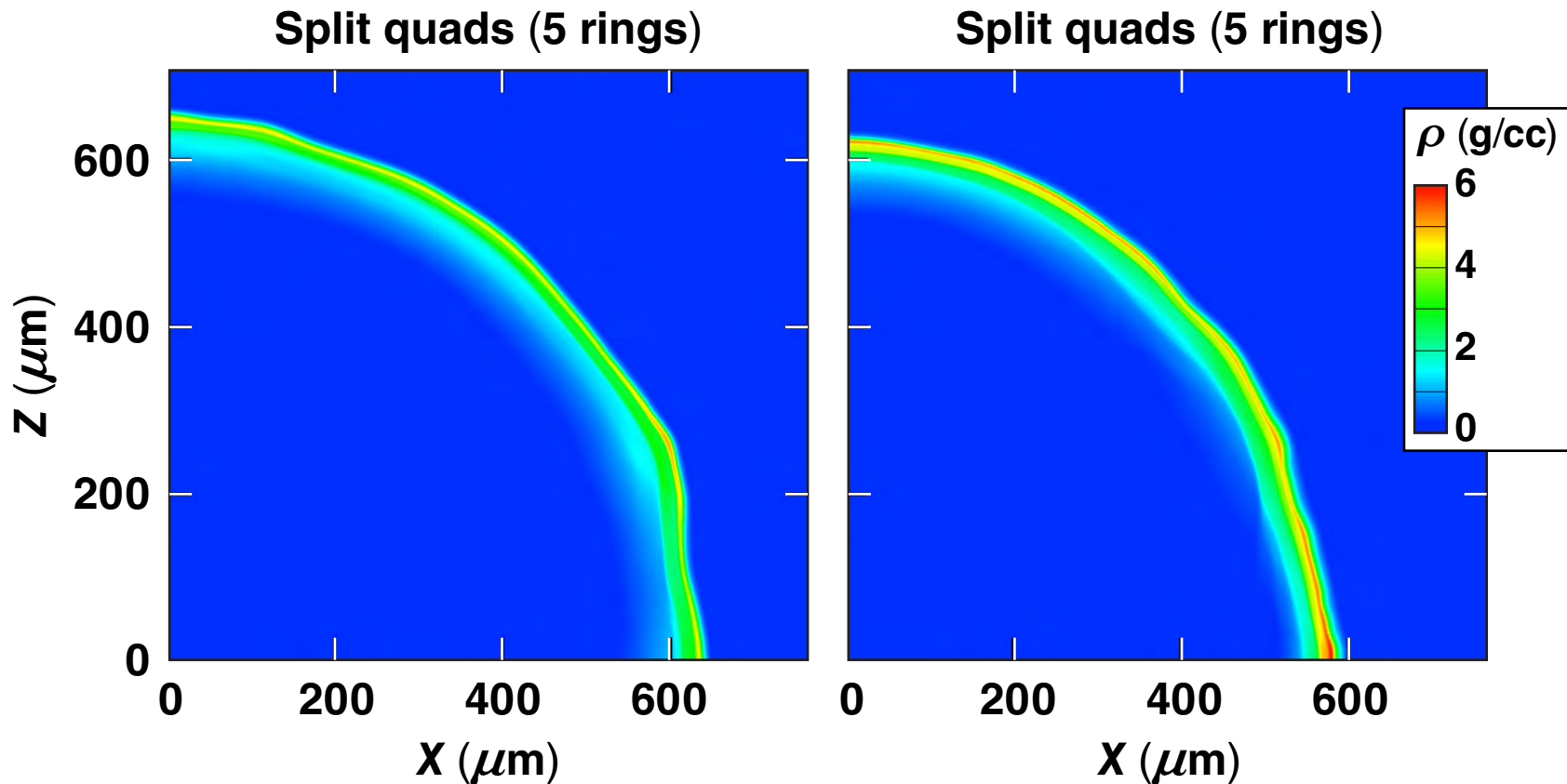
$t = 16.94$  ns



# Preliminary *DRACO* polar-drive shock-ignition simulations indicate reasonable uniformity, but refinements are needed



Time = 11.75 ns



Laser-imprint studies are also in progress.

# Laser Plasma Interactions: Late time SRS generated by the shock is probably benign and may be beneficial to the shock drive



- Early time  $2\omega_p$  hot electrons are main concern (near-term experiments?)
- SRS/ $2\omega_p$  hot electrons generated by high intensity shock may:
  - (will) be absorbed in outside of dense converging shell
  - improve the ablation process?
  - provide good ablative stabilization ?
  - contribute to symmetric shock drive by long mfp smoothing?
  - permit effective drive at  $2\omega_p$  (green)?
- Efficiency, symmetry and stability of shock coupling is a paramount research issue (near-term experiments?)

