### Introduction

### Diagnosing OMEGA and NIF Implosions Using the D<sup>3</sup>He Spectrum Line Width

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#### Abstract

Wedge Range Filter (WRF) spectrometers are used to diagnose implosions containing D and <sup>3</sup>He gas through measurements of the proton spectrum  $[D+^{3}He \rightarrow p (14.7 \text{ MeV}) + ^{4}He (3.6 \text{ MeV})]$ . The total line width is due to the thermal Doppler broadening, instrumental broadening, and several other effects. The significances of these sources of broadening are calculated using a Monte Carlo code. Using this code we constrain the ion temperature in OMEGA exploding pusher shots. Alternatively, we constrain the amplitude of high-mode asymmetries in a NIF implosion from the previous campaign (N091123), and will apply these models to D<sup>3</sup>He exploding pushers on the NIF during the Magnetic Recoil Spectrometer (MRS) calibration.

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### **Motivations**

- To investigate the possibility of using WRFs as a compact and accurate/precise T<sub>i</sub> diagnostic based on the line width method
  - Calibrate vs the yield ratio method on OMEGA
  - Could be used to check the NIF neutron time of flight (nTOF) T<sub>i</sub> on the NIF ignition diagnostics commissioning shots
- To explore possible high-mode ρR asymmetry amplitude measurements
  - Could be used on NIF SymCap shots
  - No current diagnostic for high-mode  $\rho R$  asymmetries on the NIF

### Wedge Range Filter (WRF) Spectrometers are used to measure proton spectra



We use the "D vs. E" curve to calculate  $E_d$  from the track diameter and the slope of the wedge to determine the filter thickness based on linear position:

 $\mathbf{E}_{i} = \mathbf{E}_{i}(\mathbf{d}, \mathbf{x})$ 



Each WRF is individually calibrated on the MIT accelerator

# Calculating contributions to the line width

#### We characterize each of the factors that contribute to the spectral broadening of the D<sup>3</sup>He-p spectrum

	Source		
$\sigma^2_{\ total} =$	$\sigma^{2}_{instrumental}$	Response function of the WRF	
	$+ \sigma^2_{thermal}$	Initial distribution due to finite temperature	
	$+ \sigma^2_{dispersion}$	More downshift for lower energies	
	$+ \sigma^2_{\text{straggling}}$	Not every proton is downshifted the same	
	$+ \sigma^{2}_{temporal evolution}$	ρR evolution over shock burn duration	
	$+ \sigma^2_{\text{geometric}}$	finite burn region; different cord lengths	
	$+ \sigma^2_{low-mode modulations}$	Spatially-dependent pR	
	$+ \sigma^{2}_{high-mode modulations}$	High-mode pR asymmetries	
	$+ \sigma^2_{other}$	E-field, ablated mass, etc.	

#### Calibrations on the MIT accelerator are used to infer the WRF instrumental broadening:



For more information see poster:

N. Sinenian et al. "The MIT Nuclear Products Generator for development of ICF diagnostics at OMEGA / OMEGA-EP and the NIF" 6

### A 3-D Monte Carlo code has been developed to characterize the broadening components

This code includes:

- Stopping power and straggling: Plasma [1,2,3] or cold matter (SRIM)
- Shell: arbitrary mode polar/azimuthal  $\rho R$  asymmetries
- D<sup>3</sup>He-p Source: Gaussian radial and temporal burn profile. Isotropic proton emission.
- Possible future additions:
  - Field structure around capsule, ρR and T profiles within target, ablated mass, plasma scattering.

<sup>[1]:</sup> C. K. Li and R. D. Petrasso, Phys. Rev. Lett. 70 (20), 3059 (1993).

<sup>[2]:</sup> S. T. Butler and M. J. Buckingham, Phys. Rev. 126 (1962).

<sup>[3]:</sup> N. R. Arista and W. Brandt, Phys. Rev. A. 23 (1981).

## Lower energies of a thermal distribution are ranged down more than higher energies (pR Dispersion)



# Calculating contributions to the line width (cont)

#### Because collisional processes are random, a monoenergetic

source broadens while ranging through matter (pR Straggling)



SRIM (cold matter) gives  $\approx 10$  keV more straggling broadening

#### Protons born at different times experience different downshifts due to ρR time dependence (ρR Evolution)

For a Gaussian shock burn in time, assume that  $\rho R(t) = \rho R_0 + t \times (\Delta \rho R/2\sigma_{burn,t})$ 



### An extended source creates broadening because protons experience different arc lengths in the shell



The source is modeled as Gaussian with a variable  $\sigma_{burn,r}$  on the order of tens of  $\mu m$ . Actual source profiles have been measured on OMEGA [4].



[4]: F. H. Seguin et al., Phys. Plasmas 13, 082704 (2006).

# ρR asymmetries cause broadening due to varying ρR

 $\Delta \rho R$  is the fractional amplitude of  $\rho R$  modulations.  $\rho R = \rho R_0 [1 + \Delta \rho R (\cos[n\theta] + \cos[m\phi])]$ Broadening due to low-Parameters:  $\rho R_0 = 40 \text{ mg/cm}^2$ mode asymmetry (P2)  $\sigma$  (keV)  $T_i = 10 \text{keV}$ Shell<sup>.</sup> 60  $R_{inner}=180\mu m$ 40% P2 mode 40 R<sub>outer</sub>=200µm CH 20 0  $0.1 \quad 0.2 \quad 0.3 \quad 0.4 \quad 0.5 \quad \Delta \rho R$ Broadening due to high-mode (100) modulations Even a small  $\sigma$  (keV) amplitude 400 Mode 100 (in asymmetry can 300 both angles) contribute 200  $\Delta \rho R = 0.5$ significantly to 100 the total line width  $0.2 \quad 0.3 \quad 0.4 \quad 0.5^{\Delta \rho R}$ 0.1

### **Applications**

## Feasibility of using the line width as a temperature diagnostic for OMEGA Exploding Pushers

<u>Goal</u>: To precisely measure  $T_i$  with the Doppler line width by eliminating other broadening sources.

<u>Parameters:</u> (with error estimates)

- $\rho R = 4 \pm 0.5 \text{ mg/cm}^2$
- $R_{source} = 40 \pm 5 \ \mu m$
- Temporal evolution:  $\Delta \rho R = 0.3 \pm 0.1$
- •No modulations in  $\rho R$

$$\frac{\text{Shell: } R_{\text{shell}} = 200 \ \mu\text{m}}{T_{\text{i,shell}} = 1 \ \text{keV}}$$

Most broadening consistent with above parameters:  $\sigma_{max} = 245 \text{ keV}$ Least broadening consistent with above parameters:  $\sigma_{min} = 236 \text{ keV}$ 

 $\sigma_{instrumental} = 168 \pm 18 \text{ keV}$ 

Uncertainty in  $\sigma_{\text{thermal}} \cong (((\sigma_{\text{max}} - \sigma_{\text{min}})/2)^2 + 18^2)^{1/2} = 20 \text{ keV}$ Ti =  $\sigma_{\text{thermal}}^2 / 5880$ 

Temperature uncertainty:  $\pm 20\%$ 

### Temperatures are calculated for OMEGA D<sup>3</sup>He exploding pushers

Can use simulation results to infer the amount of non-thermal broadening:

#### Parameters:

- $\rho R = 4 \text{ mg/cm}^2$
- $R_{source} = 50 \ \mu m$
- Temporal evolution:  $\Delta \rho R = 0.3$
- $\bullet$  no  $\rho R$  modulations

 $\sigma_{non-thermal} = 45 \text{ keV}$ 

 $T_i$  uncertainty = 20% (See slide 13)



For more info on ratio method T<sub>i</sub> see [5]

May be some unmodeled broadening effect remaining (E-field evolution?) or burn region effect in the yield ratio method.

[5] Poster by M. Rosenberg et al.

## Feasibility of using the line width as a high-mode asymmetry diagnostic (NIF CH implosions)

<u>Goal:</u> To put a limit on the amount of high-mode  $\rho R$  asymmetries in an implosion

<u>Parameters:</u> (with error estimates)

•  $\rho R = 40 \pm 5 \text{ mg/cm}^2$ 

Shell: 
$$R_{shell} = 200 \ \mu m$$
  
 $T_i = 1 \ keV$ 

- $R_{source} = 50 \pm 10 \ \mu m$
- Temporal evolution:  $\Delta \rho R = 0.3 \pm 0.1$
- P2 mode with amplitude 0-0.4

•
$$T_i = 10 \pm 2 \text{ keV}$$

Most broadening consistent with above parameters:  $\sigma_{max} = 385 \text{ keV}$ Least broadening consistent with above parameters:  $\sigma_{min} = 275 \text{ keV}$ 

 $\sigma_{instrumental} = 168 \pm 18 \text{ keV}$ 

$$\sigma_{\text{unc}} = \cong (((\sigma_{\text{max}} - \sigma_{\text{min}})/2)^2 + 18^2)^{1/2} = 57 \text{ keV}$$

High-mode amplitude ( $\Delta \rho R$ ) uncertainty:  $\pm .06$ 

### We attempt to constrain high-mode amplitude with WRF data from NIF D<sup>3</sup>He indirect-drive CH shell targets



### **Future Work and Conclusions**

### **Future Work**

- Additional modeling for existing data
- MRS calibration shots on the NIF (August)



#### **Summary of broadening effects**

Source	σ (keV) CH shell	σ (keV) Expl. Pusher	Notes
Instrumental	150-190	150-190	Error in $\sigma$ of +/- 15 keV
Thermal	170-240	170-240	Very well characterized; for 5 <t<10 kev<="" th=""></t<10>
ρR Dispersion	98	28	$\rho R = 40 \text{ mg/cm}^2 \text{(CH)}, 4 \text{ mg/cm}^2 \text{(E.P.)}$
ρR Straggling	53	16	$\rho R = 40 \text{ mg/cm}^2 \text{ (CH)}, 4 \text{ mg/cm}^2 \text{ (E.P.)}$
ρR Evolution	120-250	10-25	$\Delta \rho R=0.2-0.4$ ; $\rho R=\rho R_0(1\pm\Delta\rho R)$ for t= $\pm 2\sigma_{burn}$
Geometric	50-160	~20-30*	Source $r_0 = 30-60 \mu m$
Low mode ρR modulations	0-70	~0*	For $\Delta \rho R = 0-0.5$ , P2 Mode
High mode ρR modulations	0-460	0-50	For $\Delta \rho R = 0-0.5$ , mode 100
E-fields, Abl. mass	?	?	Not modeled yet
Total	280-640	230-310	

\*: poor statistics in current simulations

### Conclusions

- Using a simple Monte Carlo code we model several broadening effects of an implosion that affect the D<sup>3</sup>He spectrum line width.
- Using these results we calculate an ion temperature based on the Doppler broadening for D<sup>3</sup>He implosions on OMEGA
  - Possible other source of broadening (E-fields?).
- With the developed code we constrain the amplitude of high-mode  $\rho R$  asymmetries in a NIF implosion to  $\leq 0.26$ 
  - More modeling work is necessary to increase the confidence in this result.